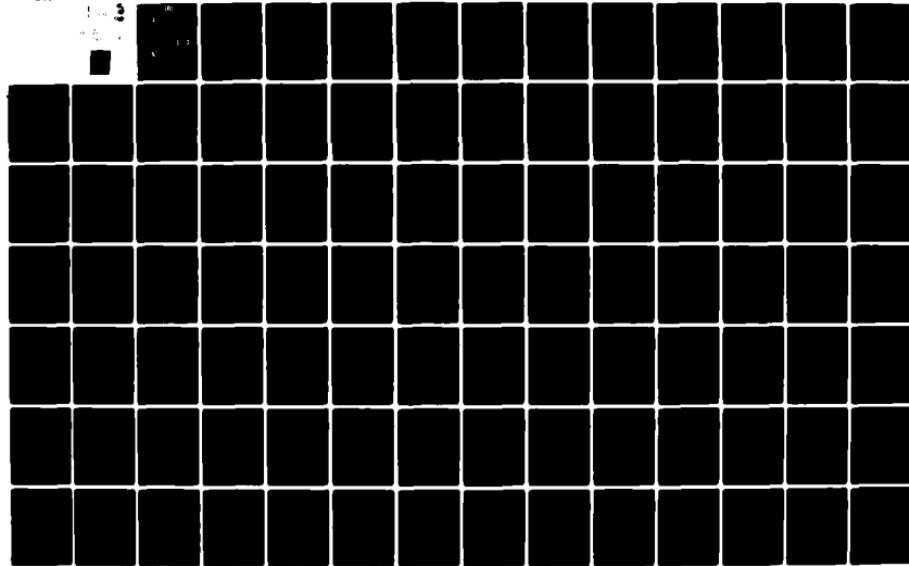


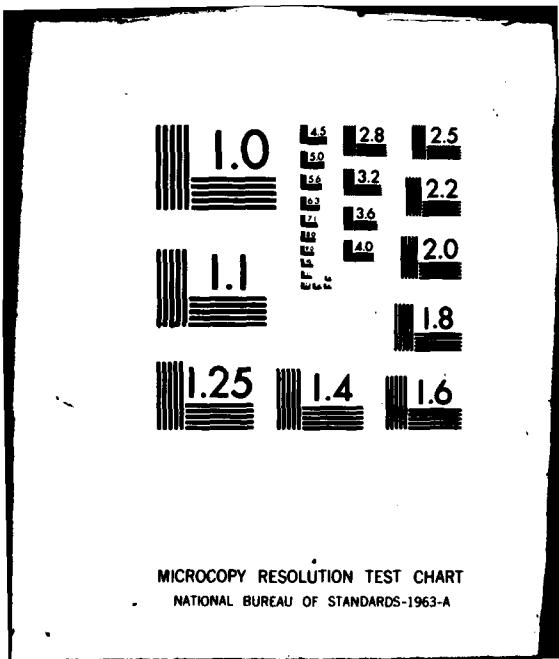
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Technical Report D-80-5

A HEURISTIC ROUTE SELECTION MODEL FOR LOW LEVEL
AIRCRAFT FLIGHT THROUGH DEFENDED TERRAIN

Michael James Dorsett
Plans, Analysis, and Evaluation Directorate
US Army Missile Command

MAY 1980

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U.S. ARMY MISSILE COMMAND
Redstone Arsenal, Alabama 35809

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information concerning air defense deployment, initial and destination points, and terrain data to specify a minimum-exposure, minimum-elevation route.

The results include the development of routes for eight 10 by 10 kilometer areas, and six larger terrain areas varying in size from 20 by 20 kilometers to 35 by 35 kilometers. Validation shows the heuristic to be competitive with visual procedures, but at a large reduction in time.

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CHAPTER I

INTRODUCTION

1.1 Background

Throughout history man has engaged in battle with his fellow man. A review of history is a review of warfare. Man seems to have a general propensity to consider warfare a major objective in his life. The early settlers of this country encountered a formidable foe in the native Americans. The covered wagon caravans were the early settlers' attempts to minimize the Indian threat when traveling West. Further, the scouts would seek high vantage points in the terrain where they could observe and provide early warning of enemy forces and their movement.

Scientific and technological developments have provided present day man with complex equipment and devices with which to do battle with his enemies. Commonplace among this arsenal are missiles, high performance aircraft, helicopters, air defense systems, tanks, radars, submarines, and a host of sophisticated hand-held weapons including lasers. It should be noted that the radar replaces the observer on the lonely hill top, while tanks and armoured vehicles replace the covered wagons. The major difference in the two scenarios is the equipment of which aircraft, missiles and air defense systems are of concern in this research effort. It is with the concept of air defense that modeling becomes paramount, since models permit reality to be depicted for a very modest investment of time and money.

1.2 Air Defense Modeling

The effectiveness of medium and high air defense systems impose a high degree of risk to aircraft survivability when an aircraft is operating in the air space protected by these systems. This situation leaves low level flight as the only option open to the aircraft to avoid these air defenses. Aircraft are a high value resource which must be utilized wisely. Regardless of the results of the analysis, the mission has to be undertaken. The battle, and in turn the war, can only be won if one attacks. Thus, one must enhance the aircraft's probability of survival.

One means to increase the aircraft's chances of survival is to plan a route which minimizes its exposure to enemy air defenses. A terrain following route can be optimized in the vertical plane, but the initial question is where to position the ground track in the horizontal plane that the aircraft will follow. If one knew the route which minimized the exposure, then there would be an easing of the vertical constraint imposed by the air defenses [1].

The objective of this research is to develop a heuristic method for selecting a minimum-exposure, minimum-elevation route for terrain following flight through defended terrain. Considering the expensive aircraft in use today, the computer modeling of air operations on the tactical battlefield is a useful tool for assessing tactics, performance, and results.

1.3 Research Topic

If one knew the location of low exposure routes, then an assessment could be made on the expected outcome of employing these routes. The high exposure route is merely to allow the aircraft to fly within the

radar coverage. This research was undertaken to find a method which allows one to find the low exposure route from some initial point to a destination point.

A minimum exposure route will logically use terrain features to hide the aircraft from the air defense sensors. This assumption implies that low elevation areas should have a lower exposure profile than high elevation areas. It is intended to use the low elevation areas as the basic units from which a minimum exposure route can be built. Thus, a heuristic route selection model will be developed in this dissertation that achieves a minimum-exposure, minimum-elevation route for low level flight.

1.4 Outline of Succeeding Chapters

Chapter II is a review of the literature pertaining to routing, aircraft and air defense. Three documents of particular interest to this research are discussed first. The remainder of the chapter pertains to the literature in general. The tactical situation from which this research derives is given in Chapter III. The scenario is typical of a medium intensity battle. The development of the model is presented in Chapter IV. The discussion follows the solution sequence of the model.

Chapter V is an example of the model selecting an appropriate route for the prescribed conditions. The calculations are based on the material of Chapter IV. The model results are contained in Chapter VI. The results for two small terrain areas are presented first, followed by the results for a much larger terrain area.

Chapter VII is the validation of the developed model. Some of the model results are compared to manually developed, preferred routes. Finally, Chapter VIII presents the conclusions of this research and recommendations for further research.

CHAPTER II

LITERATURE REVIEW

2.1 Introduction

An intensive review of the literature identifies three research results which are pertinent to this effort. A recent dissertation by James E. Funk [2] provides a method for determining the optimal vertical flight path for a given route. The second effort was reported in The University of Alabama in Huntsville Research Institute (UARI) Report, Optimal Attack Route Selection Method [3]. The third research of interest is a Helicopter Route Selection Model developed by Ohio State University for the large land combat model DYNTACS [4]. In addition, the literature pertaining to network modeling, computer software algorithms, geology and geography, highway routing, and electronic circuit routing were investigated to determine their applicability in aircraft routing.

Modern air defense systems have the capability to deny medium or high altitude aircraft attack routes to a target. To overcome this restriction, low level flight has now become a preferred method for penetrating air defenses. Low level or terrain following flight paths, however, presents the problem of impact with the terrain. In the literature this problem is also referred to as clobber.

The ideal flight path for terrain following would be a flight curve that matches the terrain curvature by some clearance height above the local terrain. The aircraft control system limits the vehicle to flying a smooth flight path which approximates this clearance curve. Figure 2.1

is an illustration of a typical terrain profile with the clearance curve and flight path for low level flight. The slower the aircraft flies the closer the flight path can approximate the clearance curve.

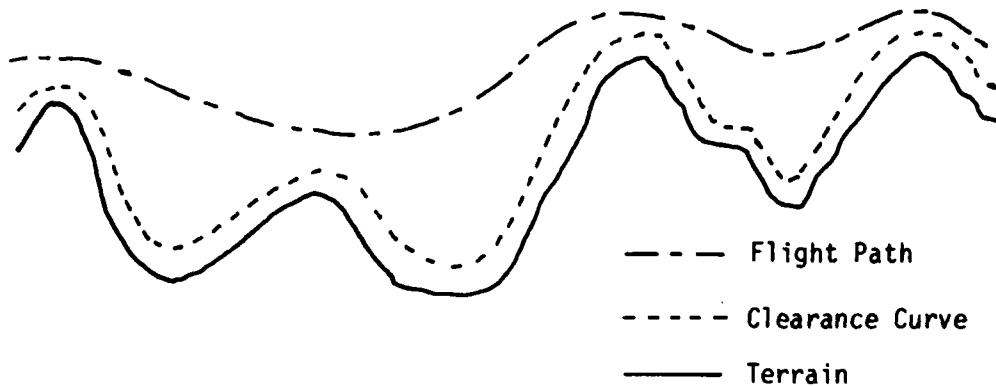


Figure 2.1. Low Level Flight Profile.

The review of unclassified documents concerning low level flight has centered on the problem of optimal aircraft control systems. Advances in microprocessors and digital electronics seem to be the controlling factor in increasing the capability of on-board flight computers and navigation systems [2, 5, 6]. With increased on-board computer capacity, real time optimization of flight profiles become possible, thereby achieving an optimal low level flight path along the selected route.

In the literature that was reviewed, a major consideration in any air defense study is terrain modeling. Terrain modeling is also utilized in such studies as highway routing and construction, pipeline routing, and land use. Most recent research in this area is directed at using computer graphics to depict the terrain in contour map form and in picture form. Existing terrain models are presently adequate for air defense modeling [7, 8, 9, 10, 11]. The terrain models, however, do not provide for aircraft route selection analysis.

2.2 Reported Research

The dissertation by J. E. Funk presents a mathematical programming method for solving the aircraft control problem in terrain following flight [2]. The first step in his approach was to construct a trajectory model which is incorporated into the objective function or, as he has defined it, the performance function. The performance function is defined in terms of an excess clearance variable. The function is optimized subject to differential constraints of height, slope and curvature of the flight path.

To provide computational ease the problem is discretized. The performance function and constraints are transformed to a matrix form which can now be considered as a quadratic or linear programming (LP) problem. This quadratic or LP problem is solved using existing algorithms. To develop a complete flight path this procedure considers overlapping segments. Segment i of the flight path is optimized and then the next overlapping segment, $i+1$, is optimized with the initial portion of segment $i+1$ defined by segment i . Since the discrete segments overlap, the resulting flight path is continuous and there are no discontinuities at the boundaries.

In Funk's research, only the vertical terrain avoidance is examined, and not the lateral terrain avoidance. His results give a solution to the aircraft control system to yield the optimal flight path over a given terrain route.

In the UARI report, a dynamic programming approach for determining optimal attack routes is presented [3]. Although this work was performed several years ago, it is still current with techniques recently reported. The backwards solution method was employed to evaluate the recursive function.

The route selection process that was developed is a direct application of dynamic programming. To represent the multi-stage decision process, a grid network was used where each grid point is equivalent to a stage in the decision process. Thus, the optimal decision path is the optimal attack route.

The probability of survival, (P_s), is the return at each stage. The optimal path has the highest probability of survival or is the least risk route. The probability of survival at a grid point is given by:

$$P_s = (1 - P_k).$$

The probability of kill (P_k) for an air defense site is the resultant of the probabilities of acquisition, tracking, missile launch, missile flight, and warhead lethality.

Two recommendations for further research in this report were of interest. This technique had only been applied to small scale problems, and further research on large scale problems with multi-attackers and multi-radar sensors were suggestions for consideration. Also, it was recommended that network techniques such as shortest path or least cost path be considered.

The Helicopter Route Selection Model that has been developed is another method using dynamic programming [4]. This model is an adaptation of the ground unit route selection model that is a subroutine of DYNTACS X. The first step is to determine the intervisibility areas for each weapon. These areas define the masked and unmasked portions of the battlefield. From the set of masked areas a series of concealed areas in close proximity to one another can be connected to form an avenue of approach. Having identified this avenue the route can be selected that follows the general shape of the approach corridor.

Up to this point all analyses of intervisibility and terrain have been performed outside of the actual model. With the process completed the route corridor is defined in the model. The intervisibility areas are defined by a set of irregular convex shapes having straight line boundaries between each vertex. Along each boundary one or more points define the possible beginning (or end) of a route segment across the convex shapes (Figure 2.2). These points are shown as circles on Figure 2.2 and are also entered into the model as data.

With the terrain area thus described for the model, the route selection routine can be utilized. A series of nine points that are in the direction of attack are selected for route analysis. The selection routine evaluates these boundary points identified by the probability of survival at each point. The point with the highest probability of survival is selected and then the next series of nine points along the route corridor are considered. This process is the forward solution method for dynamic programming problems.

2.3 Open Literature

One of the first areas in the open literature to be investigated was cluster analysis. An excellent presentation of cluster analysis can be found in Anderberg's text [12]. When data has no discernible pattern, cluster analysis can provide a tool to uncover the pattern. Hierarchical clustering is widely utilized to develop the linking of data as each entity is processed. In this research, the idea of nearest neighbor and centroid of a cluster that is used with non-hierarchical clustering, are utilized as a basis for processing the terrain data.

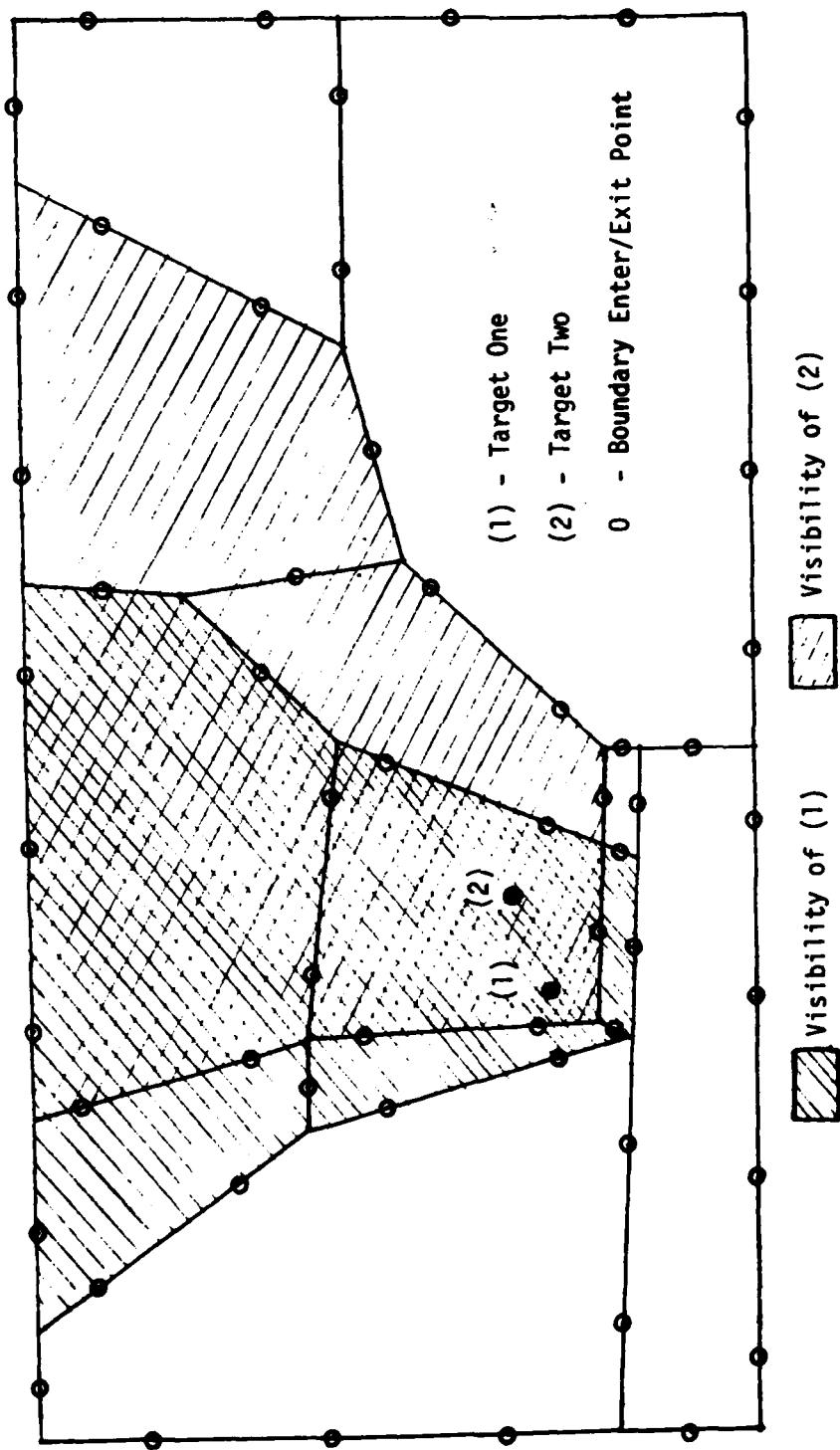


Figure 2.2. Partitioned Terrain Area.

For a data set of N observations, clustering into subsets of like values indicates an association or similarity for the cluster membership which is not shared by those outside that cluster. Typically, the members of a cluster will minimize some criterion such as minimal distance from the mean of the cluster. The mean of a cluster can be utilized as the centroid. For the total data set of k clusters, membership in cluster i can have a point to centroid distance different from cluster j , which would indicate an individual cluster density. Thus, a higher order clustering can be performed on the initial clusters because their centroids are now the data points. The centroids of the first order cluster can be weighted according to density and be the point used as the value for the higher order clustering.

Clustering methods are means by which data can be grouped, associated, or placed in some classification scheme for analysis. There is no one preferred method to be used, as several methods normally need to be used to determine if there is any pattern or intelligence to be derived from the data.

The aircraft routing problem can be formulated as a network or a graph problem. In the literature, the theoretical aspects of a network are referred to as graph theory, whereas the practical aspects are known as network analysis. A highway network connecting cities would be vertices for the cities and edges for the highways when related to graph theory. Networking would refer to the cities as nodes and the highways as arcs. Depending on the reference, the terminology for the cities could also be called junction points, intersection points, or simply points; and likewise, an arc could also be a branch, link, path or line.

For a network or graph G there is a collection of points x_1, x_2, \dots, x_n (denoted by the set X), and a collection of lines a_1, a_2, \dots, a_m (denoted by the set A) which join some or all of these points. The graph is described and denoted by the doublet $G(X, A)$ [13]. An edge joining x_i with x_j is denoted by $[x_i, x_j]$.

In network analysis and cluster analysis there are three distance measures that are of interest. First, the standard Euclidean distance or metric for two points in space is given by:

$$d = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}.$$

Second, in many location problems, especially in urban areas, travel is along an orthogonal set of streets. Travel which is restricted to directions parallel to the coordinate axes use a rectilinear or Manhattan metric that defines distance between two points (x_1, y_1) and (x_2, y_2) by:

$$|x_1 - x_2| + |y_1 - y_2|.$$

The rectilinear metric could have been used in the UARI Optimal Attack Route Method since travel was restricted to grid lines. Third, when travel is restricted to take place on a network, then the internode lengths are the distance measure [14].

The above concepts were utilized in developing the approach to the route selection process for low flying aircraft. The ideas of nearest-neighbor and cluster centroid form the bases for the terrain data reduction.

CHAPTER III

PROBLEM FORMULATION

3.1 Tactical Scenario

This research considers an area of air defense war gaming. There are two basic situations that a tactician can analyze. In one case, the tactical situation is portrayed from the defender or air defense site aspect. For the other case, the tactical situation is presented from the attacker or pilot's viewpoint. The specific problem this research addresses is that of selecting a route which a low flying aircraft can use to penetrate the air defense coverage, while at the same time minimizing the aircraft exposure to these defenses. Low flying aircraft ordinarily fly within 200 meters of the terrain.

The defender desires to allocate his air defenses in a pattern to achieve maximum coverage. The sensors (radar, infrared, or visual) are positioned in the terrain to be defended such that visibility is maximum in the principle direction the site is responsible for protecting. In actual terrain there can be certain azimuths for which coverage is marginal or non-existent. To ensure that the total area is covered, the air defense sites are situated so that individual site visibilities overlap each other thereby providing a pattern with total coverage. Thus, any portion of the total area is being covered by one or more air defense sites. The attacker is faced with the situation of attempting to select a route which avoids these sites and maximizes his survival while reaching the target, and accomplishing the mission.

Along with terrain following, there are some other options the tactician can choose to enhance the aircraft and pilot's survivability. The attacker can use electronic countermeasures (ECM), better known as jamming. An anti-radiation missile (ARM) could be fired at each radar. Decoys or remotely piloted vehicles (RPV's) could be utilized to saturate the skies so that an aircraft can be hidden among the RPV's. To reach the primary target, a preemptive raid could be made against the air defenses. Of course, the defender is fully aware of these and other methods that can be employed to negate the air defense's ability to engage the attackers.

3.2 Aircraft Route Selection

In this research, the air defense situation is a heavily defended 35 by 35 km area through which a helicopter force must penetrate. The air defense sensors are assumed to be deployed within this region such that maximum coverage exists.

Using military terminology, the line of battle between two forces is known as the forward edge of the battle area (FEBA). The helicopter force is flying a terrain following flight path from their base across FEBA to raid an enemy rear area base. The enemy air defense sensor capability is assumed to have good low altitude coverage for a 10 km radius and good long range coverage for medium and high altitude.

In performing this raid, the objective is to traverse the whole route undetected, thus preserving the element of surprise in the attack. The air defense sensors are not being attacked or jammed in this raid. In an attempt to obscure the helicopters' approach to the target, the mountains and hills would be utilized as a mask. Intuitively, the best low level aircraft route would follow the lowest terrain. To offset this

tactic, the enemy will position some air defense sites to cover low altitude corridors into his area.

The interaction of these tactics results in the helicopter route selection being that of finding the low level route which has the fewest air defense sites covering it. Thus, a route is a linkage of several low level path legs into a continuous path that will allow the aircraft to avoid detection.

3.3 Sensor Coverage

With low altitude targets, radar sensors have clutter problems when receiving the return signal. There can be a high level of noise because of ground objects and terrain features which tend to obscure any targets that may be nearby. Any aircraft operating in an area with opposing air defenses will attempt to fly as low as possible so as to be in the clutter of the radar return signal. However, the faster the aircraft speed the higher it must fly to be responsive to the pilot's terrain avoidance commands. Thus, the aircraft pilot has two conflicting constraints; first, the aircraft must fly no higher than X meters to avoid detection, yet, second, it must fly at least Y meters above the terrain to maintain a clearance altitude. A major problem exists for the pilot when Y is greater than X.

The degree of coverage a radar site possesses from a given location is dependent on the target altitude and the local terrain. An aircraft at 50 meters altitude is more likely to be detected than an aircraft at 20 meters altitude. To graphically illustrate sensor visibility, a series of actual coverage diagrams for three sites were made at target altitudes of 20 and 50 meters. Penetrating aircraft are assumed to be approaching the sites from the west (left edge of figures). Coverage diagrams are

generated using a computer routine that generates the visibility from a site to the target altitude for 0 to 360 degrees in azimuth.

The first site, Figure 3.1, has excellent coverage to the west at each altitude. For increasing target altitudes only a small improvement in visibility is obtained. Visibility for a 10 km radius at 20 meters target altitude is 28.02 percent of the total area. At 50 meters, visibility is 31.85 percent.

In Figures 3.2 and 3.3, the site has good coverage at each altitude. At 20 meters target altitude, visibility is 29.85 percent and improves to 43.10 percent at 50 meters. The prominent direction of coverage is west, but this site also has some coverage to the east.

Lastly, in Figure 3.4, a poor site location is shown. Visibility at this site varies from 5.31 percent at 20 meters to 8.63 percent at 50 meters. Coverage provided by this site is southerly.

These three site locations are deployed in the same area and the composite coverage is shown in Figure 3.5. In the overall coverage, the poorly situated site provides sensor detection to the south which the other sites lack. Thus, the poor location is better than expected because it furnishes satisfactory coverage when considering the combined coverage.

As can be seen in these series of figures, the coverage of an area by air defense sensors limits the ability of an aircraft to penetrate the area undetected. The deployment of several air defense sites imposes a visibility constraint on the selection of routes through the area. It may be impossible to find an undetectable corridor.

3.4 Terrain Data

The terrain data base used in this research is Defense Mapping Agency (DMA) terrain data which provides the height above sea level for

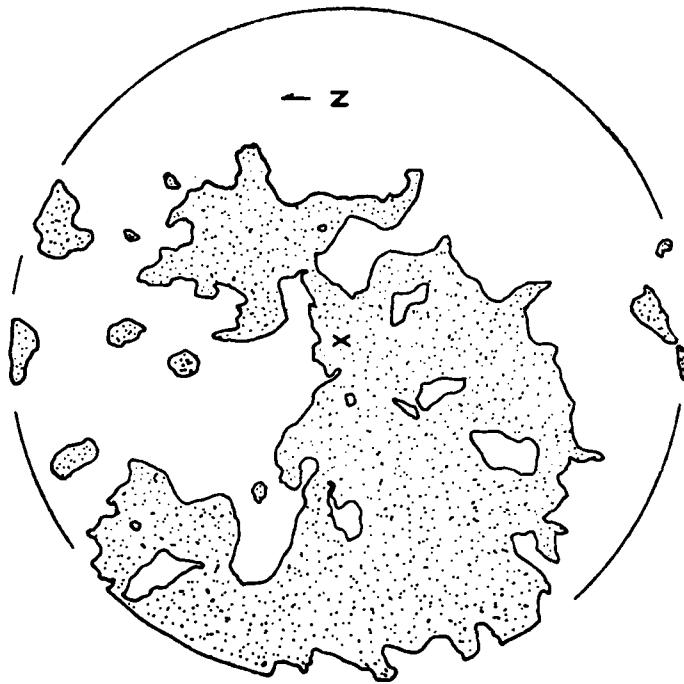


Figure 3.2 Site 2 - Target Altitude 20 Meters, Visibility 29.858

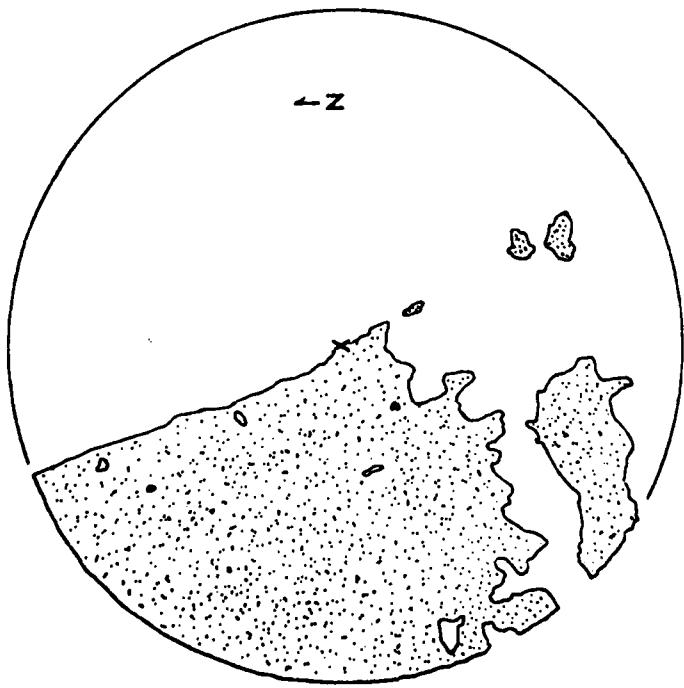


Figure 3.1 Site 1 - Target Altitude 20 Meters, Visibility 28.025

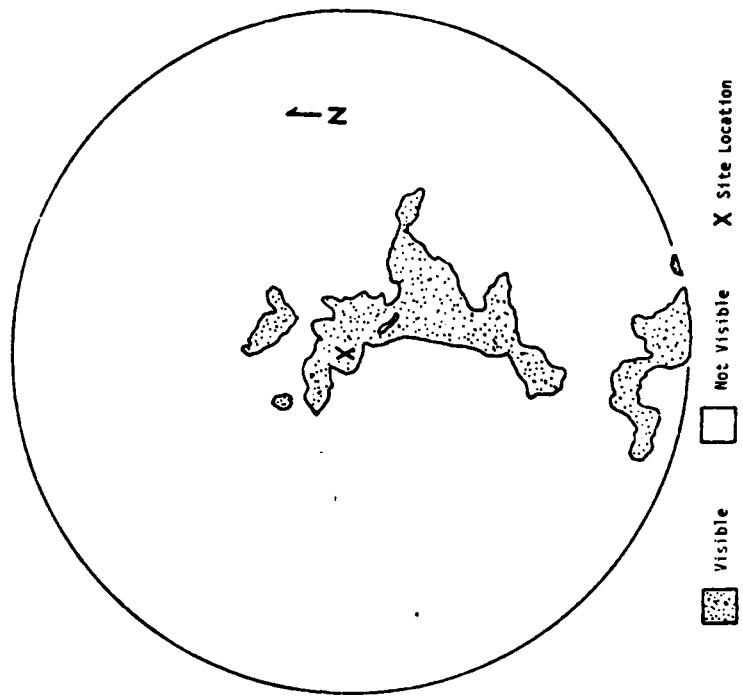


Figure 3.4 Site 3 - Target Altitude 20 Meters, Visibility 5.315

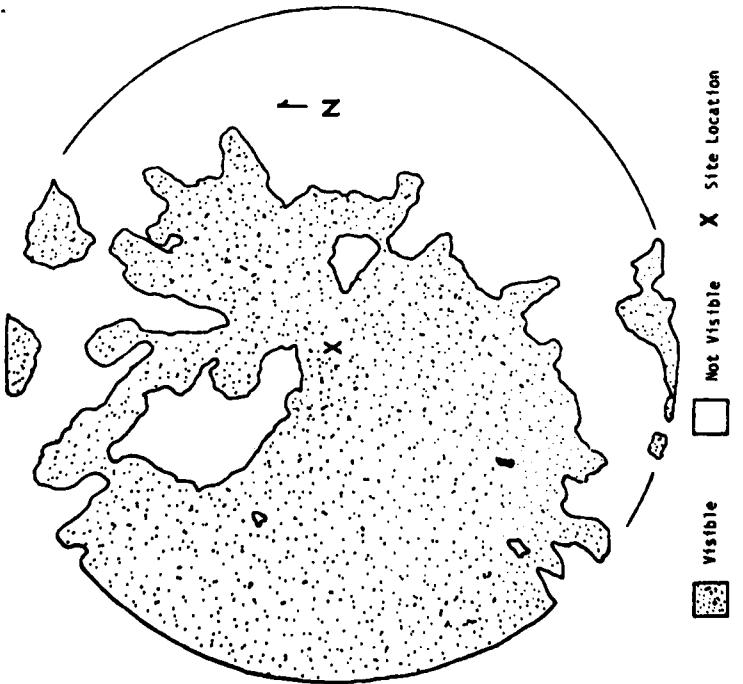


Figure 3.3 Site 2 - Target Altitude 50 Meters, Visibility 43.105

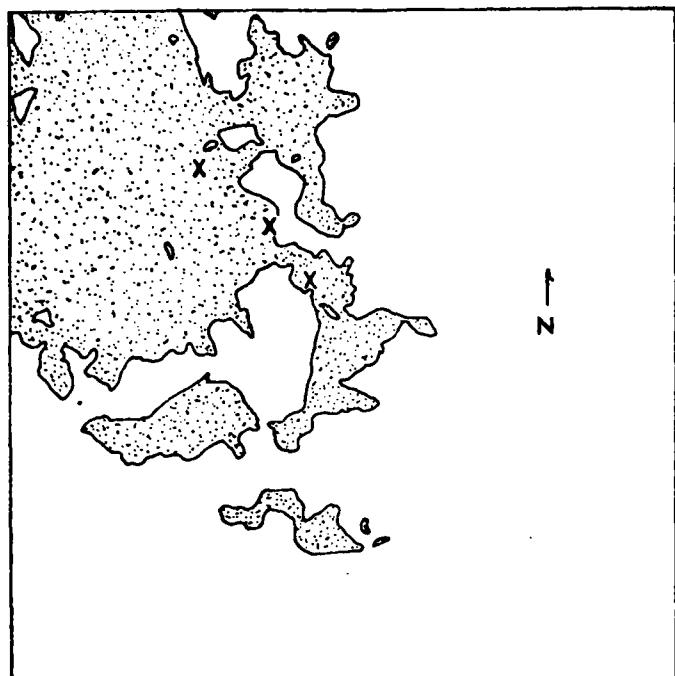


Figure 3.5 Composite of Sites 1, 2, and 3, Target Altitude 20 Meters

each terrain location. A granularity of 70.0 meters was selected in utilizing the data base. A problem with this fine a grid is the quantity of data points for even a moderate size area. For a 20 by 20 km area, this density results in 90,000 entries.

The first requirement in utilizing this data is to convert from a packed format into an array format of unpacked terrain points. The geographical area selected requires a 525 by 525 array (35 by 35 km). Since this array is too large for efficient computer processing, the area was partitioned into smaller arrays of 15 by 15. This arrangement results in a strip of 35 arrays to cover the north-south direction and 35 strips in the east-west direction (Figure 3.6). A map sheet is 15 data points from west to east, and 35 arrays of 15 data points from south to north.

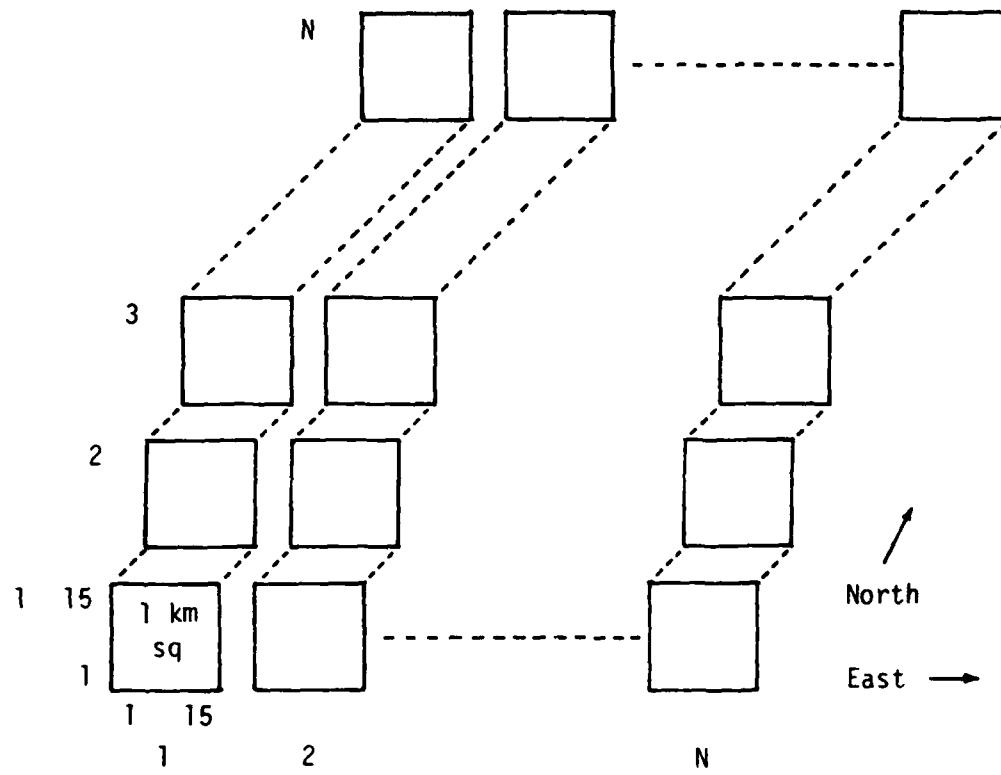


Figure 3.6. Terrain Data Arrays.

Once the terrain data is available from the conversion processing, some assumptions need to be made relating the data to the route selection problem. The premise that the aircraft route will follow the valleys and low areas requires that the low elevation terrain be identified from the terrain data. Thus, it is assumed that by a grouping or clustering process, these low elevation areas can be found. Also, the partitioning of the area allows for identification of local minimum altitudes rather than a single global value.

An example of terrain data arrays is shown in Table 3.1. As can be seen in this table, the variation in the point to point values can be stratified. Once the data is grouped into elevation intervals (or bands), the terrain relief is shown as plateaus with the lowest plateau being the lowest elevation area. The lowest stratum is a cluster of lowest terrain points from which the cluster center can then be used as a node point in the routing network.

With the terrain data analyzed and the node points established, the route can now be developed. The terrain route for the helicopter has only two known points at the onset - the initial point and the terminal point. All intermediate route points need to be selected from the nodes.

Table 3.1 Elevation Array

CHAPTER IV

MODEL DEVELOPMENT

4.1 Introduction

The route selection development begins with the basic terrain elevation data and ends with the minimum-exposure, and minimum elevation route. The model consists of several logical divisions that progressively solves this problem.

Initially, the model groups the terrain data into elevation bands from which cluster centroids (or centers) are developed. These centers become the node points for a routing network. Around a route node a neighborhood of node points is selected as possible links to this node. In this neighborhood each point has an exposure value which is a function of its visibility to enemy sensors, its altitude, and its distance from the node point. The exposure value is a penalty for the use of this point. Each linkage is a path or leg of the route, and all the linked nodes form a route connecting the minimum-exposure, and minimum-elevation points. The resulting path between the initial and final nodes provides a route for a penetrating low flying aircraft.

4.2 Clustering of Terrain Data

To group the terrain data into elevation bands the integer arithmetic feature of Fortran software is exploited. When arithmetic operations are performed on integer numbers, only the integer portion is

retained and the decimal portion is discarded. The following relation is utilized:

$$NE = (((E - 1)/INT) INT) + INT$$

where NE = the new elevation value,

E = the old elevation value,

INT = the band interval.

This calculation results in all elevation values within an INT interval of each other being assigned the maximum value of that interval. The process is identical to class intervals utilized in constructing a frequency table in statistical analysis. Instead of using the midpoint of the interval, the maximum in the class interval is used.

Once all the terrain data is stratified, then clusters of both high and low elevation points can be found. Each array of 15 by 15 covers an area of 1050 by 1050 meters. Within this area at least one low elevation cluster is identified along with a high elevation cluster. There are some cases where the whole array represents level terrain and the array consists of the same elevation values. When this situation occurs, it is necessary to check adjacent arrays to determine if this terrain is a low elevation cluster.

Since more than one low elevation cluster can occur in an array a method was developed to determine if two points were adjacent to each other. For a square grid a single point I has eight points around it as shown in Figure 4.1. The points labeled A through Q (less I) form a ring around the numbered points and cannot be adjacent to the point I.

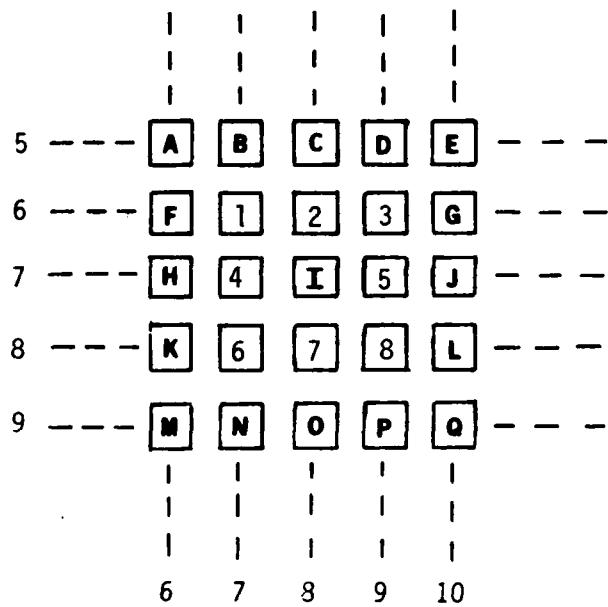


Figure 4.1 Points Adjacent to I

The array is processed sequentially by searching across each row; therefore, cluster membership is identified in order of occurrence from the beginning of the array. For example, assume that a cluster consists of the following points - I, 5, J, 7, 8 and P. These six points are a cluster located in the 15 by 15 array. The clustering procedure identifies all points of the same elevation by entering their position into a list. The indexes of a point are combined by letting INDEX = 100 (IROW) + JCOL, where IROW is the row index and JCOL is the column index. This coded number is the location of the point within the array.

In this example, let the point I be in row 7, column 8. The stored INDEX value for I is 708. The other cluster membership values are given in Table 4.1.

Table 4.1 Cluster Membership

Member	INDEX Value	I-Difference
I	708	0
5	709	1
J	710	2
7	808	100
8	809	101
P	909	201

When searching this list for cluster membership the value of INDEX provides a means to separate clusters. Since the membership is sequential, only those points occurring after I need to be examined (points 5, 6, 7 and 8). By subtracting INDEX values the difference indicates adjacency.

For a point to be adjacent to I the difference must be either 1, 99, 100 or 101; any other value indicates that the point is separated by one or more rows (or columns). Points 5, 7, and 8 are identified as belonging to the same cluster as point I before considering the next point in the list. When point 5 is evaluated, point J is placed in the I cluster. The evaluation of point J does not add any new points to the cluster since all points adjacent to J are already in the cluster.

Point 7 evaluation adds the last point P to the cluster. This subtraction method is a quick process for identifying adjacency.

After determining which points are in the cluster, a center or centroid of the cluster can be calculated. Since the data points are planar, then each cluster has a centroid that is defined by the mean values for X and Y within the cluster:

$$(\bar{X}, \bar{Y}) = \left(\sum_{i=1}^n \frac{x_i}{n}, \sum_{i=1}^n \frac{y_i}{n} \right)$$

The centroids are now used as node points in the route selection process. The centroids are separated into two groups. If the centroid is for a low elevation cluster, it is placed in a low elevation array. Likewise, centroids for a high elevation cluster are placed in a high elevation array. The centroids in the high elevation array are identified by a minus sign. Figure 4.2 gives the location of the low and high elevation centroids that were found in the 10 by 10 km area utilized in the model development.

4.3 Sensor-Node Line of Sight

A major consideration in selecting a tactical aircraft route is to ensure that the route avoids enemy air defenses as much as possible. To determine the degree of visibility along a route, each centroid has to have its line of sight (LOS) to each sensor determined. The result of this determination is an exposure value associated with each node point.

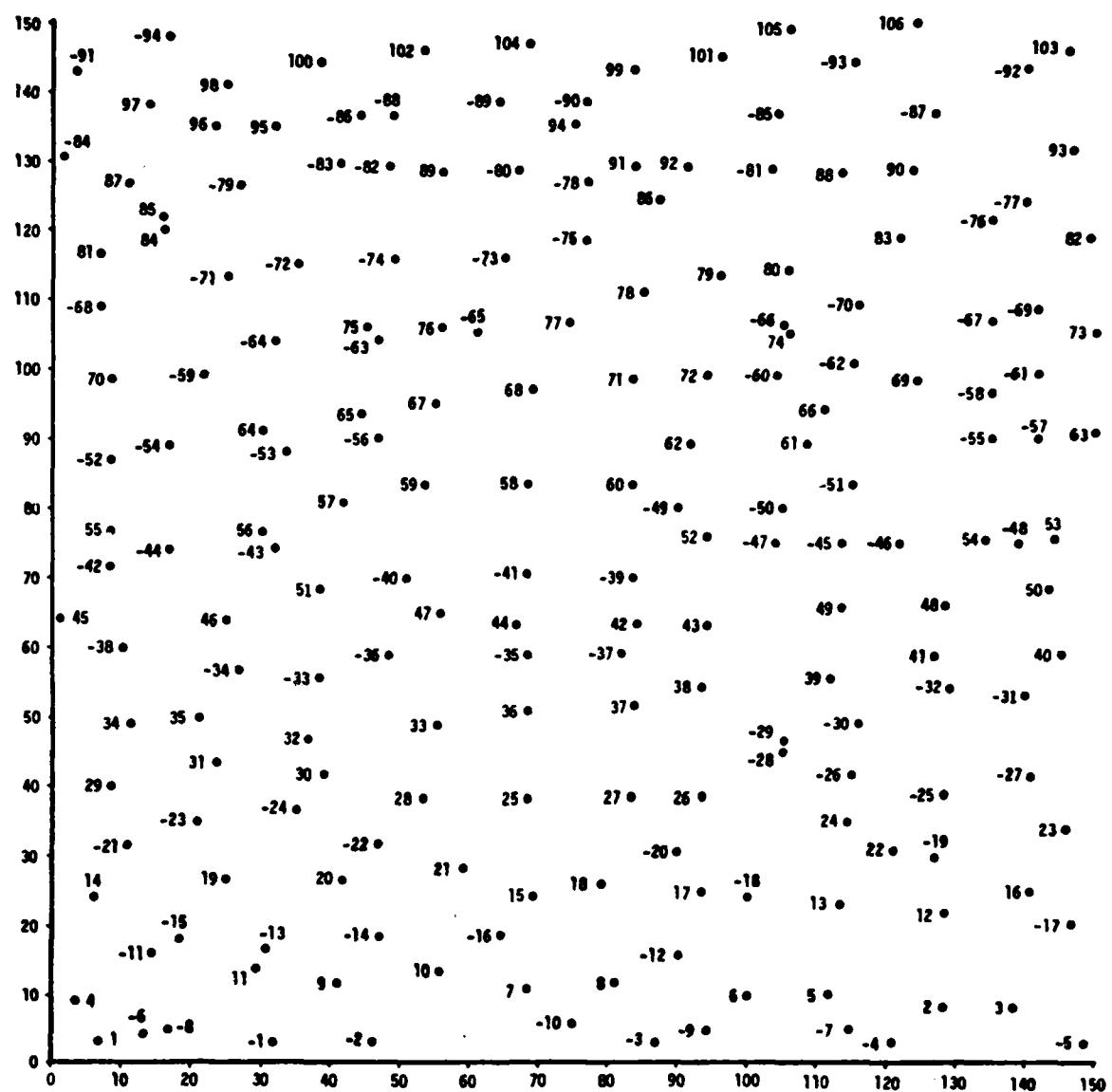


Figure 4.2 High and Low Nodes for Area One

To calculate the exposure value of a node point, the range between the node-sensor combination, together with the number of sensors, is required. The further a sensor is located from the node, the less of a threat it is since the probability of kill (P_k) is partially a function of range. However, the number of air defense sites having visibility to a point will increase the P_k . Since the sensors will tend to be deployed behind and along the general flow of the main battleline, an average range to sensors was selected as an exposure value. The exposure value is given by:

$$EP = NS \cdot \left[\frac{R_{max} - \sum_{S=1}^{NS} R_{Sj}}{R_{max}} \right]$$

where EP = the exposure value for node j with all sensors that have LOS with this node,

NS = the number of sensors that have LOS with node j,

R_{max} = the maximum node-sensor separation that exists for all node-sensor combinations,

R_{Sj} = the distance between the sensor and node j.

The value EP is calculated for all node-sensor combinations for both high and low elevation. As the route is being developed, the exposure values for the nodes are used as part of a penalty function. This discussion of the route selection is deferred to the next section.

For large areas of terrain, the data base has to be analyzed in segments or subareas that remain within computer core capacity. To satisfy

this restriction requires a bookkeeping method of array pointers to record the progress of the LOS calculations and which node-sensor pairs have been completed.

Referring back to Figure 3.6, the partition of the terrain data base is shown. Figure 4.3 presents the basic planar relationship between two nodes and a sensor. The + indicates the boundaries between each array of 15 by 15 terrain data points. Within this base the terrain elevation points represent X - Y coordinates of a square grid system. The vector between the node and sensor will intersect these grid lines and the array boundary lines. Along the X-axis the array boundary lines are also the map sheet boundary lines. Each intersection point of the vector and grid line is within 35 meters of a known elevation point. This known point is checked for masking of the node from the sensor. If masking occurs, the processing of this vector (or radial line as it is called in the air defense literature) is complete and the next node-sensor combination is processed [15]. If LOS exists at this intersection point, then the routine steps out of the vector to the next intersection. When the sensor location is reached and no masking terrain point has been encountered, then LOS exists between the node point and the sensor. The number of sensors which can see this node is then incremented by one.

To know which terrain point is along the LOS vector, the array indices are calculated from the vector-grid line intersection. The map sheets are read from west to east; therefore, all node-sensor vectors are oriented from west to east to allow one pass through all the data. In the model, the map sheet boundaries are named after the compass directions -

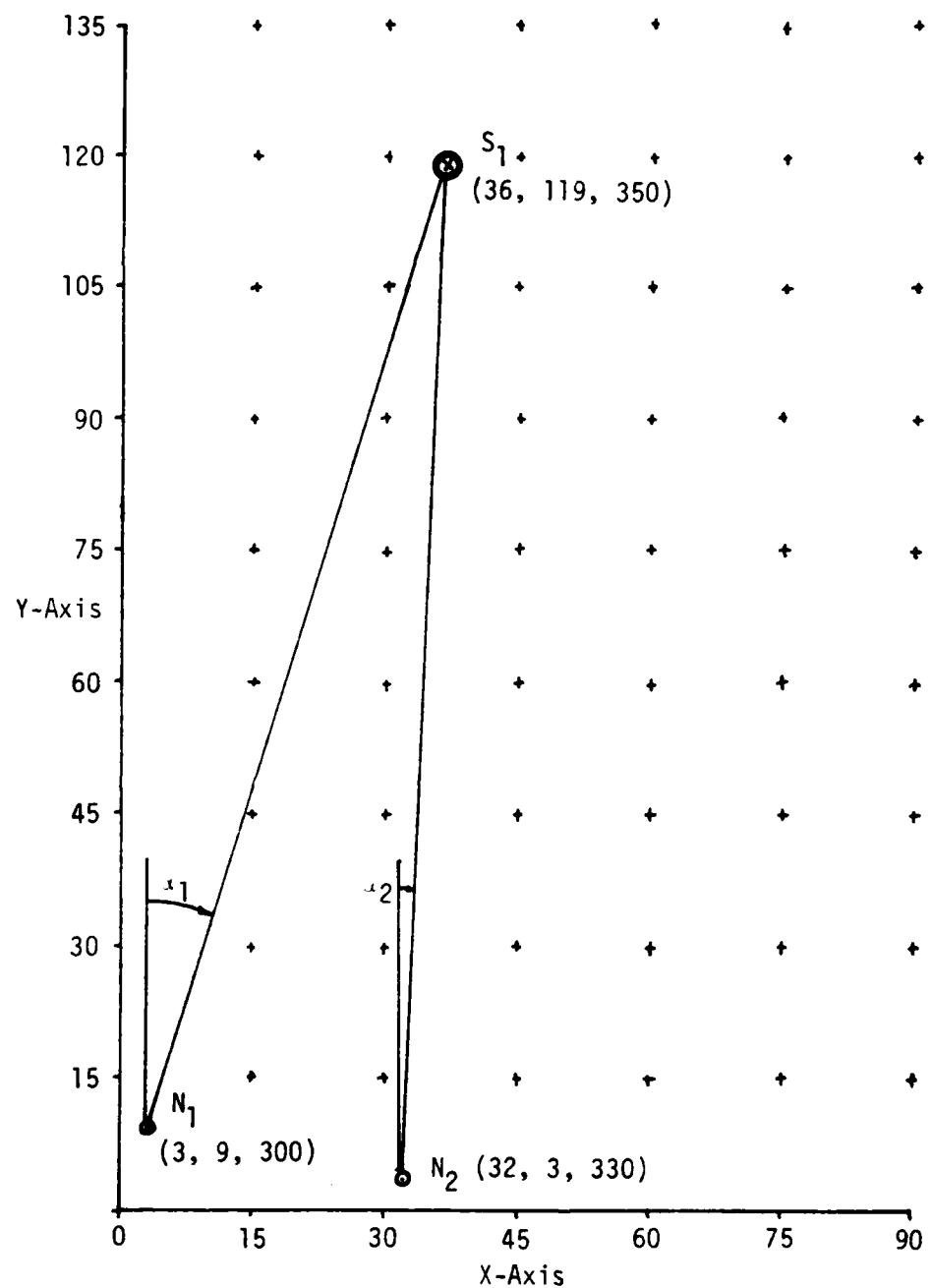


Figure 4.3 Sensor-Point Locations (X, Y, Z)

EAST, WEST, NORTH and SOUTH. As each map sheet is read, the previous EAST becomes the current WEST.

In Figure 4.3 the node point N_1 (3, 9, 300) and sensor location S_1 (36, 119, 350) define the end points of the vector $N_1 S_1$ with an azimuth angle α_1 . The other node-sensor vector is $N_2 S_1$ with an azimuth angle α_2 . The location of terrain points along these vectors becomes a trigonometric problem. The parameters defined below provide the indices needed to extract the terrain points from the data base.

$$d = \left[(x_2 - x_1)^2 + (y_2 - y_1)^2 \right]^{\frac{1}{2}}$$

$$\cos \alpha = (y_2 - y_1)/d$$

$$\sin \alpha = (x_2 - x_1)/d$$

$$\text{Comp } x = \begin{cases} 1 & , x_1 < \text{WEST} \\ (x_1 - \text{West})+1, & x_1 > \text{WEST} \end{cases}$$

$$\text{Left Comp } y = \begin{cases} \cos \alpha ((\text{WEST}-x_1)/\sin \alpha), & x_1 < \text{WEST} \\ 0 & , x_1 > \text{WEST} \end{cases}$$

where: d = the magnitude of the vector,

$\cos \alpha$ = the cosine of the azimuth angle,

$\sin \alpha$ = the sine of the azimuth angle,

Comp x = the x -axis component of the vector within the map sheet,

Left Comp y = the y -axis component of the vector for the West boundary.

From these parameters the row and column indexes can now be determined.

For a vector, the indices are given below.

$$\text{COLUMN } (x\text{-axis}) = \begin{cases} x + \Delta x & , |\sin\alpha| > \sin 45^\circ \\ (\Delta y / \cos\alpha) \sin \alpha + x & , |\sin\alpha| < \sin 45^\circ, x > \text{WEST} \\ (\Delta y / \cos\alpha) \sin \alpha + x - \text{WEST} + 1, & |\sin\alpha| < \sin 45^\circ, x < \text{WEST} \end{cases}$$

$$\text{ROW } (y\text{-axis}) = \begin{cases} y + \Delta y & , |\sin\alpha| < \sin 45^\circ \\ (\Delta x / \sin\alpha) \cos\alpha + y & , |\sin\alpha| > \sin 45^\circ \end{cases}$$

The final value of the row index has to be transformed to indicate which array on the map sheet is the correct one. Thus, the final row index is given by integer arithmetic.

$$\text{ARRAY} = (\text{ROW} - 1)/15$$

$$\text{ROW} = \text{ROW} - (\text{ARRAY}-1)(15)$$

The terrain data located at (ROW, COLUMN, ARRAY) is checked to determine if its elevation will block the LOS. If it does not mask the node, the indices are incremented to the next value to be evaluated. After all node-sensor combinations have been processed, the route development can begin.

4.4 Route Selection.

With the node points for a route and their visibility determined, the method for linking these nodes into a route can be finalized. Two other characteristics of a node need to be considered along with its visibility. The first is its elevation in relation to surrounding nodes and the second is the distance to these surrounding nodes.

To determine the area size that should be considered a neighborhood about a node, several military helicopter pilots were contacted to discuss terrain following or nap of the earth flying. These pilots unanimously report that a range of one kilometer is utilized to consider their next position. Even though major terrain features used for reference points can be seen several kilometers away, terrain following flights require a pilot to concentrate on the immediate area to avoid terrain impact. Therefore, one kilometer was selected as the rectilinear distance about a node to define a neighborhood.

Depicting the relationship of nodes in a neighborhood, Figure 4.4 contains the nodes surrounding nodes 13 and 17. These nodes are in the neighborhood of either 13 or 17. Table 4.2 lists these nodes, the coordinates, and the distance from the center (1 unit = 70 meters). The negative nodes are the high elevation centers and the positive nodes are the low elevation centers. As can be seen in Figure 4.4 and Table 4.1, five nodes are shared by nodes 13 and 17.

With this information, a value can be assigned to these neighborhood nodes based on their elevation and distance from the primary node. The higher elevation nodes would normally be avoided in favor of traveling to a low elevation node. A penalty for height is added to the exposure value of each node by the following factor.

$$ZP_j = \left(\frac{z_j - z_{\min}}{ZR} \right)$$

where ZP_j = the penalty assigned to node j ,

z_j = the elevation of node j ,

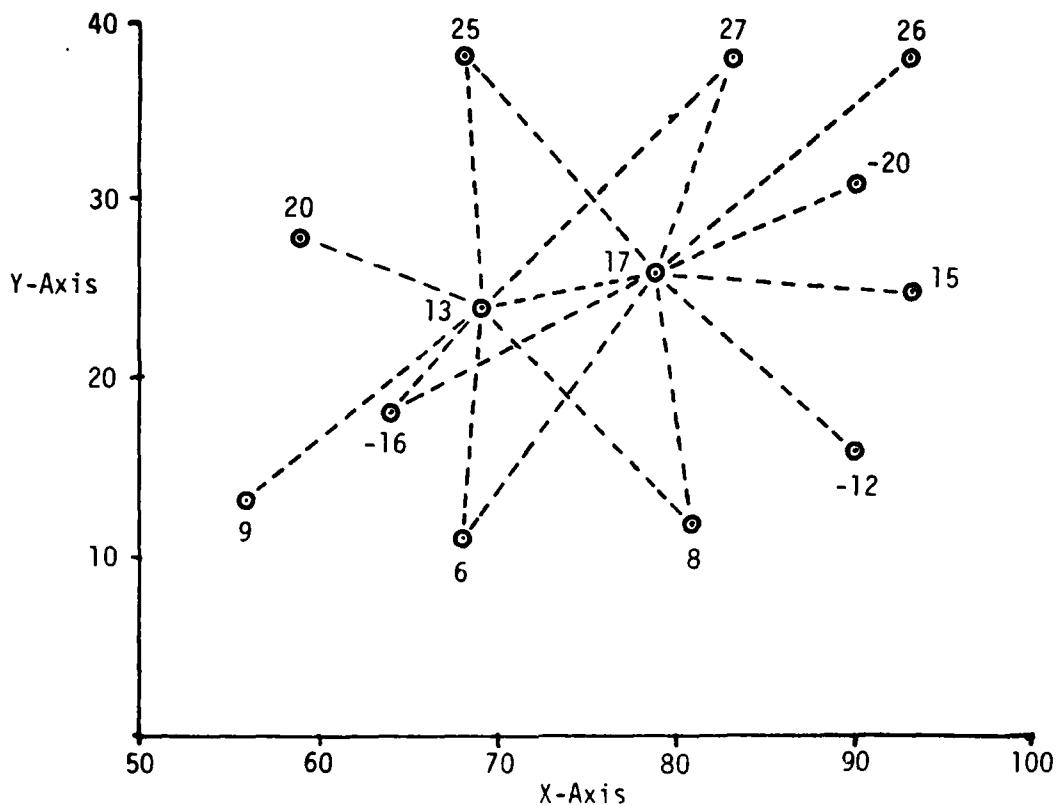


Figure 4.4 Node Linkage

Table 4.2 Node Links

Node 13 (113, 23, 300)					
No.	(X,Y,Z)	Distance	No.	(X,Y,Z)	Distance
6	(100, 10, 300)	13.038	20	(42, 27, 290)	10.770
8	(8, 10, 300)	16.971	25	(68, 8, 280)	14.036
9	(41, 12, 300)	17.029	27	(83, 38, 280)	19.799
17	(93, 25, 290)	10.198	-16	(64, 18, 290)	7.810

Node 17 (93, 26, 290)					
No.	(X,Y,Z)	Distance	No.	(X,Y,Z)	Distance
6	(100, 10, 300)	18.601	26	(93, 38, 280)	18.439
8	(81, 21, 290)	14.142	27	(83, 38, 280)	12.649
13	(113, 23, 300)	10.198	-12	(70, 16, 300)	14.866
15	(69, 24, 280)	14.036	-16	(64, 18, 290)	17.000
25	(68, 38, 280)	16.279	-20	(90, 31, 290)	12.083

Z_{min} = the minimum elevation of the neighborhood nodes,

ZR = the range between the maximum and minimum elevation in the neighborhood.

$$0 \leq ZP_j \leq 1$$

To account for distance from the central node, the penalty is associated with traveling short distances rather than long distances. The idea is to travel as far as possible in the neighborhood to reach a low, least exposed node. Thus the distance factor is given by:

$$DP_j = \left(1 - \frac{D_j - D_{min}}{DR} \right)$$

where DP_j = the penalty for a short distance between the central and neighborhood node,

D_j = the distance to the neighborhood node j ,

D_{min} = the minimum distance,

DR = the range between the maximum and minimum distance in the neighborhood.

$$0 \leq DP_j \leq 1$$

Adding these two factors to the exposure value results in the following function.

$$EP(ij) = \min_j \left[NS \cdot \left[\frac{R_{max} - \sum_{S=1}^{NS} R_{sj}}{\frac{NS}{R_{max}}} \right] + \left(\frac{Z_j - Z_{min}}{ZR} \right) + \left(1 - \frac{D_j - D_{min}}{DR} \right) \right]$$

The linkage (ij) is from node i to node j for which j is the minimum value within the neighborhood. Since each point and neighborhood is considered independently of any previous neighborhoods, this method is a dynamic programming approach to solving this problem.

The route objective is to provide a path to the terminal position. Therefore, some weighting should be given to those nodes which lie in the general direction of travel. To implement this idea, the vector-heading from the current position to the terminal node is found. The nodes which lie within 90° of either side of this heading have a weight of 1. Those nodes greater than 90° are located behind the current position and have a weight of 2. The exposure penalty of a neighborhood node is multiplied by this weight to give preference to those nodes which are ahead of the current position. If a position behind the current one has a very low exposure penalty it can still be selected, but the route procedure will reorient to the terminal node and will favor the destination direction.

When the route model has reached a position within 1 km of the terminal node the weighting scheme is modified to be more selective. The angle of preference is reduced to 45° of the route heading and pertains to those nodes lying inside the 1 km range. The weighting schemes for the selection process are given in Figures 4.5 and 4.6.

In developing the model, it was found that these weighting schemes lack one vital criterion - radar avoidance. The first two weightings provide the model with decision logic which improves the performance considerably; however, if the minimum exposure point was located on the other side of a sensor, then the logic would still choose this same point even though the route would then be directly over the sensor. After some testing of the model, a radar avoidance scheme was added to the weighting preference.

Air defense radars usually will have an acquisition range greater than the engagement range of the weapon system (guns or missiles). An

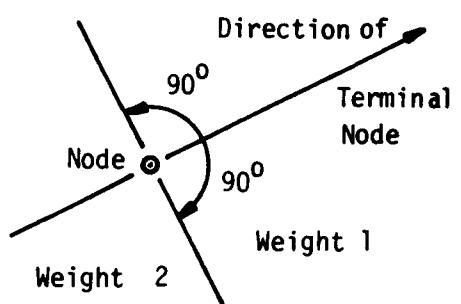


Figure 4.5 Weighting of Heading

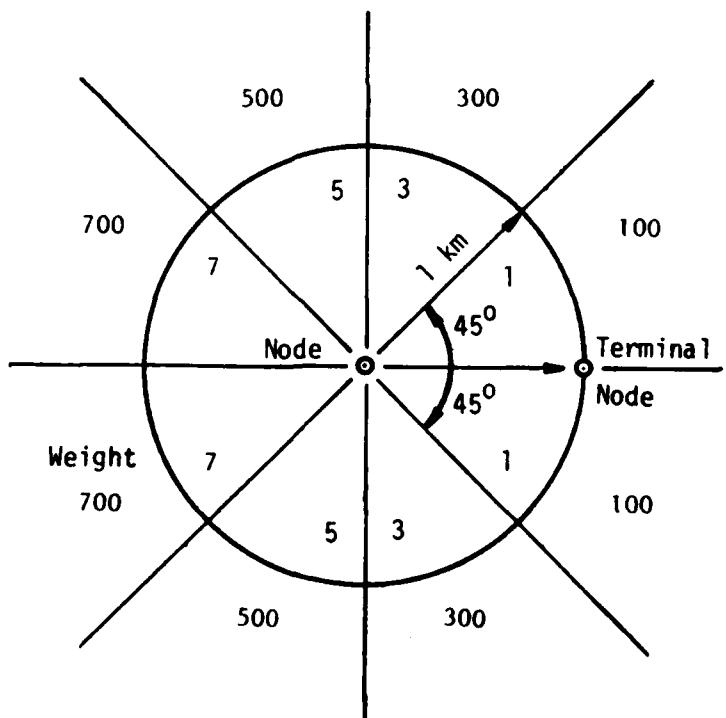


Figure 4.6 Weighting of Terminal Node

engagement boundary around the air defense site is assumed to be the weapon's kill radius. A vector from the current position to the sensor is calculated to give the azimuth and range to the sensor. A cone is used to form a high rejection area for nodes. The current position is the apex of the cone and the base is twice the kill radius, with the sensor at the base midpoint. A neighborhood node lying in this cone and ahead of the kill zone has a weight of 2. If it lies beyond this boundary the weight is 10. A node point which would cause the route to overfly or pass too close to the air defense site is thus avoided.

Figure 4.7 shows the relationship between the current node and the sensors, the terminal node and the new node. The angles shown in the figure are utilized in calculating the weighting values. Integer arithmetic allows a uniform weight to be assigned within any one area. The equations for calculating these weightings follows.

Angle of new node j from destination heading is:

$$ANT = \begin{cases} AN_j - AH & , -180^\circ \leq ANT \leq 180^\circ \\ AN_j - AH + 360^\circ & , ANT < -180^\circ \\ 360^\circ + AH - AN_j & , ANT > 180^\circ \end{cases}$$

Direction Weight is:

$$W_j = |ANT|/90^\circ + 1$$

Terminal Weight is:

$$RW_j = \begin{cases} 2|ANT|/45^\circ + 1 & , < 1 \text{ km} \\ (2|ANT|/45^\circ + 1) 100 & , > 1 \text{ km} \end{cases}$$

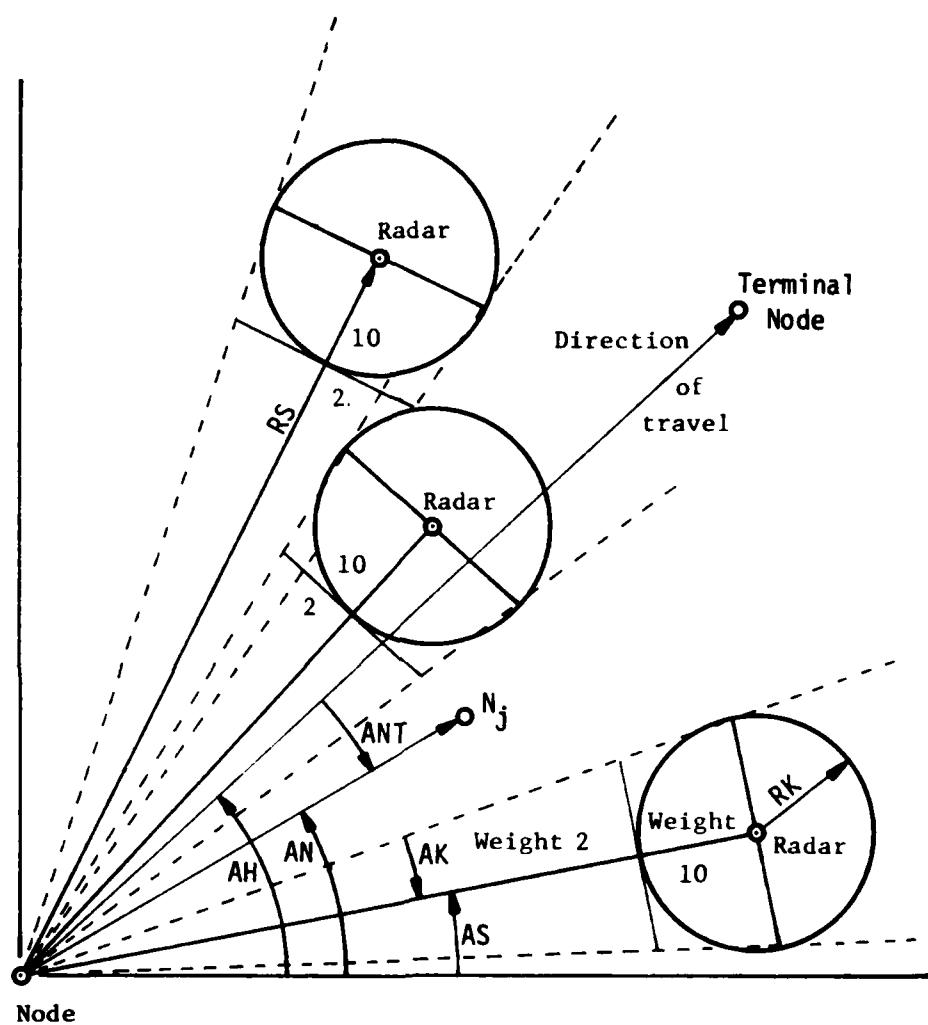


Figure 4.7 Radar Avoidance Weighting

Radar Avoidance Weight is:

$$AW_j = \begin{cases} 0, & AS - AN_j > AK \\ 2, & RN_j > RS - RK, AS - AN_j < AK \\ 10, & RN_j < RS - RK, AS - AN_j < AK \end{cases}$$

Where the variables in the equations and Figure 4.7 are:

- AN_j = the angle from the x-axis to the new node j,
- AH = the angle from the x-axis to the terminal node,
- ANT = the angle between the new node and the terminal node,
- AS = the angle to the sensor from the x-axis,
- AK = the angle to each side of the sensor heading which would be within the kill radius,
- RS = the range to the sensor from the current route node,
- RK = the kill radius of the weapon system,
- RN_j = the distance to the new node j,

The final exposure penalty for a node is defined by:

$$N_k = \min_j (W_j + RW_j + AW_j) \cdot EP(ij)$$

- Where N_k = the next node selected for the route,
- W_j = the weight of node j based on its angle heading,
- RW_j = the weight of node j based on its range to terminal node,
- AW_j = the weight of node j based on whether or not it lies in the radar avoidance cone.

4.5 Route Refinement

A review of the resulting routes as developed by the model indicates a need for route refinement; therefore, it is necessary for the route selection logic to evaluate whether or not route nodes are

adjacent to each other. In an attempt to avoid air defense sites, the route may double back on itself. Thus, the route must be refined by determining if each node j ahead of the current position i is the closest one. If, for example, the ninth route node ahead of the current one is the closest position, then that node becomes the next node to link with node i . Node i is linked to node j by the following relation.

$$L(ij) = \min_j [(x_j - x_i)^2 + (y_j - y_i)^2]^{1/2}$$

$$j = i + 1, \dots, n$$

where $L(ij)$ = the link between i and j ,

(x_i, y_i) = the current node position,

(x_j, y_j) = the next node position.

With this refinement to the model route logic, a shorter more direct route to the destination can be found. With the model development complete, an example will be given in the next chapter.

CHAPTER V

ROUTE SELECTION EXAMPLE

5.1 Introduction

The model is now utilized in selecting a route. The example described in this chapter is a portion of a route found by the model. Additional route problems that were solved by the model are contained in Appendix A. The general computer outline of the model and each subroutine is given in Appendix B. In addition the model software is commented throughout for ease in understanding the logic.

The area of analysis is 10 by 10 km. This size area is large enough to exercise the model yet small enough to run in 30 CPU seconds (6.5 seconds compile, 23.04 execution). The actual terrain is rolling hills with an elevation range from 270 to 400 meters. Within this area, 3 sensors are located to provide radar coverage.

Two positions were arbitrarily selected on opposite sides of the area as an initial and terminal node. These two positions are situated such that the three sensors are between these points. Any route found will have to consider node positions that lie near the sensors since they act as a barrier to be crossed.

5.2 Elevation Nodes

The initial part of the model provides the clustering of terrain data into high and low elevation groups. Within each group a center is found that becomes a node point for selection. The example clustering results were 106 low elevation nodes and 94 high elevation nodes.

Within the low elevation group, the initial and terminal nodes are inserted so that when the nodes are ordered by rows they will be in sequence. The first node is also the initial node. The terminal node is number 86. All high nodes are indicated by a minus sign.

5.3 Line of Sight Calculations

The amount of calculation required in identifying the nodes is minimal and consists mostly of comparisons and list searching. The first portion requiring any degree of computation is the LOS calculation in subroutine RADIAL.

For these calculations low elevation node 10 and high elevation node -11 were selected as examples for determining LOS. Two sensors will be used, as the calculations for more combinations are the same. The coordinates of the two nodes and sensors are given in Table 5.1.

Table 5.1 Node-Sensor Coordinates

Node (N_i) (X, Y, Z)	Sensor (R) (X, Y, Z)
10 (29, 14, 310)	1 (68, 70, 300)
-11 (12, 16, 330)	2 (47, 99, 310)

The first step performed by the model is to determine if the node or sensor is the western most point. Comparing X values in Table 5.1 indicates that both nodes are to the West of sensor 1. Node 10 will be analyzed first.

Table 5.2 gives the initial values for the variables used in this example. The horizontal scale is one unit equals 70 meters and the vertical values are in meters.

Table 5.2 Parameter Values

Map Sheet	2
EAST	30
WEST	16
SOUTH	1
NORTH	150
Earth Curvature (RE) (radar 4/3)	8490200.0 meters
Vehicle Height (V) (Aircraft)	10.0 meters
Sensor Height (S)	3.0 meters
GRID	70.0 meters

The first value needed is the horizontal distance between the node and the sensor.

$$d = [(x_2 - x_1)^2 + (y_2 - y_1)^2]^{\frac{1}{2}}$$

$$d = [(68 - 29)^2 + (70 - 14)^2]^{\frac{1}{2}}$$

$$d = 68.242$$

The azimuth angle cosine and sine are:

$$\cos \alpha = (y_2 - y_1) / d$$

$$\cos \alpha = (70 - 14) / 68.242$$

$$= 0.821$$

$$\sin \alpha = (x_2 - x_1) / d$$

$$\sin \alpha = (68 - 29) / 68.242$$

$$= 0.571$$

The tangent between these two points will determine whether the eastern point lies above or below the horizontal as measured from the western point. When calculating the tangent, the height of the vehicle and sensor are added to the appropriate point. In addition, the earth curvature for the radar beam atmospheric refraction is accounted for by the following relation [16].

$$\begin{aligned}
 \text{Ref} &= 0.5 (d)(d)/(RE/\text{GRID}) \\
 \text{Ref} &= 0.5 (68.242)(68.242) / (8490200.0/70) \\
 &= 2328.5 / 121288.57 \\
 &= 0.0192
 \end{aligned}$$

The tangent is:

$$\begin{aligned}
 \tan \beta &= ((z_R + S) - (z_{N_i} + V) - \text{REF}) / (d)(\text{GRID}) \\
 \tan \beta &= (303 - 320 - 0.0192) / (68.242)(70) \\
 &= -0.0036
 \end{aligned}$$

The absolute value of $\sin \alpha$ is compared to the sine of 45° . Since $0.571 < \sin 45^\circ$, then the direction is either north or south. The cosine is a positive 0.821 which indicates a north heading. When the cosine is negative, a south heading is indicated. The y position is found for the north or south direction by incrementing y by one plus any west boundary offset. In this example the Left Comp y is zero. The integer value of y is used for the data base row index and is found by integer arithmetic.

$$\begin{aligned}
 \text{ROW} &= y + \Delta y \\
 &= 14 + 1 = 15 \\
 \text{ARRAY} &= (\text{ROW} - 1)/15 + 1 \\
 &= (15 - 1)/15 + 1 = 1.93 = 1 \\
 \text{ROW} &= \text{ROW} - (\text{ARRAY} - 1) (15) \\
 &= 15 - (1 - 1) (15) = 15
 \end{aligned}$$

The column position can be found by the following.

$$\begin{aligned}
 \text{COL} &= (\Delta y / \cos \alpha) \sin \alpha + x - \text{WEST} + 1 \\
 &= (1/0.821) (0.571) + 29.0 - 16 + 1 \\
 &= 14.70 = 14
 \end{aligned}$$

The position of the first point to be extracted from the data base is located at (ROW, COL, ARRAY) = (15, 14, 1) of the second map sheet.

Now that the elevation of 308 has been found at this point a tangent is calculated to determine if this new point masks node 10 from sensor 1.

The distance to the new point, d' , is given by:

$$\begin{aligned} d' &= \Delta y / \cos \\ &= 1 / 0.821 = 1.22 \\ \text{Ref}' &= 0.5 (1.22)(1.22) / (8490200.0 / 70) \\ &= 0.5 (1.22)(1.22) / 121288.57 \\ &= 0.000006 \end{aligned}$$

Tangent α for the new point is calculated by:

$$\tan \alpha = (Z_n - (Z_i + V) - \text{Ref}') / (d')(\text{GRID})$$

where Z_n = the elevation of the new point.

$$\begin{aligned} \tan \alpha &= (308 - 320 - 0.000006) / (1.22)(70) \\ &= -0.14 \end{aligned}$$

Since $\tan \alpha < \tan \beta$, this new point does not mask the node (-0.14 < -.0036). The value of y is incremented to find the next grid point to be extracted from the data base.

$$\begin{aligned} y &= 2 \\ \text{ROW} &= 14 + 2 = 16 \\ \text{ARRAY} &= (16 - 1) / 15 + 1 = 2 \\ \text{ROW} &= 16 - (2 - 1) (15) = 1 \\ \text{COL} &= (2 / 0.821) (0.571) + 29.0 - 16 + 1 \\ &= 15.39 = 15 \end{aligned}$$

The second point from the data base is located in position (1, 15, 2) ($Z = 304$). Since the column is equal to 15, the eastern edge of the map sheet has been reached. In this case this second point does not mask the node, but any further calculations have to wait until the third map sheet is read into core storage.

The second node, number -11, is located on map sheet 1. Since this example began on map sheet 2, then the procedure for starting on the second map sheet, where the first map sheet processing stopped, will be shown. The basic calculations of sine, cosine, etc. are similar and are given below:

$$\begin{aligned} d &= [(68 - 12)^2 + (70 - 16)^2]^{\frac{1}{2}} \\ &= 77.795 \end{aligned}$$

$$\begin{aligned} \cos \alpha &= (70 - 16)/77.795 \\ &= 0.694 \end{aligned}$$

$$\begin{aligned} \sin \alpha &= (68 - 12)/77.795 \\ &= 0.720 \end{aligned}$$

$$\begin{aligned} \text{Ref} &= 0.5 (77.795)(77.795)/(121288.57) \\ &= 0.0249 \end{aligned}$$

$$\begin{aligned} \tan \alpha &= (303 - 340 - 0.0249)/(77.795) (70) \\ &= -0.0068 \end{aligned}$$

In this case, $\sin \alpha > \sin 45^\circ$; thus the direction is east. For a easterly vector the value of x is incremented by one to find the next position, but the value of y is calculated. Since $x < \text{WEST}$, x and COL are set to 1. The row index of y is calculated by

$$\begin{aligned} \text{ROW} &= (\Delta x / \sin \alpha) \cos \alpha + y \\ &= ((16 - 12 + 1) / 0.720) 0.694 + 16 \\ &= 20.82 \end{aligned}$$

$$\begin{aligned}
 \text{ARRAY} &= (\text{ROW} - 1)/15 + 1 \\
 &= (20.82 - 1)/15 + 1 = 2 \\
 \text{ROW} &= \text{ROW} - (\text{ARRAY} - 1) (15) \\
 &= 20.82 - (1)(15) = 5
 \end{aligned}$$

The first position in the second map sheet for node -11 is (5, 1, 2).

The tangent of this new point is calculated the same as shown for node 10. The $\tan \alpha < \tan \beta$ in this case; therefore, the next position on the vector is found and checked for LOS.

The result of these computations is the number of sensors which can see this node. Having obtained this count on each node-sensor combination the exposure value for the node can be computed. For node 10 the count is 3, since all sensors can see this node. The R_{\max} value for the node-sensor combinations in this example was found to be 161.941. The sum of the distances to the three sensors is 252.589. The exposure value is:

$$\begin{aligned}
 \text{EP} &= \text{NS} \cdot \left[R_{\max} - \frac{\sum_{S=1}^{\text{NS}} R_{Sj}}{\text{NS}} \right] \\
 &= 3 \cdot \left[\frac{161.941 - \frac{252.589}{3}}{161.941} \right] \\
 &= 1.440
 \end{aligned}$$

5.4 Route Selection

For the route selection method, the initial point and the next to last point along a route were chosen as examples. The initial point is

also node 1 (7, 3, 270) and the terminal point is node 86 (87, 124, 310).

Starting at node 1, the route seeks the minimum exposure point in the neighborhood. The nodes surrounding node 1 are given in Table 5.3.

Table 5.3 Neighborhood Nodes

Node	(x, y, z)	Distance	Exposure Value
4	(3, 9, 300)	7.211	0.672
-6	(13, 4, 400)	6.083	1.122
-8	(17, 5, 400)	10.198	1.167
-11	(12, 16, 330)	13.928	1.310

The distance and height penalties are now added to the exposure value for these points. The height penalty is given as:

$$ZP_j = \frac{z_j - z_{\min}}{ZR}$$

$$ZP_4 = \frac{300 - 300}{100} = 0.0$$

$$ZP_{-6} = \frac{400 - 300}{100} = 1.0$$

$$ZP_{-8} = \frac{400 - 300}{100} = 1.0$$

$$ZP_{-11} = \frac{330 - 300}{100} = 0.3$$

The distance penalty is:

$$DP_j = 1.0 - \left(\frac{D_j - D_{\min}}{DR} \right)$$

$$DP_4 = 1.0 - \left(\frac{7.211 - 6.083}{7.845} \right)$$

$$= 1.0 - 0.144 = 0.856$$

$$\begin{aligned}
 DP_{-6} &= 1.0 - \left(\frac{6.083 - 6.083}{7.845} \right) \\
 &= 1.0 \\
 DP_{-8} &= 1.0 - \left(\frac{10.198 - 6.083}{7.845} \right) \\
 &= 1.0 - 0.525 = 0.475 \\
 DP_{-11} &= 1.0 - \left(\frac{13.928 - 6.083}{7.845} \right) \\
 &= 1.0 - 1.0 = 0.0
 \end{aligned}$$

The final penalties associated with these nodes are:

Node 4	1.528
Node -6	3.122
Node -8	2.642
Node -11	1.610

The direction weighting of these penalty values are determined by computing the azimuth of the terminal and neighborhood nodes. Table 5.4 gives the azimuth angle to the nodes, their weight and their final penalty value.

Table 5.4 Weighted Penalty Value

From	To	Angle x-axis	Angle from Heading	Weight	Penalty
1	86	56°	0°	-	-
1	4	123°	67°	1	1.528
1	-6	9°	-47°	1	3.122
1	-8	11°	-45°	1	2.642
1	-11	68°	12°	2	3.220

To compute the Table 5.4 entries for node 4 the following values are found using integer arithmetic.

$$\begin{aligned} \text{x-axis } AN_4 &= \text{ARCTAN } (Y/X) \\ &= \text{ARCTAN } ((9-3)/(3-7)) \\ &= -56.31^\circ \end{aligned}$$

Since the angle is negative, it is subtracted from 180° .

$$\begin{aligned} AN_4 &= 180^\circ - 56.31^\circ = 123.69^\circ = 123^\circ \\ \text{ANT} &= 123^\circ - 56^\circ = 67^\circ \\ \text{Weight } W_j &= \text{ANT} / 90^\circ + 1 \\ &= 67^\circ/90^\circ + 1 \\ &= 0 + 1 = 1 \\ \text{Penalty EP}_{ij} &= (W_j) (EP_j) \\ &= (1)(1.528) = 1.528 \end{aligned}$$

Node -11 is the only one in Table 5.4 that utilized the radar avoidance weighting. Sensor 2 is almost collinear with nodes 1 and -11. For this example, the weapon system kill radius is 1.5 km or 21.43 in units of 70 meters. The calculations below would be made for all sensors and all nodes in the neighborhood, however, only node -11 is affected in this case.

Angle to sensor 2 is given by:

$$\begin{aligned} \text{x-axis } AN_{-11} &= \text{ARCTAN } (Y/X) \\ &= \text{ARCTAN } ((99 - 3)/(47 - 7)) \\ &= 67.38^\circ = 67^\circ \end{aligned}$$

Angle of 1/2 cone is given by:

$$\begin{aligned} RS &= [(99 - 3)^2 + (47 - 7)^2]^{1/2} \\ &= 104.00 \\ AK &= \text{ARCTAN } (21.43/104.00) \\ &= 11.64^\circ \end{aligned}$$

Angle between sensor 2 and node -11 is given by:

$$\begin{aligned} AS - AP &\text{ (from Table 5.4)} \\ -1^\circ &= 67^\circ - 68^\circ \\ -1^\circ &< 11.64^\circ \end{aligned}$$

Therefore, node -11 is in the cone of high rejection.

$$\begin{aligned} AW_j &= 2, \text{ distance node } -11 < \text{sensor 2} \\ &\quad (13.9 < 104.00) \end{aligned}$$

The next to last node along the route, number 78, utilizes the terminal weighting scheme. The values associated with node 78 are in Table 5.5. In this table the terminal node 86 has the smallest weighted exposure. The values in Table 5.5 are computed as shown previously except for the weight entry. The weight value for nodes 71 and 72 are found below.

For node 71:

$$\begin{aligned} RW_j &= 2 \text{ ANT}/45^\circ + 1, \quad (13.153)(70) < 1 \text{ km} \\ &= 2 (-179/45) + 1 \\ &= 2 (4) + 1 = 7 \end{aligned}$$

Table 5.5 Node 78

From	To	Distance	Exposure	Height	Penalty	Distance	Penalty	Angle X-axis	Heading	Weight	Penalty
78	71	13.153	2.438	0.0	0.423	-98°	-179°	7	2009		
78	72	15.000	2.306	0.0	0.000	-53°	-134°	500	115500		
78	79	11.180	2.234	0.0	0.874	10°	-71°	3	933		
78	86	13.153	0.730	0.5	0.423	81°	0°	1	163		
78	-75	10.630	1.576	1.0	1.000	138°	57°	3	1059		

For node 72:

$$\begin{aligned}
 RW_j &= (2 \text{ ANT}/45^\circ + 1) 100 , \quad (15.0)(70) > 1 \text{ km} \\
 &= (2 (-134/45) + 1) 100 \\
 &= (2 (2) + 1) 100 = 500
 \end{aligned}$$

5.5 Route Refinement

To provide an example of route refinement consider the following situation given in Table 5.6.

Table 5.6 Linkage

From Node (X, Y, Z)	To Node (X, Y, Z)	Distance
31 (11, 45, 280)	30 (23, 43, 280)	12.166
30 —	28 (8, 40, 280)	15.297
28 —	35 (21, 50, 280)	16.401
35 —	34 (11, 49, 280)	10.050
34 —	45 (1, 64, 300)	18.028

The linkage between these points can be seen in Figure 5.1.

From the figure, it is seen that node 34 is the closest node to node 31. The model determines this fact by comparing distances between nodes. The distance from node 31 to each of the nodes ahead of it is computed to the end of the route by the model; however, for this example, the process will stop at node 45. Table 5.7 gives the distance values for each of these nodes.

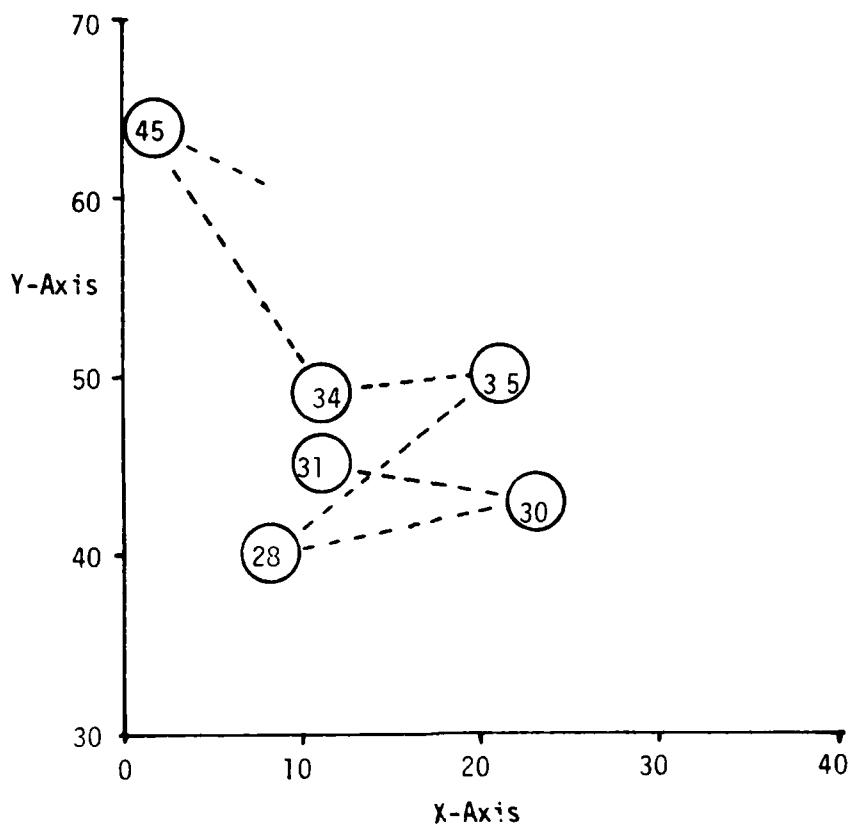


Figure 5.1. Linkage Example.

Table 5.7 Distance from Node 31

Node	Distance
30	12.166
28	5.831
35	11.180
34	4.000
45	21.471

The closest node to node 31 is node 34. In the refinement procedure, node 31 would be linked to node 34. Nodes 30, 28 and 35 would be eliminated from the route. The next node in the sequence, node 34, would now be compared with all nodes ahead of it for the closest node. The model continues to evaluate each new node on the route until the destination is reached. The results of this procedure become the refined route.

CHAPTER VI

MODEL RESULTS

6.1 Introduction

To evaluate the effect of sensor location on the route selection, two sets of sensor deployments were chosen along with two sets of beginning and end points. Since the test area was predominantly level terrain, a second small area was chosen of moderately rough terrain.

The results of the two small 10 by 10 km terrain areas are presented first, followed by the large 35 by 35 km area. To run the large terrain required increasing the dimensions of several primary arrays. The computer processing time for the large area increased by a factor of 10.

A plot of the route has proven to be the best analysis tool in evaluating the resulting routes. The tables provide the quantitative results; however, the route figures provide a visual comparison between routes that is discernible.

6.2 Small Area Analysis

The performance of this model was judged by varying sensor and route end points to provide different routes. Tables 6.1 and 6.2 provide the location of sensors and route end points utilized in the two small terrain areas. Each set of sensors was deployed against each route, resulting in four cases for each area as shown in Table 6.3.

Table 6.1 Sensor Locations

Area 1					
Set 1			Set 2		
Sensor	(X,Y,Z)		Sensor	(X,Y,Z)	
1	(68, 70, 300)		1	(115, 116, 330)	
2	(36, 119, 350)		2	(90, 84, 340)	
3	(47, 99, 310)		3	(103, 45, 320)	

Area 2					
Set 1			Set 2		
Sensor	(X,Y,Z)		Sensor	(X,Y,Z)	
1	(28, 114, 330)		1	(78, 57, 350)	
2	(61, 90, 380)		2	(85, 42, 340)	
3	(78, 71, 350)		3	(100, 17, 320)	

Table 6.2 Initial and Final Route Points

Area 1					
Route	Node	From (X,Y,Z)	Node	To (X,Y,Z)	
1	1	(7, 3, 270)	86	(87, 124, 310)	
2	31	(11, 45, 280)	96	(135, 135, 360)	

Area 2					
Route	Node	From (X,Y,Z)	Node	To (X,Y,Z)	
1	3	(26, 4, 350)	81	(118, 111, 310)	
2	35	(11, 50, 300)	84	(128, 114, 320)	

Table 6.3 Route Cases

Case	Area	Route	Sensor Set
1	1	1	1
2	1	2	1
3	1	1	2
4	1	2	2
5	2	1	1
6	2	2	1
7	2	1	2
8	2	2	2

The initial point and the destination point are placed in the low elevation array with their node number within that array given in Table 6.2. Except for the initial and destination nodes, the set of high and low elevation nodes for an area is determined solely on elevation. They remain constant for all scenarios. Table 6.4 indicates 106 low elevation nodes and Table 6.5 indicates 94 high elevation nodes. Tables 6.6 and 6.7 give the exposure values of these nodes for the first set of sensors. These values will change with each sensor deployment and the number of sensors. The first entry in Table 6.6 corresponds to the first entry in Table 6.4 with the other values corresponding in the order given. Likewise, Table 6.7 entries correspond to the entries in Table 6.5 in the same manner. The data contained in these four tables provide the basic information required for the route selection.

The results of the route selection process for the first case is given in Table 6.8. The node linkage is from node i to node j with the

Table 6.4. Low Elevation Node Points

X-COORDINATE	7	138	128	3	112	100	68	81	41	56
Y-COORDINATE	3	8	8	9	10	10	11	12	12	13
Z-COORDINATE	270	300	300	300	300	300	290	290	300	290
X-COORDINATE	29	128	113	6	69	141	93	79	25	42
Y-COORDINATE	14	22	23	24	24	25	25	26	27	27
Z-COORDINATE	310	300	300	300	280	300	250	280	300	290
X-COORDINATE	59	121	146	112	68	93	83	53	8	39
Y-COORDINATE	26	31	34	35	38	38	38	38	40	42
Z-COORDINATE	260	300	300	300	280	280	260	260	280	280
X-COORDINATE	23	37	55	11	21	68	83	93	112	145
Y-COORDINATE	43	47	49	45	50	51	52	54	55	59
Z-COORDINATE	280	280	280	280	260	280	260	280	300	300
X-COORDINATE	127	84	94	67	1	25	56	128	113	145
Y-COORDINATE	59	63	63	62	64	64	65	66	66	68
Z-COORDINATE	310	290	290	290	300	300	250	200	360	300
X-COORDINATE	36	94	144	134	8	30	42	68	53	83
Y-COORDINATE	68	76	76	76	77	77	81	83	83	83
Z-COORDINATE	300	300	300	310	340	310	300	300	300	300
X-COORDINATE	108	92	150	30	44	111	55	65	124	8
Y-COORDINATE	89	85	91	91	93	94	95	97	58	58
Z-COORDINATE	330	300	360	350	310	350	300	300	350	350
X-COORDINATE	53	94	150	106	45	56	73	85	56	106
Y-COORDINATE	98	99	105	105	106	106	107	111	113	114
Z-COORDINATE	300	300	360	330	320	320	300	300	300	310
X-COORDINATE	7	145	122	16	16	97	11	113	57	123
Y-COORDINATE	117	119	119	120	122	124	127	128	128	129
Z-COORDINATE	300	340	330	360	300	310	300	330	330	330
X-COORDINATE	86	91	147	75	32	23	14	25	83	38
Y-COORDINATE	129	129	132	135	125	135	127	141	143	144
Z-COORDINATE	300	300	330	310	310	300	300	300	300	360
X-COORDINATE	96	53	146	65	106	124				
Y-COORDINATE	145	146	146	147	145	150				
Z-COORDINATE	300	300	320	300	300	320				

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Table 6.5. High Elevation Node Points

X-COORDINATE	32	46	67	121	149	13	115	17	94	75
Y-COORDINATE	3	2	3	3	3	4	5	5	5	6
Z-COORDINATE	330	310	300	310	330	400	310	400	310	300
X-COORDINATE	12	90	31	67	18	64	147	100	127	93
Y-COORDINATE	16	16	17	18	18	18	20	24	30	31
Z-COORDINATE	330	300	310	300	330	290	310	300	320	290
X-COORDINATE	11	47	21	35	128	115	141	105	105	116
Y-COORDINATE	32	32	35	37	39	42	42	45	46	49
Z-COORDINATE	290	290	300	290	320	330	330	320	320	330
X-COORDINATE	140	129	38	27	68	48	62	10	83	51
Y-COORDINATE	53	54	56	57	55	59	59	60	70	70
Z-COORDINATE	330	330	300	300	250	300	250	310	300	300
X-COORDINATE	68	8	32	17	113	122	104	139	90	105
Y-COORDINATE	71	72	74	74	75	75	75	75	80	80
Z-COORDINATE	300	330	310	330	340	330	330	310	310	340
X-COORDINATE	115	8	23	17	125	97	142	135	22	104
Y-COORDINATE	63	67	68	69	60	90	90	97	99	99
Z-COORDINATE	350	350	320	350	370	310	390	400	350	330
X-COORDINATE	142	115	47	32	61	105	136	9	142	116
Y-COORDINATE	99	101	104	104	105	106	107	107	108	109
Z-COORDINATE	400	350	330	350	320	330	350	350	400	350
X-COORDINATE	25	35	65	49	77	135	140	77	27	67
Y-COORDINATE	113	115	116	116	118	122	124	127	127	128
Z-COORDINATE	350	350	330	340	320	350	350	320	350	330
X-COORDINATE	103	48	91	2	104	94	127	49	64	77
Y-COORDINATE	129	129	130	131	137	137	137	137	138	138
Z-COORDINATE	330	350	350	380	320	340	340	340	330	310
X-COORDINATE	3	140	115	17						
Y-COORDINATE	143	143	144	142						
Z-COORDINATE	380	350	330	340						

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Table 6.6. Exposure Values for Low Elevation Nodes

0.900	.697	.825	.672	1.039	1.160	1.381	1.359	1.405	1.440
1.392	.526	1.217	1.360	1.612	1.000	1.465	1.595	1.587	1.675
1.711	0.000	0.000	1.390	1.866	1.666	1.766	1.892	0.000	1.275
0.600	.762	1.400	0.000	0.000	2.095	1.984	1.263	1.624	.520
1.404	2.118	1.970	2.307	0.000	1.477	2.347	.629	1.688	.537
2.300	2.066	0.000	0.000	1.315	1.590	1.710	2.459	2.526	2.268
1.263	2.134	0.000	1.555	1.753	1.811	2.582	2.452	1.579	1.375
2.264	2.050	0.000	1.874	2.594	2.548	1.601	1.480	1.596	1.832
0.000	0.000	0.950	0.000	0.000	0.647	0.000	1.623	1.494	1.457
.619	.609	.510	0.000	0.000	0.000	0.000	0.000	0.000	0.000
.506	0.009	.301	0.000	.530	.424				

Table 6.7. Exposure Values for High Elevation Nodes

1.214	1.252	1.149	.636	.486	1.122	.532	1.167	1.129	1.265
1.310	1.345	1.050	1.526	1.390	1.520	0.000	1.380	.214	1.589
1.107	1.777	1.605	1.615	.625	1.433	1.034	1.610	1.622	1.494
1.142	1.332	2.135	2.060	2.213	2.234	2.055	.637	2.203	2.397
2.421	.629	2.317	.604	1.739	.665	1.494	0.000	2.149	1.697
1.731	1.352	2.495	1.445	1.145	2.574	1.249	1.384	1.513	1.925
1.256	1.732	2.667	1.598	2.509	1.687	1.366	.818	1.239	1.690
1.547	1.630	1.535	2.505	1.445	.827	.762	1.346	1.492	1.442
1.766	1.519	1.222	1.096	.878	1.179	.863	.791	0.000	
1.144		.967	.786						

Table 6.8. NODE LINKAGE FOR ROUTE

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
1	490	7210	4	153	210	7630
4	210	7630	-6	263	1190	7350
-8	1190	7350	11	164	2030	7980
11	2030	7980	9	207	2870	7840
9	2870	7840	10	145	3920	7910
10	3920	7910	15	184	4830	8680
15	4830	8680	27	177	5810	9660
27	5810	9660	26	266	6510	9660
26	6510	9660	-29	276	7350	10220
-29	7350	10220	35	247	7840	10520
39	7840	10920	49	242	7910	11620
49	7910	11620	48	152	9960	11620
48	8960	11620	-48	59	9730	12250
-46	9730	12250	53	262	10080	12320
53	10080	12320	63	72	10500	13370
63	10500	13370	73	27	10500	14350
72	10500	14350	82	67	10430	15330
82	10430	15330	93	96	10290	16240
93	10290	16240	103	124	10220	17220
103	10220	17220	13	154	6540	15330
13	8540	15330	98	228	7910	15960
18	7510	15960	-65	234	7280	16590
-65	7780	16590	-60	44	5790	16660
-60	5390	16660	66	97	6090	15680

Table 6.9. Node Linkage

NODE NO.	1	TOTAL LINKS	4
X,Y,Z COORDINATE	70	30	270
LINKED TO	4	-6	-8
EXPOSURE	152	311	263
WEIGHTED	152	312	264
NODE NO.	4	TOTAL LINKS	5
X,Y,Z COORDINATE	30	50	300
LINKED TO	14	-6	-11
EXPOSURE	172	311	257
WEIGHTED	146	312	256
NODE NO.	-2	TOTAL LINKS	6
X,Y,Z COORDINATE	170	50	400
LINKED TO	11	-6	-11
EXPOSURE	163	311	197
WEIGHTED	164	624	198
NODE NO.	11	TOTAL LINKS	6
X,Y,Z COORDINATE	250	140	310
LINKED TO	9	19	20
EXPOSURE	206	215	167
WEIGHTED	207	216	156
NODE NO.	9	TOTAL LINKS	5
X,Y,Z COORDINATE	410	120	300
LINKED TO	10	-14	-2
EXPOSURE	144	277	246
WEIGHTED	145	278	244
NODE NO.	10	TOTAL LINKS	7
X,Y,Z COORDINATE	560	130	290
LINKED TO	7	21	15
EXPOSURE	244	214	187
WEIGHTED	245	430	188
NODE NO.	15	TOTAL LINKS	7
X,Y,Z COORDINATE	650	240	280
LINKED TO	18	21	7
EXPOSURE	219	246	285
WEIGHTED	243	247	572
NODE NO.	27	TOTAL LINKS	7
X,Y,Z COORDINATE	830	360	280
LINKED TO	26	18	37
EXPOSURE	265	231	257
WEIGHTED	266	464	2580
NODE NO.	26	TOTAL LINKS	7
X,Y,Z COORDINATE	930	360	280
LINKED TO	17	37	18
EXPOSURE	216	219	159
WEIGHTED	434	420	320
NODE NO.	-29	TOTAL LINKS	7
X,Y,Z COORDINATE	1050	460	320
LINKED TO	59	24	38
EXPOSURE	246	218	161
WEIGHTED	247	430	324
NODE NO.	39	TOTAL LINKS	5
X,Y,Z COORDINATE	1120	560	300
LINKED TO	65	61	-30
EXPOSURE	241	172	346
WEIGHTED	242	346	694
NODE NO.	49	TOTAL LINKS	6
X,Y,Z COORDINATE	1130	660	300
LINKED TO	48	41	-45
EXPOSURE	78	171	371
WEIGHTED	158	349	372

Table 6.9. (cont'd.)

NODE NO.	46	TOTAL LINKS	8
X,Y,Z COORDINATE	126°	66°	300
LINKED TO	-42	54	50
EXPOSURE	264	81	77
WEIGHTED	533	52	156
NODE NO.	-49	TOTAL LINKS	4
X,Y,Z COORDINATE	139°	75°	310
LINKED TO	-53	54	50
EXPOSURE	150	114	125
WEIGHTED	252	230	252
NODE NO.	53	TOTAL LINKS	5
X,Y,Z COORDINATE	144°	76°	300
LINKED TO	-50	54	63
EXPOSURE	153	98	71
WEIGHTED	308	69	72
NODE NO.	63	TOTAL LINKS	5
X,Y,Z COORDINATE	150°	91°	360
LINKED TO	-73	-57	-61
EXPOSURE	26	299	283
WEIGHTED	27	630	284
NODE NO.	73	TOTAL LINKS	7
X,Y,Z COORDINATE	150°	105°	360
LINKED TO	-82	-65	-61
EXPOSURE	56	322	312
WEIGHTED	-57	323	313
NODE NO.	82	TOTAL LINKS	5
X,Y,Z COORDINATE	145°	115°	340
LINKED TO	-93	-77	-65
EXPOSURE	95	214	288
WEIGHTED	96	215	289
NODE NO.	93	TOTAL LINKS	4
X,Y,Z COORDINATE	147°	132°	330
LINKED TO	-103	-77	-92
EXPOSURE	61	273	154
WEIGHTED	124	548	155
NODE NO.	103	TOTAL LINKS	6
X,Y,Z COORDINATE	145°	146°	320
LINKED TO	-90	83	-92
EXPOSURE	171	98	170
WEIGHTED	144	198	342
NODE NO.	63	TOTAL LINKS	5
X,Y,Z COORDINATE	122°	114°	330
LINKED TO	-90	88	-70
EXPOSURE	245	227	280
WEIGHTED	246	228	261
NODE NO.	86	TOTAL LINKS	5
X,Y,Z COORDINATE	115°	126°	330
LINKED TO	-90	80	-81
EXPOSURE	310	198	341
WEIGHTED	622	398	342
NODE NO.	-85	TOTAL LINKS	12
X,Y,Z COORDINATE	104°	137°	330
LINKED TO	-91	90	66
LINKED TO	-70	-75	
EXPOSURE	115	254	130
EXPOSURE	-77	193	
WEIGHTED	232	510	262
WEIGHTED	278	368	
NODE NO.	-90	TOTAL LINKS	5
X,Y,Z COORDINATE	77°	138°	310
LINKED TO	-91	66	-78
EXPOSURE	154	96	303
WEIGHTED	135	97	608

corresponding penalty associated with this pairing. The easting and northing values are the number of meters from the southwest corner of the area. This corner is the standard position for reference on a map. Knowing the southwest corner of the actual map area being analyzed, the nodes can be positioned on the map by finding the point X meters easting and Y meters northing from the southwest corner. Table 6.9 contains the neighborhood nodes for each node along the route. Three data items are provided: The nodes are listed on the third line, the unweighted exposure value pertaining to that node is listed on the fourth line, and the final weighted penalty for the node is given on the fifth line.

Figure 6.1 shows the position of the sensors and the resulting route for the first case. The route avoids the air defense sensors by traveling east before turning north. The destination point is approached from an easterly direction.

Figures 6.2 through 6.8 are the resulting routes for the cases listed in Table 6.3. In each Figure the location of the sensors are shown. The terrain in Figures 6.1 through 6.4 is flat to moderately hilly. There is a valley that proceeds from the southwest to the northeast through the center of this terrain. The rough terrain is located to the southeast and east. A large flat-top hill is located in the northwest.

The terrain in the second area is rougher (Case 5 through 8). There is a prominent ridge running from the southeast to the center of the area. There are valleys on each side of this ridgeline that join in the northwest. In Figures 6.5 and 6.7, the route selection was difficult with the sensors located in the northern and central areas. When the sensors were located on top of the ridge and to the south,

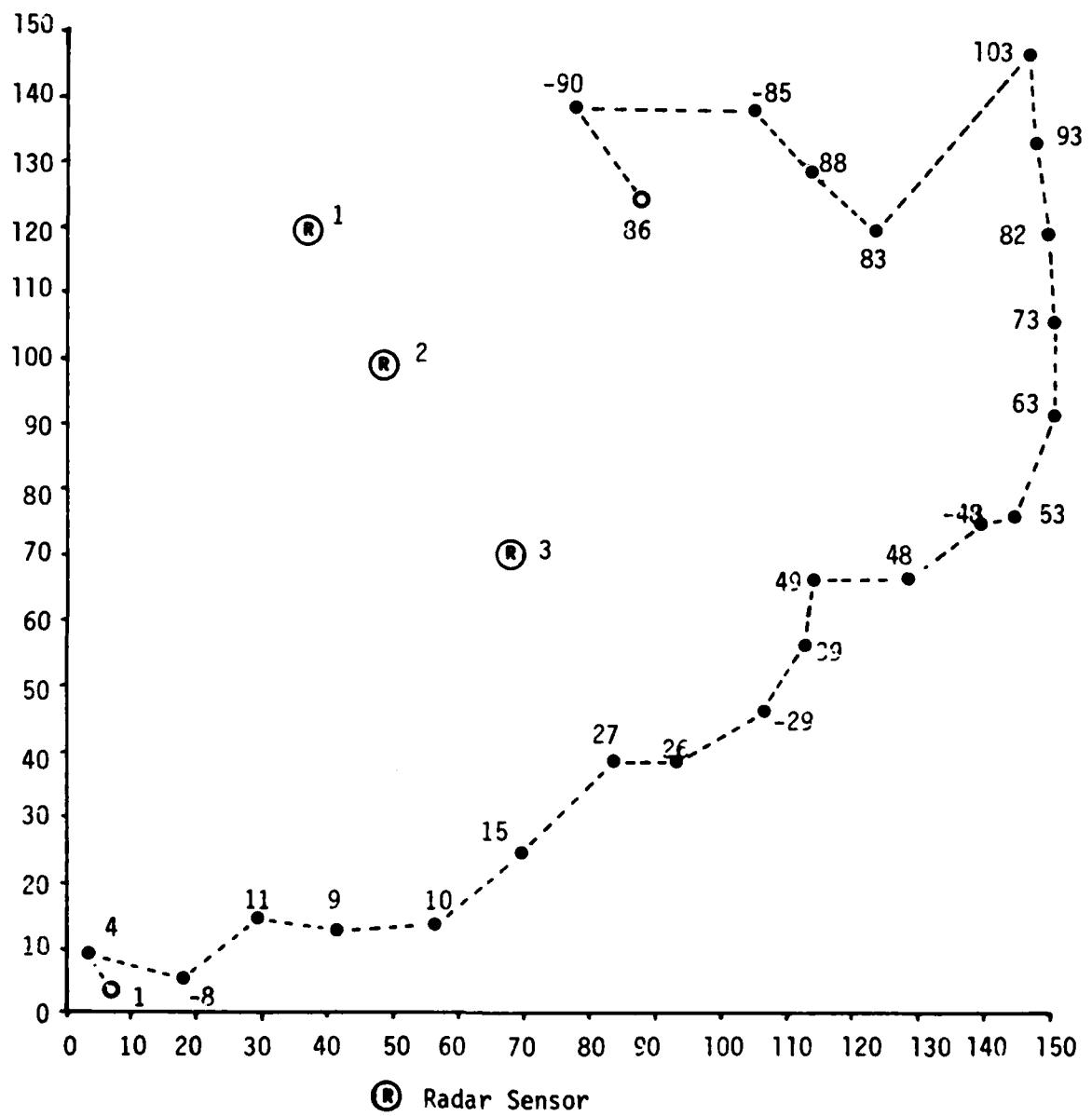


Figure 6.1. Case 1 - A1, R1, S1.

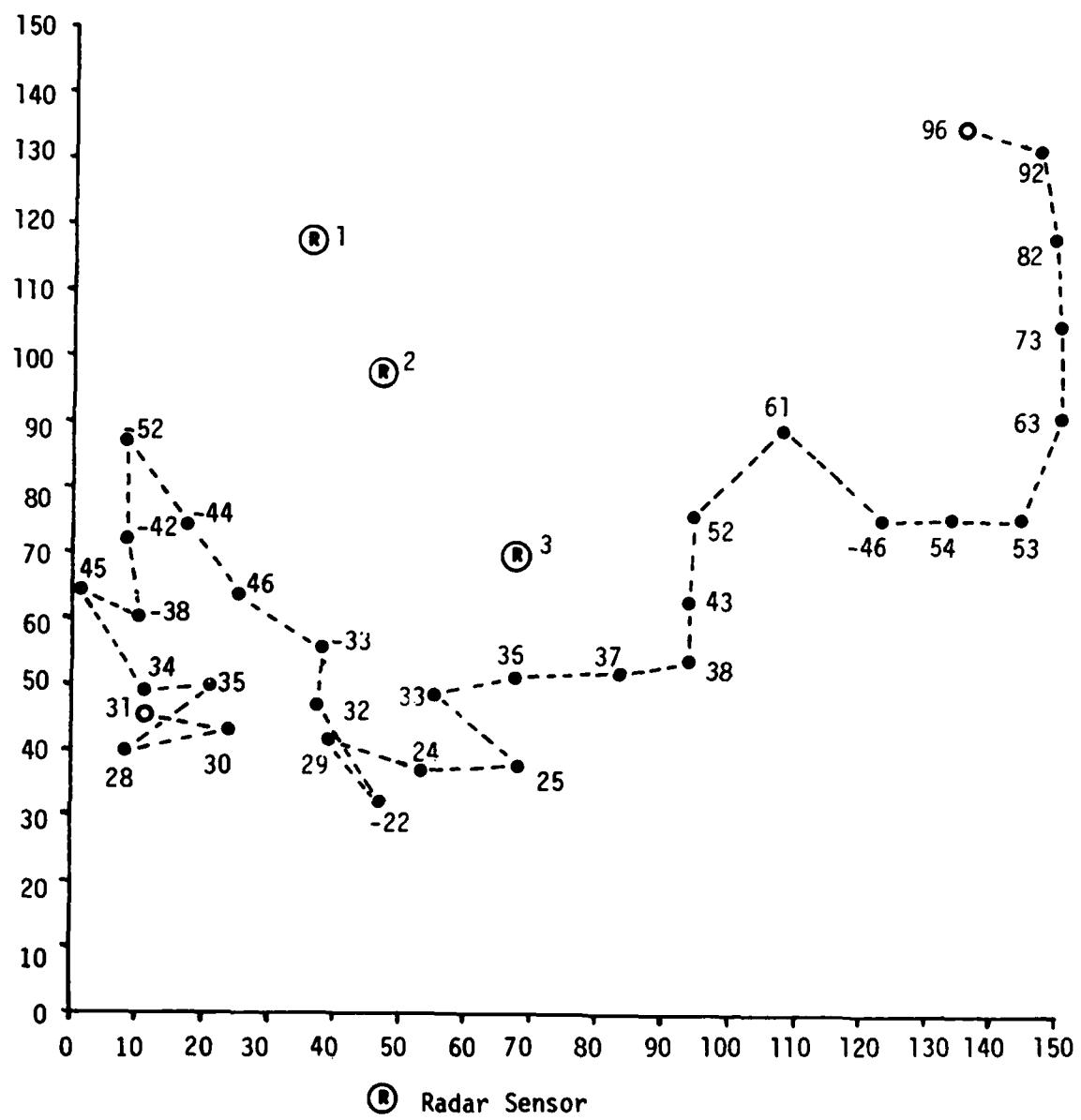


Figure 6.2. Case 2 - A1, R2, S1.

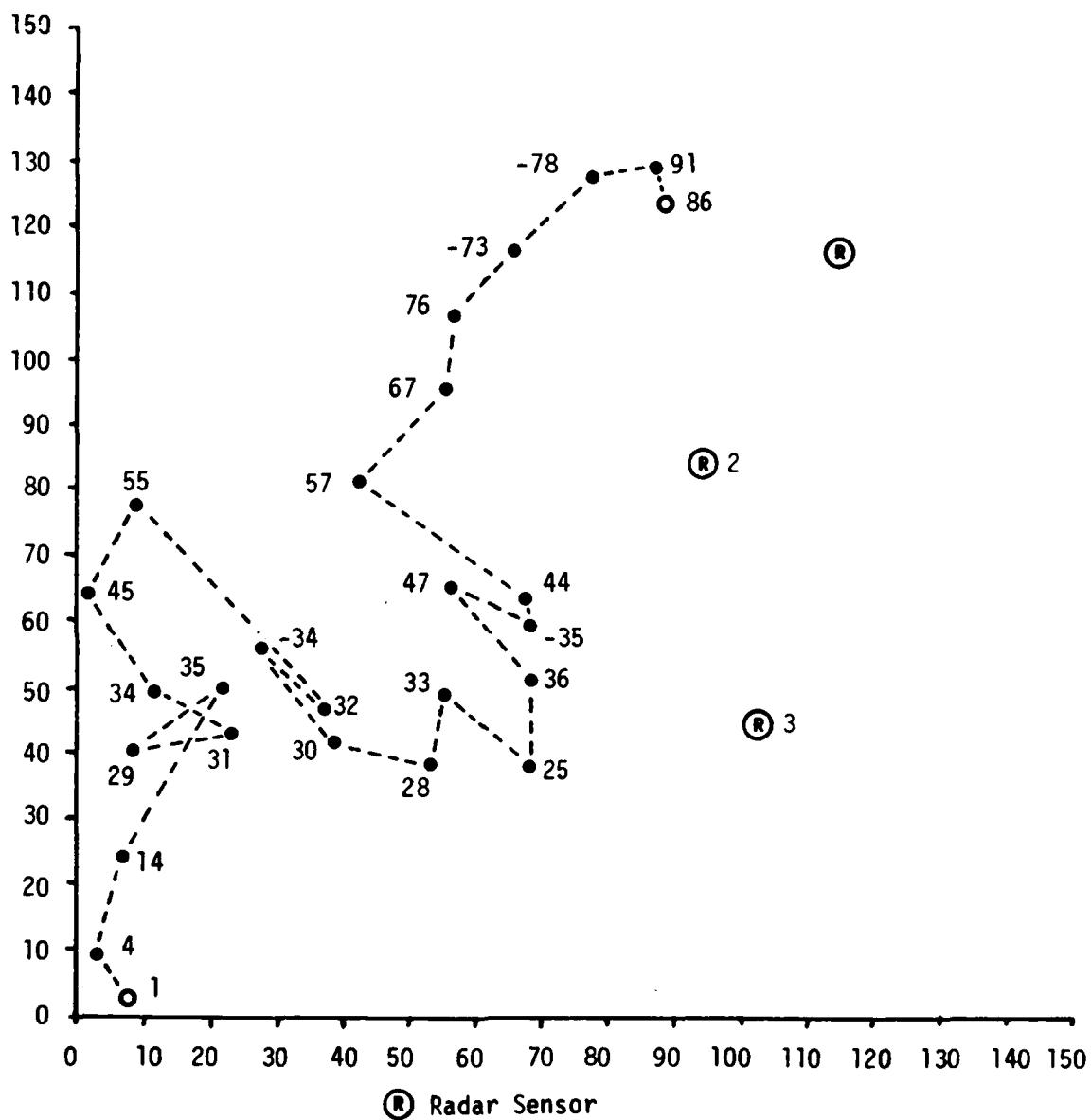


Figure 6.3. Case 3 - A1, R1, S2.

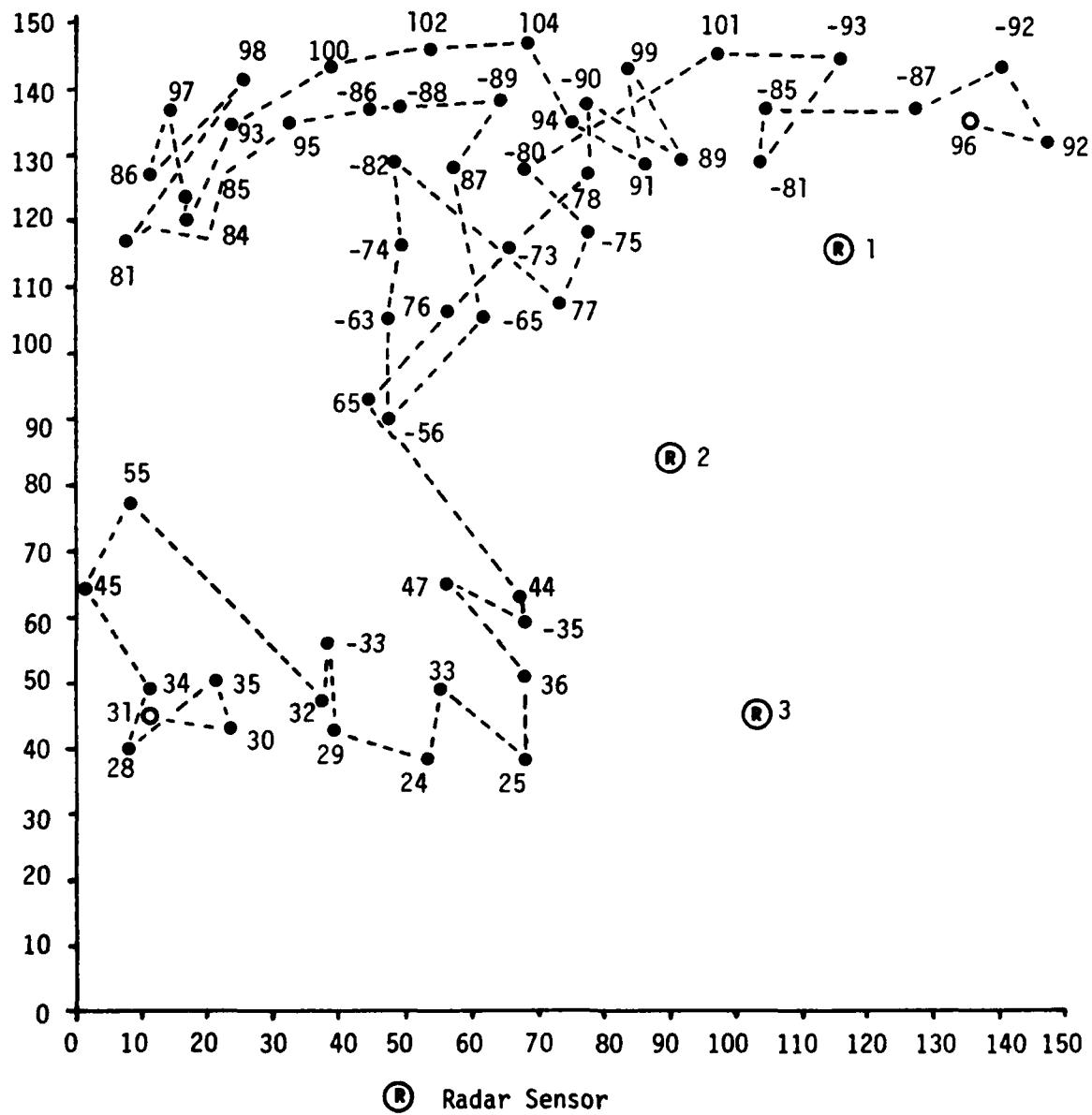


Figure 6.4. Case 4 - A1, R2, S2.

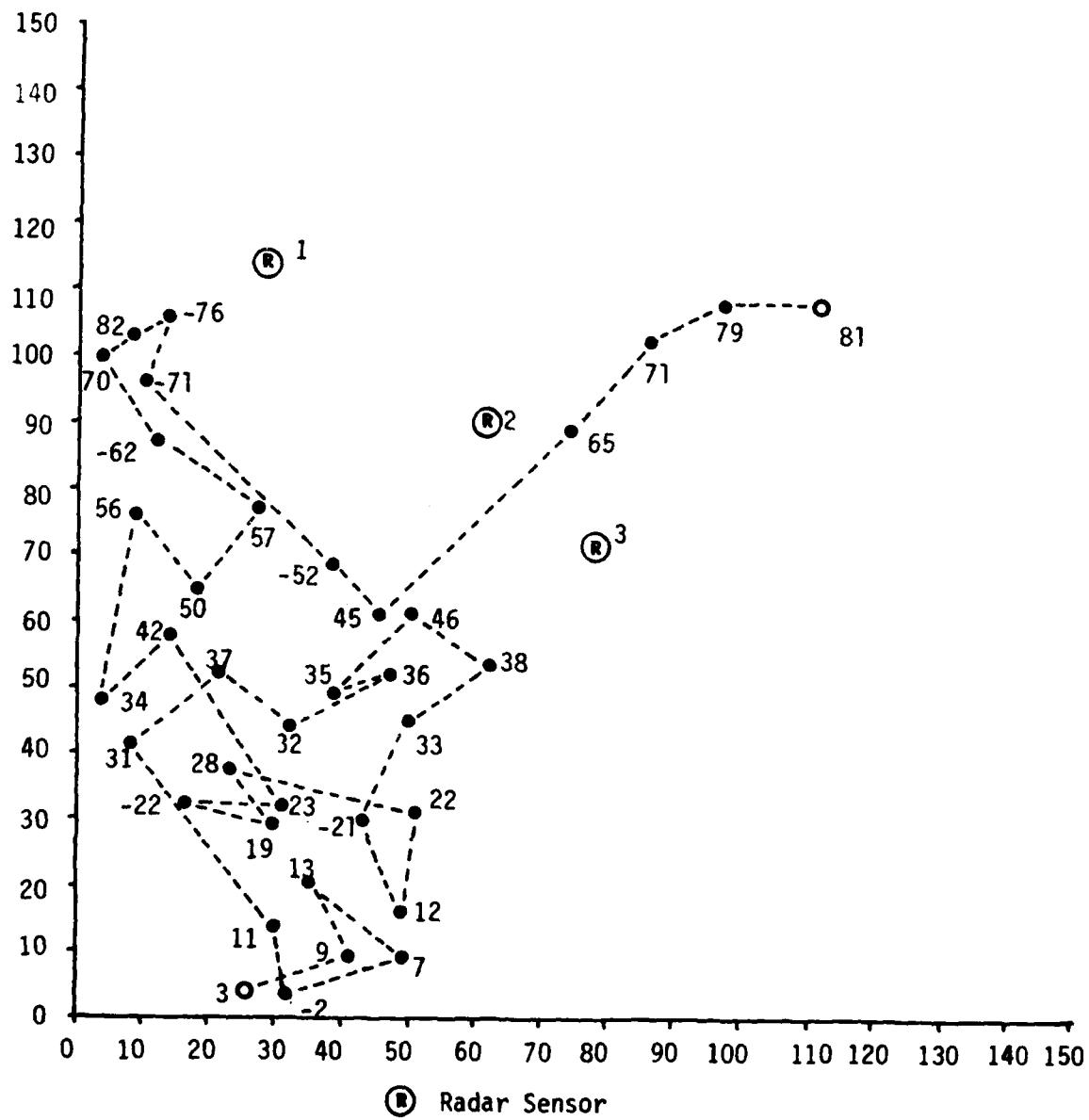


Figure 6.5. Case 5 - A2, R1, S1.

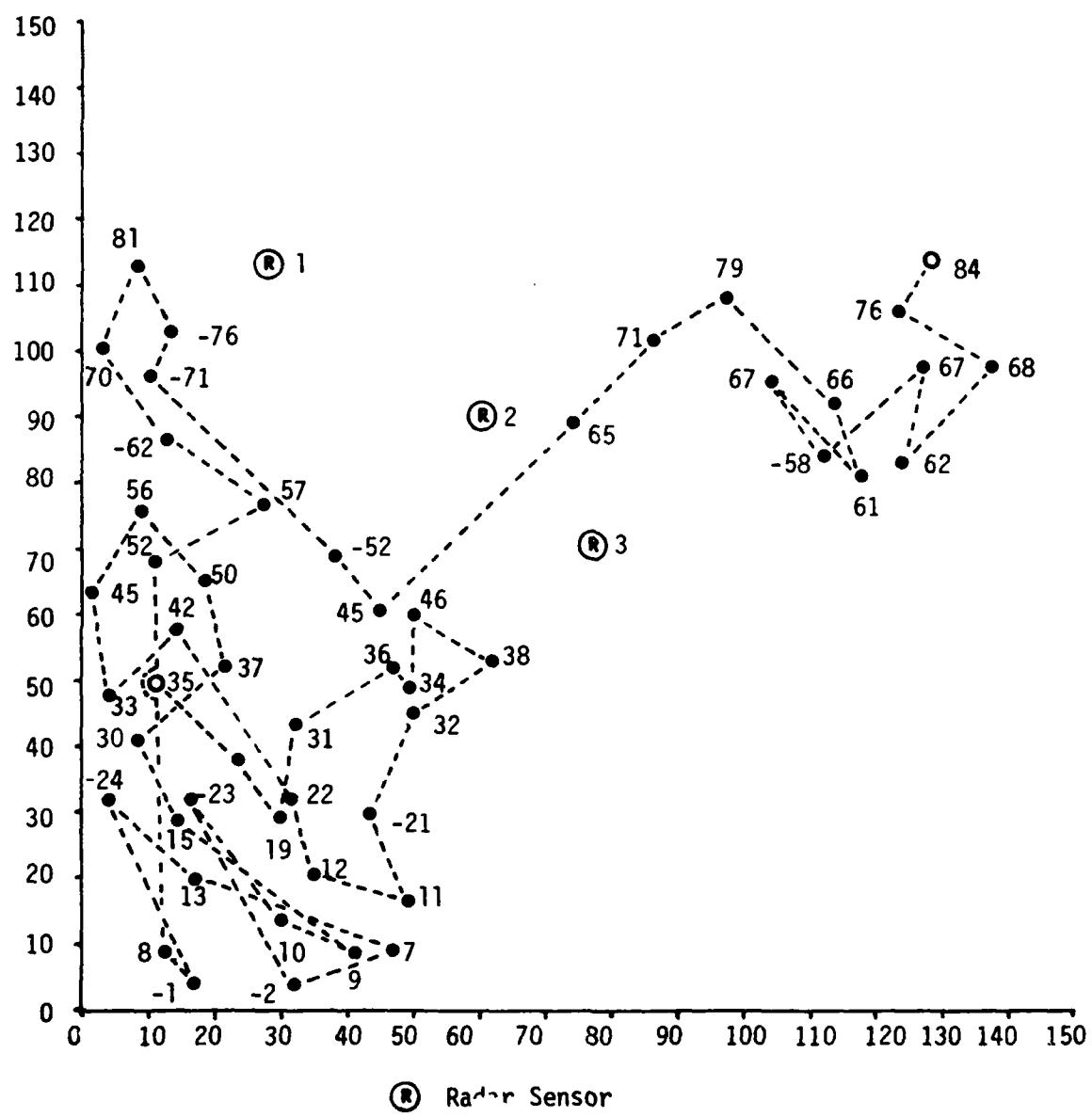


Figure 6.6. Case 6 - A2, R2, S1.

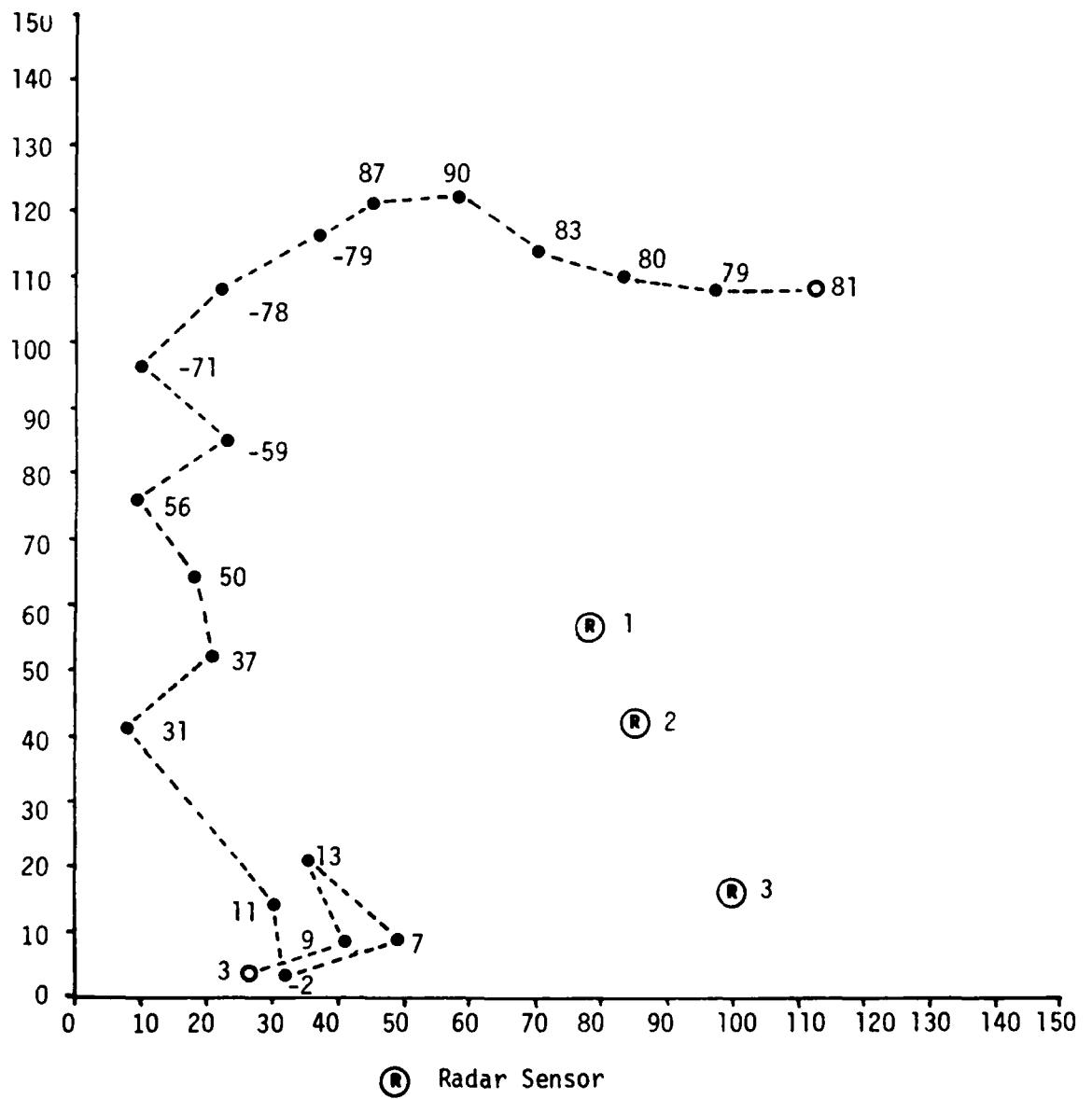


Figure 6.7. Case 7 - A2, R1, S2.

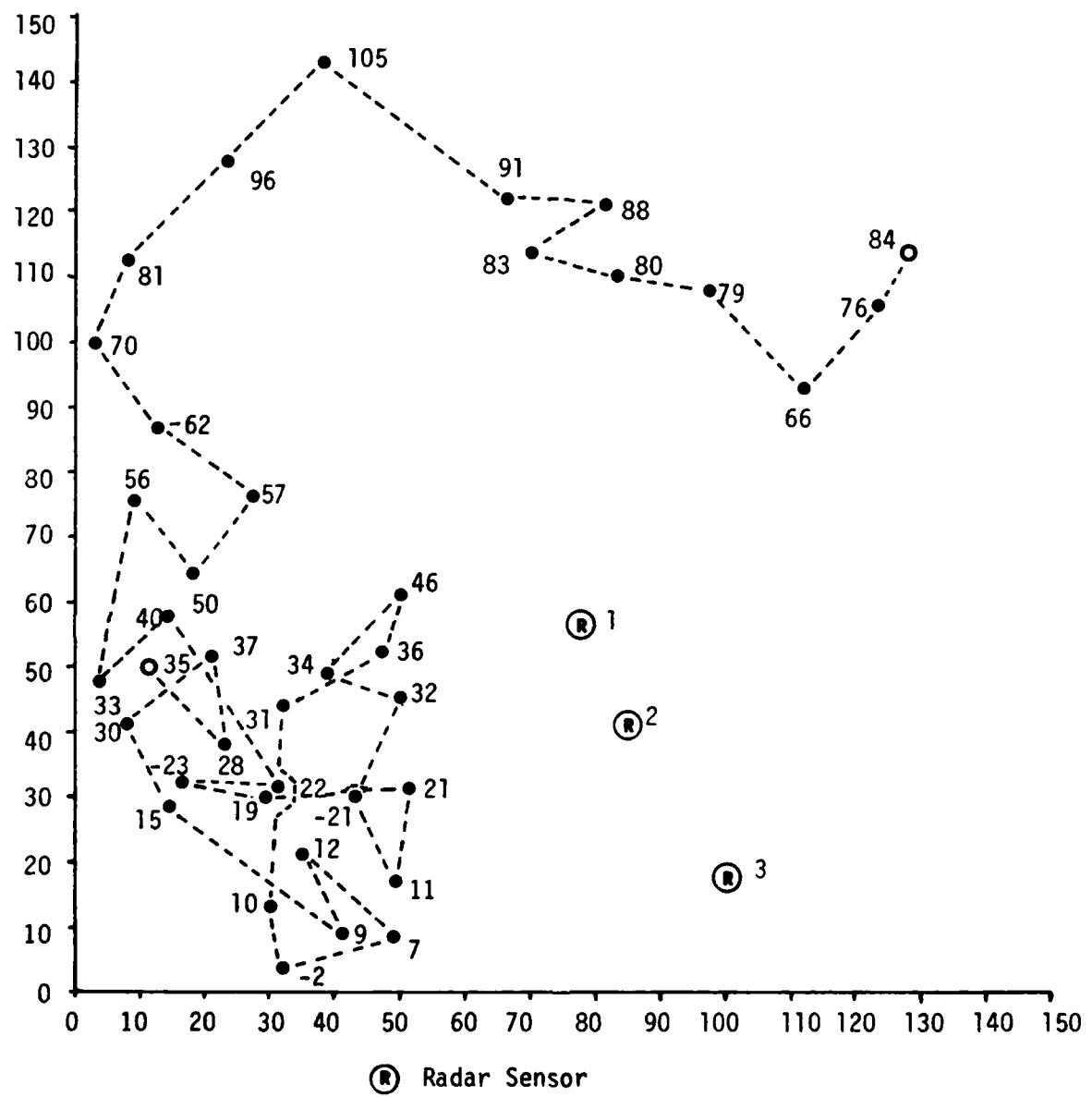


Figure 6.8. Case 8 - A2, R2, S2.

the routes selected follow the base of this ridge (Figures 6.6 and 6.8).

6.3. Refined Routes

These initial routes shown in Figures 6.1 through 6.8 were refined and the new routes are shown in those cases where improvement could be achieved. For case one, the refinement process accepted the initial results as final.

In the other cases improvement was achieved by the refinement process. The improvement in case two occurs at the beginning of the route (Figure 6.9). The route initially headed north and was not able to avoid the air defenses. The model reversed directions and utilized a southern route. The route refinement eliminates the first several nodes to achieve the improvement.

The radars are located in the east for cases three and four. The initial routes are to the north; however, the hilly region in the northwest caused the selection process to change directions and proceeds south. The refinement in case three smoothed the initial portion of the route (Figure 6.10). The destination point in case four is located beyond the line of radars; thus, causing the route selection to double back to avoid the air defenses. There is significant improvement when the route is refined (Figure 6.11).

In area two, the rougher terrain resulted in three of the four routes doubling back significantly. With the radars deployed on the high ground to cover the approach corridors, the route meanders considerably since the model searched for an acceptable low exposure route (Figures 6.5 and 6.6). The selection process finally reached node 45 from which the radars could be breached. Figures 6.12 and 6.13

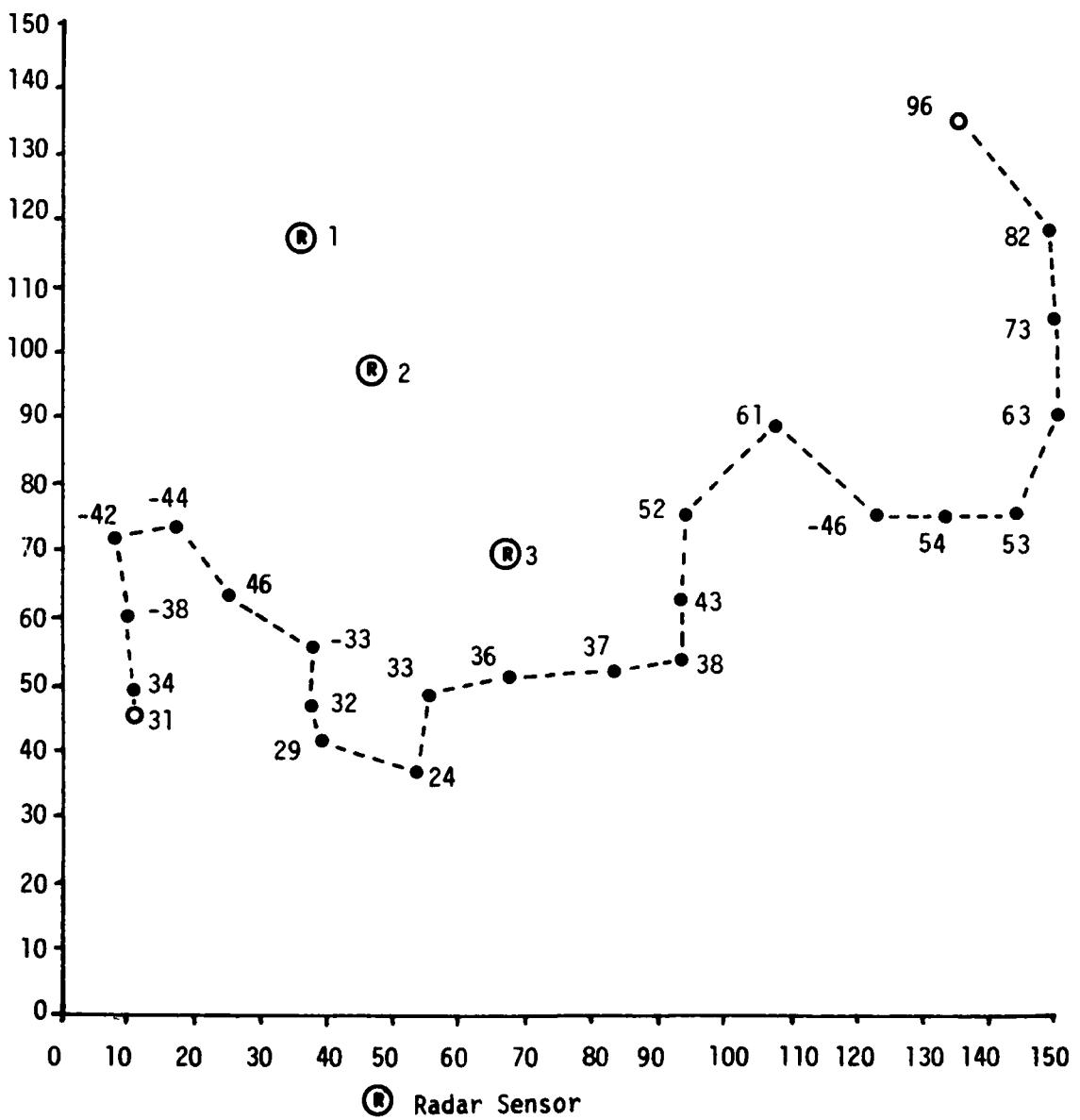


Figure 6.9. Case 2 - Refined Route.

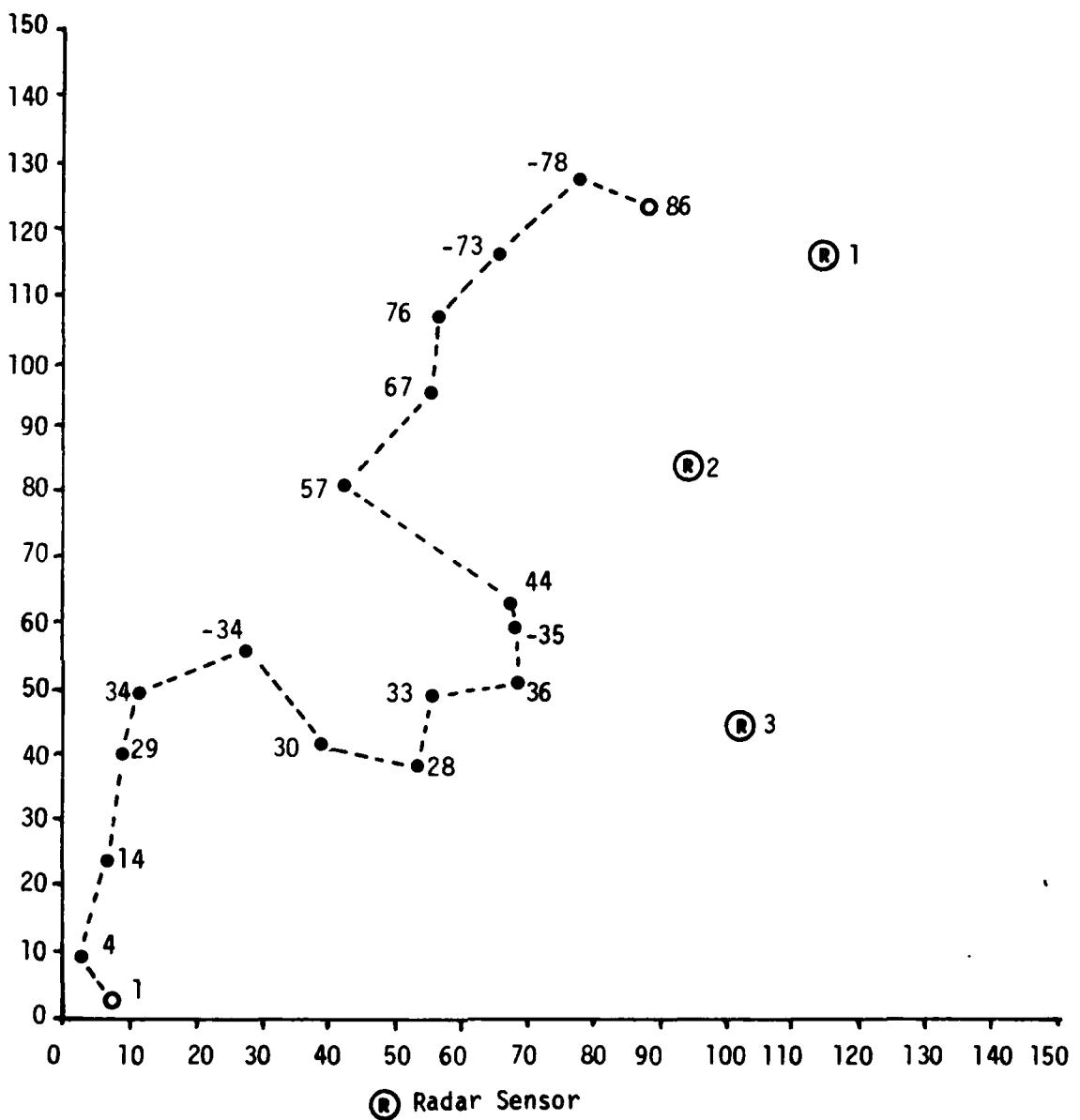


Figure 6.10. Case 3 - Refined Route.

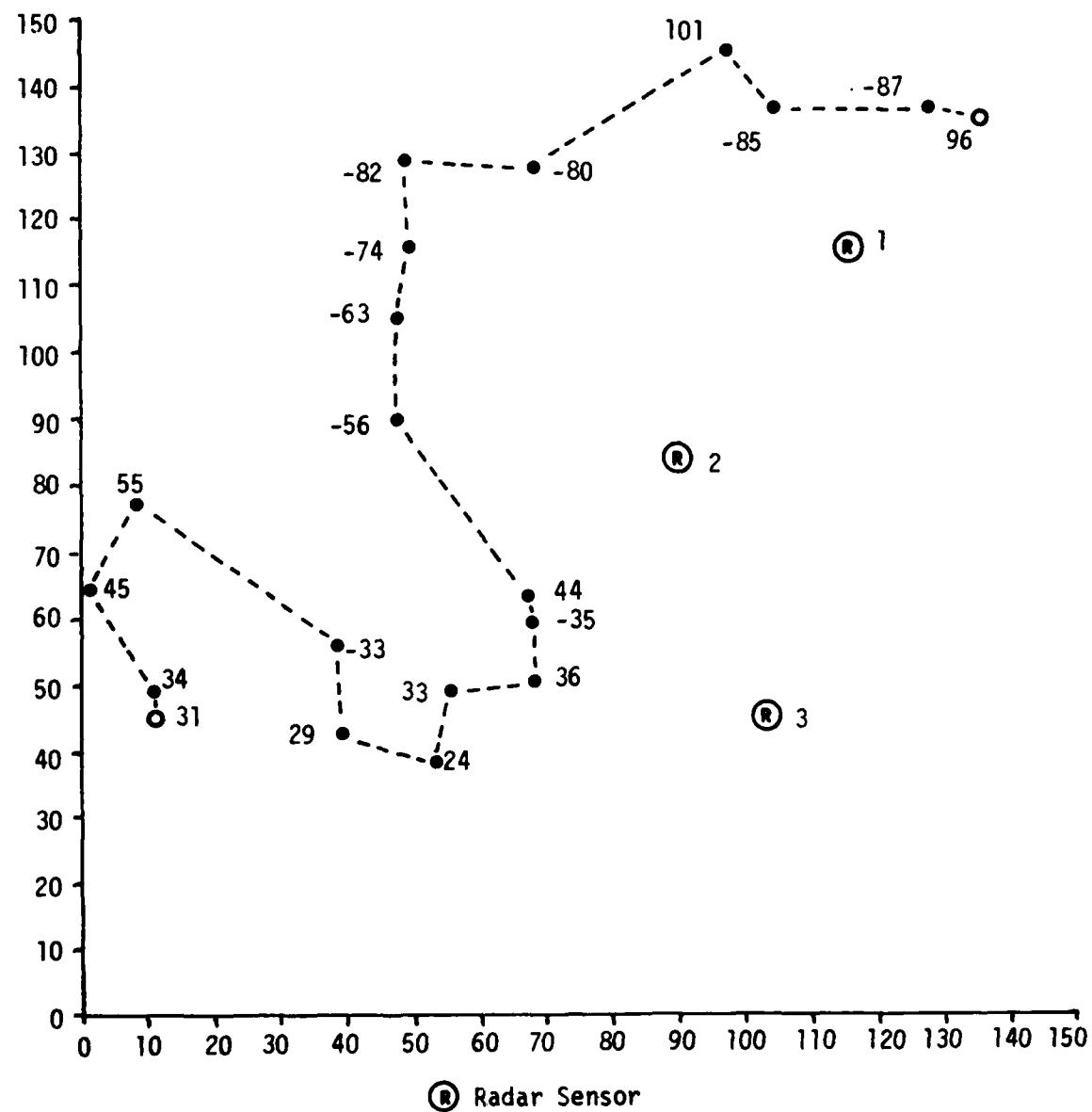


Figure 6.11. Case 4 - Refined Route.

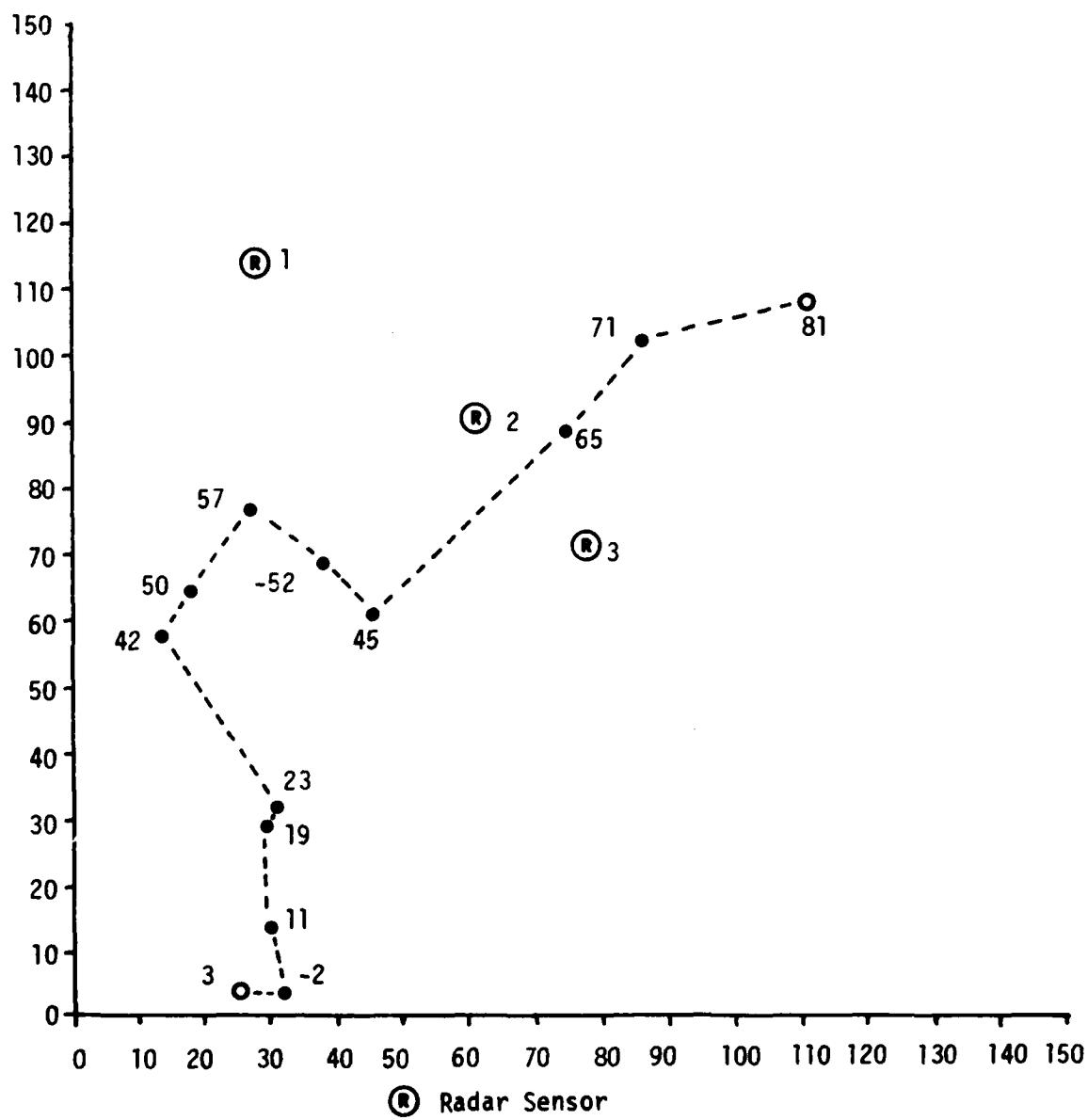


Figure 6.12. Case 5 - Refined Route.

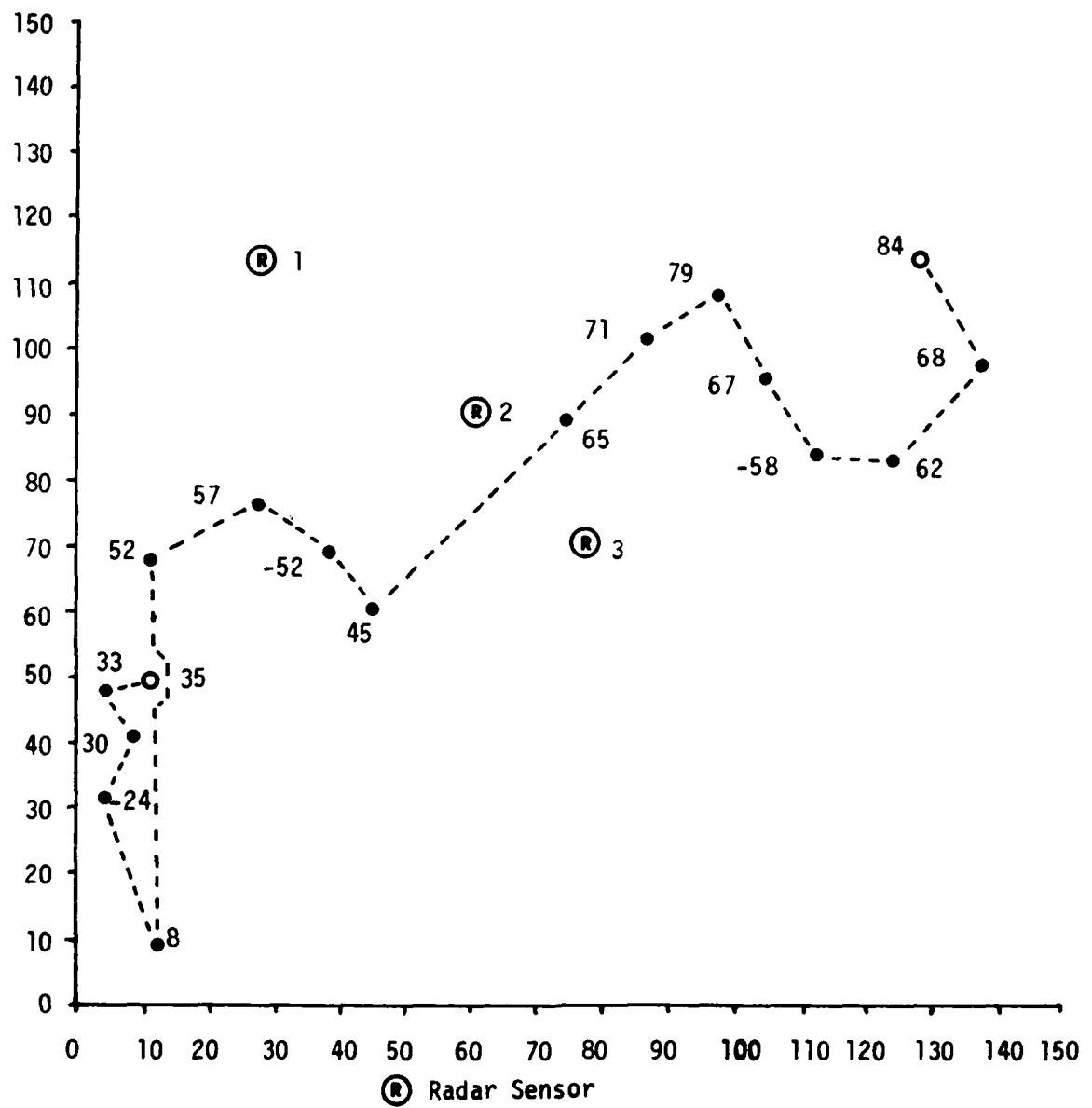


Figure 6.13. Case 6 - Refined Route.

shows considerable route improvement when these routes are refined.

Figure 6.13 indicates that the route refinement is not perfect in that there is obvious improvement by proceeding directly from node 35 to node 52.

Case seven was the only route in area two that the initial route was acceptable. Only the first three nodes are eliminated in the refinement. For case eight, the initial node is located in a narrow valley forcing the route selection to proceed south. This direction is towards the air defenses causing the meandering in the route. The refinement caused the route selection to be across the valley entrance slope to achieve an acceptable route. The routes in Figures 6.14 and 6.15 are mostly along the base of the ridge. In Table 6.10 is a summary of the improvements in terms of nodes traversed.

Table 6.10 Route Improvement (Node Traversed)

Case	Initial	Final
1	25	25
2	32	24
3	26	18
4	57	20
5	37	13
6	51	17
7	20	16
8	39	15

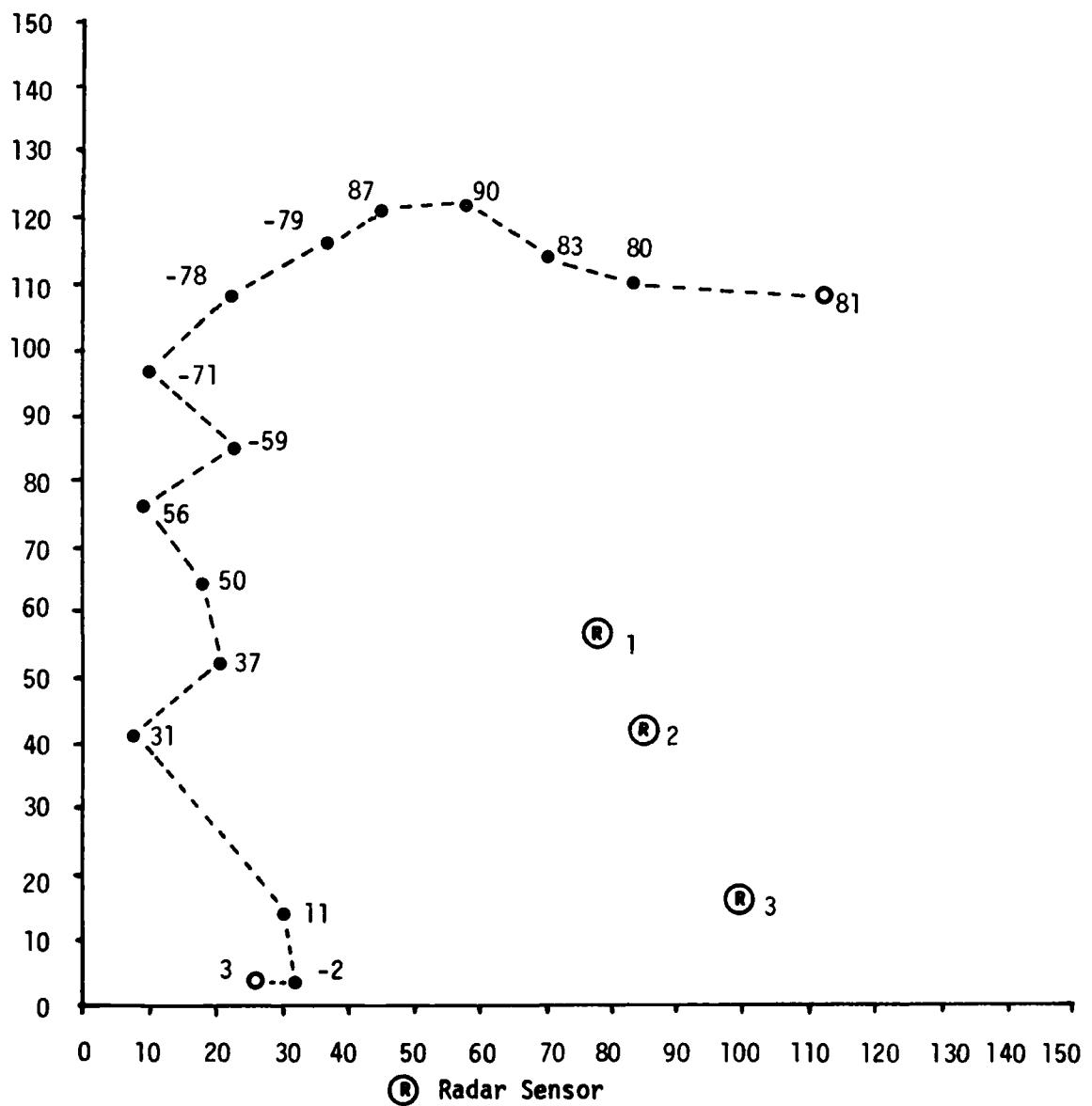


Figure 6.14. Case 7 - Refined Route.

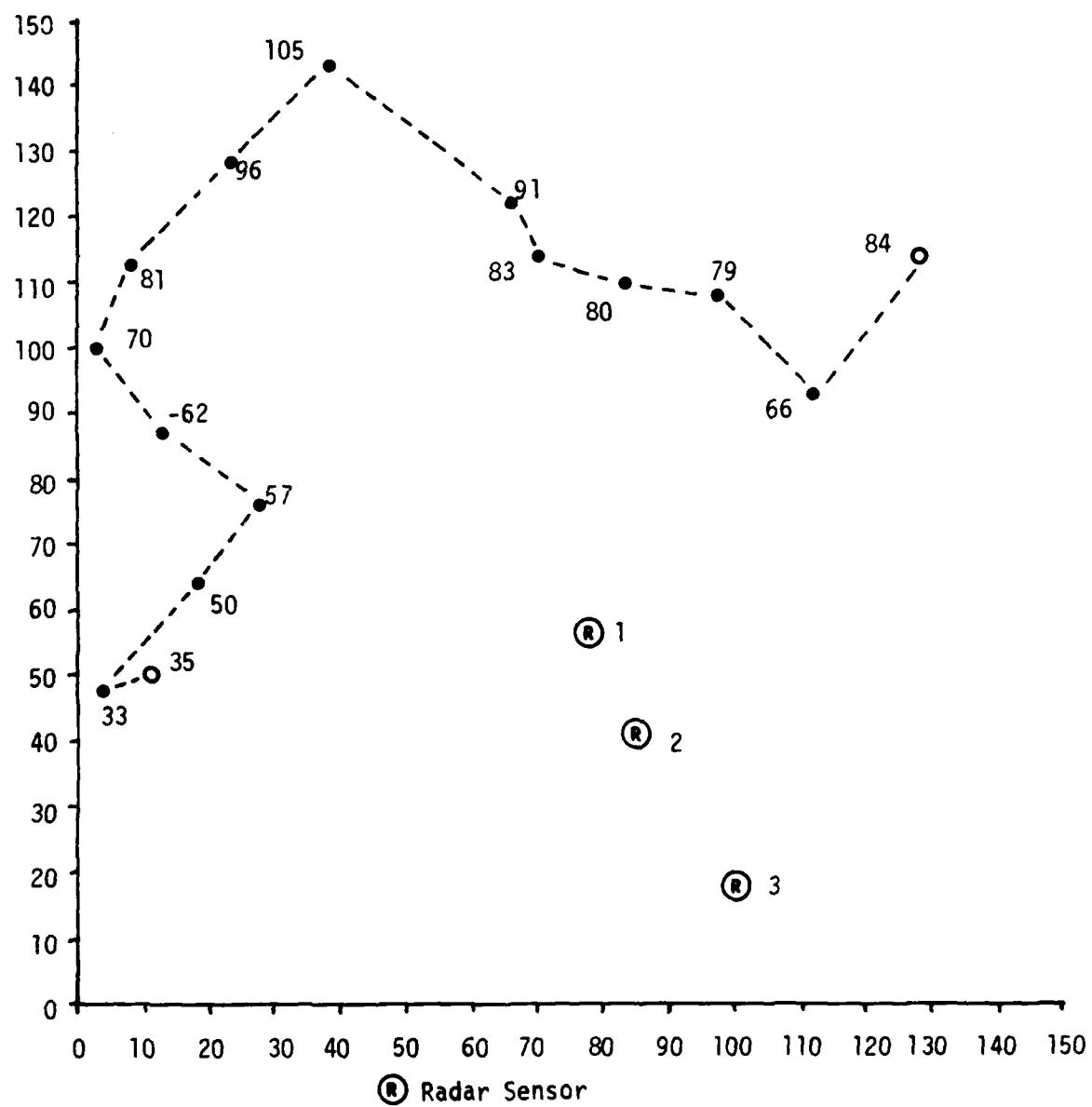


Figure 6.15. Case 8 - Refined Route.

6.4 Large Area Analysis

Several size terrain areas were utilized to evaluate the model's performance. The initial point was held constant and the destination and number of sensors were varied. Table 6.11 gives the location of the sensors and the size area where they were utilized. The areas ranged from 20 by 20 km to 35 by 35 km. The elevation varied from 270 to 610 meters for the 20 by 20 km case and varied from 270 to 850 meters for the 35 by 35 km cases. The limiting factor in the area size is computer core capacity.

The southwest corner of each area is the same. The larger size areas are obtained by increasing the x and y distance from this corner. The test area discussed in section 6.2 is the southwest 10 x 10 km sector of these larger areas. As one travels from the southwest to the northeast the terrain becomes progressively rougher. Thus, the routes were selected to travel this same direction. They begin in the southwest and end in the northeast sector. Since the areas are larger the lethal radius of the systems were increased to 6 km.

The large size of these areas resulted in voluminous output from the model. Therefore, the results are summarized rather than presented in detail as the small areas. The routes developed by the model had the same characteristics of the small areas. The route end points and the sensor deployment determined the smoothness of the route. The routes for all cases would begin fairly straight; however, the deployment of the sensors and terrain roughness would cause meandering of the route when it reached the central area of the 35 by 35 km case. The refinement process eliminated the doubling back as it had done in the small cases.

Table 6.11 Sensor Deployment

20-20 km Area		35-35 km Area	
<u>Sensor</u>	<u>(X,Y,Z)</u>	<u>Sensor</u>	<u>(X,Y,Z)</u>
1	(97, 280, 500)	1	(300, 414, 490)
2	(165, 250, 440)	2	(371, 214, 490)
3	(193, 71, 400)	3	(14, 314, 450)
25-25 km Area		4	(285, 328, 460)
<u>Sensor</u>	<u>(X,Y,Z)</u>	5	(228, 407, 520)
1	(97, 280, 500)	6	(285, 243, 450)
2	(165, 250, 440)	7	(200, 214, 410)
3	(193, 71, 400)	8	(336, 71, 350)
30-30 km Area		9	(364, 288, 530)
<u>Sensor</u>	<u>(X,Y,Z)</u>	10	(97, 280, 500)
1	(97, 280, 500)		
2	(336, 71, 350)		
3	(364, 288, 530)		

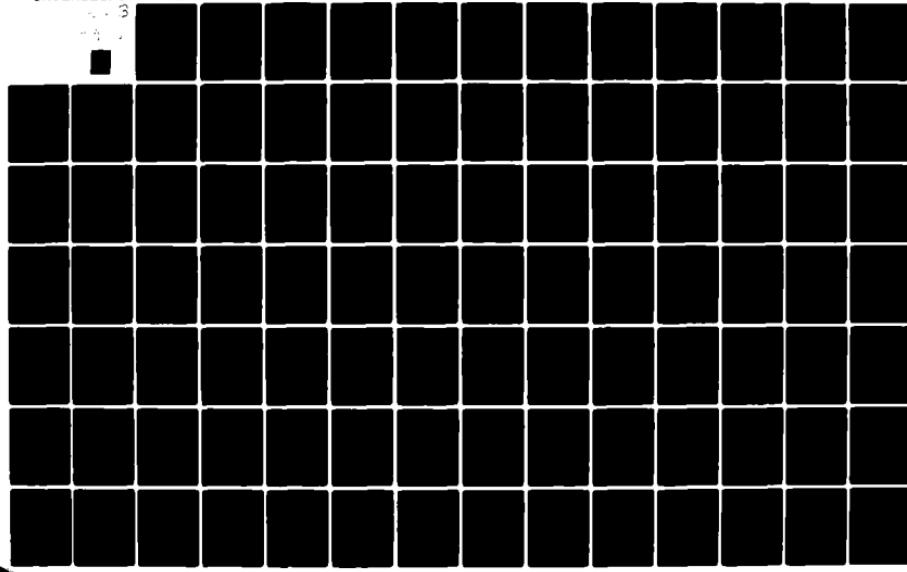
Table 6.12 provides an overall summary of the six large cases. The computer processing time for each of the cases indicates that terrain size significantly increases the run times for the model. The 30 by 30 km case, when compared to the 35 by 35 km case of three radars, indicates the deployment and route end points can produce very different results. The initial routes for these two cases are refined to approximately the same size. In all cases the refinement provided an improvement in route performance by reducing the penalty.

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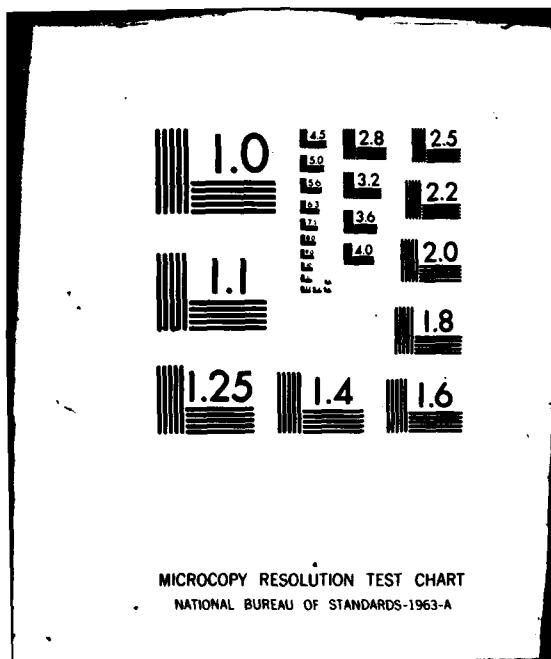


Table 6.12 Large Area Cases

Area	Sensors	Low Nodes	High Nodes	Route Nodes	Penalty	Refined Nodes	Penalty	Run Time (sec)
20-20	3	415	389	63	6996	28	3510	79.5
25-25	3	648	624	218	17498	35	5086	114.1
30-30	3	938	918	458	44499	63	7793	155.1
35-35	3	1289	1258	181	12783	66	5325	187.6
35-35	5	1289	1258	331	29082	86	7097	216.9
35-35	10	1289	1258	466	95154	97	19942	284.3

CHAPTER VII

MODEL VALIDATION

7.1 Introduction

For the model to be of any utility, it must be tested and validated. A comparison is required between a tactician's route analysis and the heuristic model which attempts to approximate that analysis.

The test area has relatively flat terrain through the center region and high ground on the eastern edge and in the northwest corner. The hilly areas are difficult for the model logic to process into a smooth route line that an individual would expect to see for a route.

A tactician planning a route needs to visually perceive the relationship between the route initialization, positions to be avoided, and the final destination. The air defense sensors will be bypassed, if possible, by traveling around these positions outside their effective engagement limits. However, one tactician's ideal route may be another tactician's worst case. The manually produced route is a highly subjective analysis.

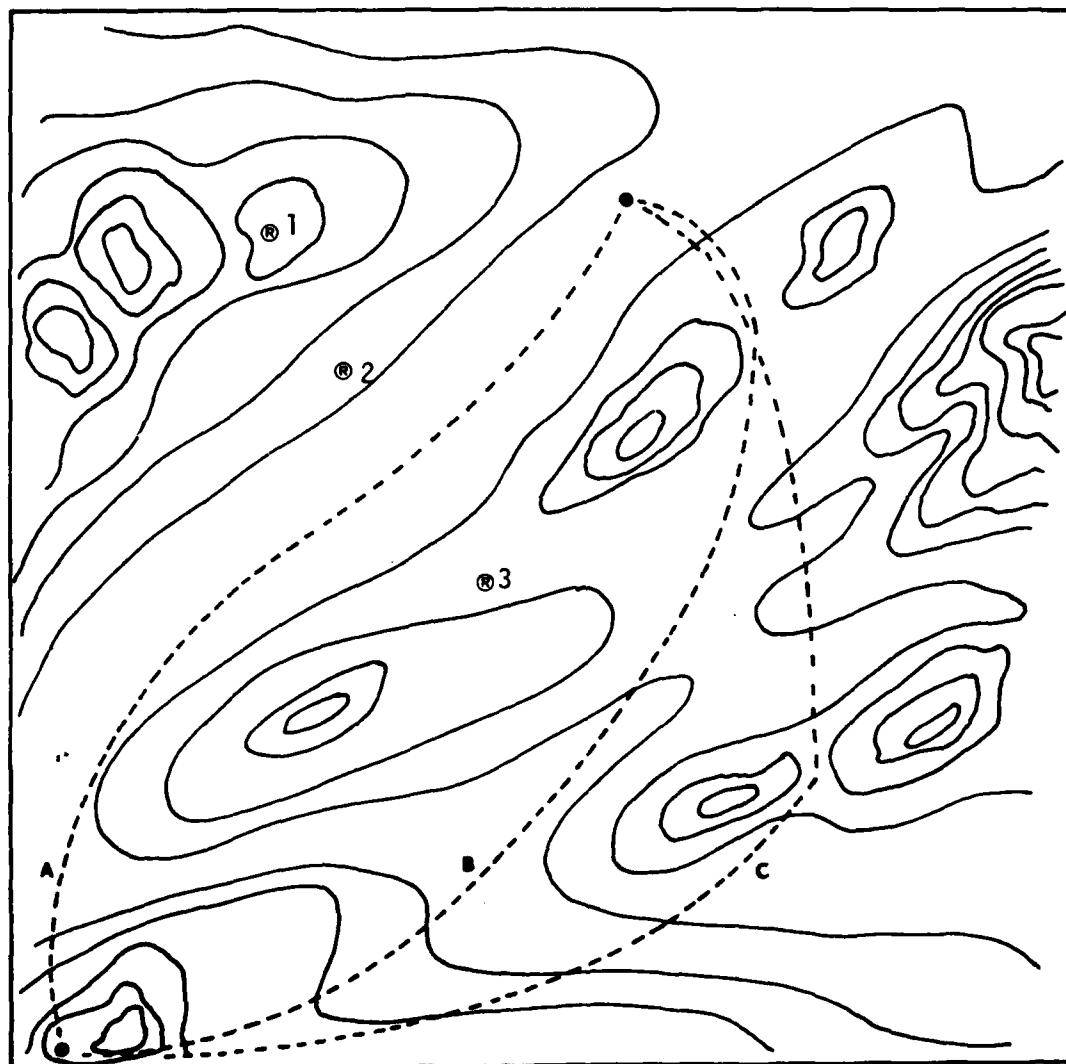
7.2 Manual Route Selection

The development of a route by manual analysis requires studying a topographic map of the appropriate area. The development of a low flying aircraft route dictates the type of information desired: The

location of the air defenses, the valleys, the hill tops, and the built-up areas is important. The information concerning the area is utilized in the route selection to avoid the air defenses and enemy concentrations.

The problem with reading a topographic map is trying to perceive the 3-dimension aspects of the terrain. Ordinarily, relief is shown by contour lines. For level terrain the contour lines are widely spaced whereas rough or hilly terrain will have densely packed contour lines. The rivers and streams give the location of valley floors and lowest points in flat terrain. One method for showing the vertical aspects of the terrain is to draw a profile of the elevation. Along a line between any two points the contour elevations are plotted, from which LOS can be determined and the degree of terrain roughness (see Figure 2.2). For a large area and even a modest number of points this approach is impractical.

Figure 7.1 depicts the terrain area used in the test case and indicates the relative position of the hills and valleys with the sensors. The routes shown in Figure 7.1 were developed by questioning analysts whose expertise is in air defense routing. Providing them with the location of the sensors and the route end points on a topographic map, the routes A, B, and C were chosen. If a direct route is required, route A is proposed since it follows the valley floor and passes midway between two of the sensors. If the sensors are to be avoided, routes B and C are chosen since they utilize the hills as masks and bypass



① Radar Sensor
A,B,C Routes

Figure 7.1. Terrain Area One.

the sensors. Routes B and C are preferred by all the analysts. The question of model validity is whether or not similar routes are produced when the model uses its decision logic.

7.3 Model Route Selection

For development and testing of the model a 10 by 10 km area was selected from the 35 by 35 km data base that is representative of both relatively flat and hilly terrain. In the initial testing, the model would form a circuit through several nodes before returning to the starting node. After these first runs, decision logic was added in the form of weighting as described in Chapter IV. The major piece of information the model considers that the tactician has difficulty in assimilating is the LOS determination. The degree of visibility a node has with the sensors provides a basis upon which a quantitative selection can be made.

To test this hypothesis, the model was run with different levels of information available to the decision logic. With only the distance and height of neighboring nodes, the model produced a very irregular route. The model would exhaust the nodes in the neighborhood before leaving that immediate region for any new points (Figure 7.2).

With the exposure value of a node added to the decision logic, this second level of information allowed the model to produce a node linkage which resembled a route (Figure 7.3). The third level provided data on radar location and range with which the model was able to produce a route that approximates the route an individual analyst would

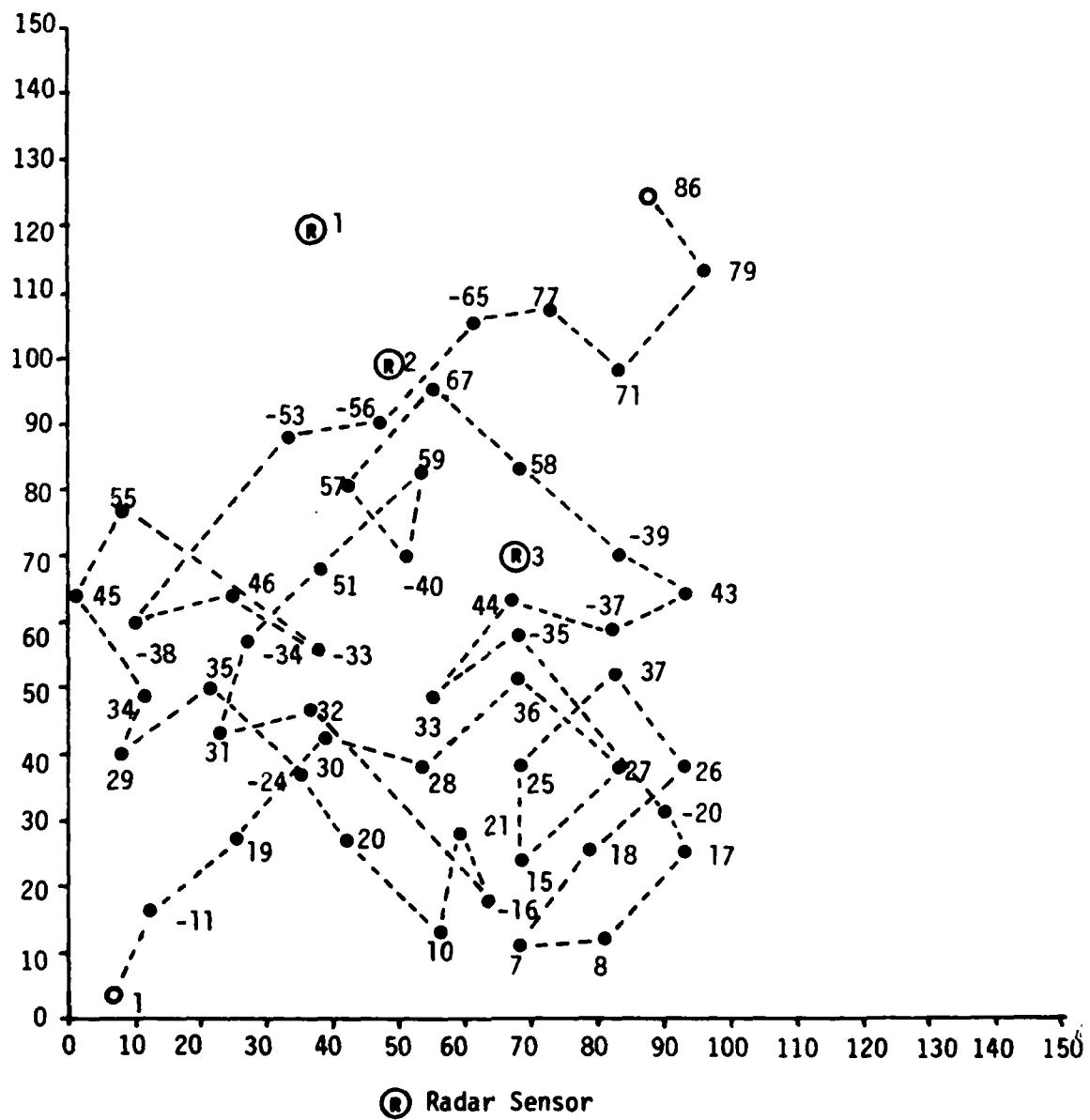


Figure 7.2. Minimal Information Route.

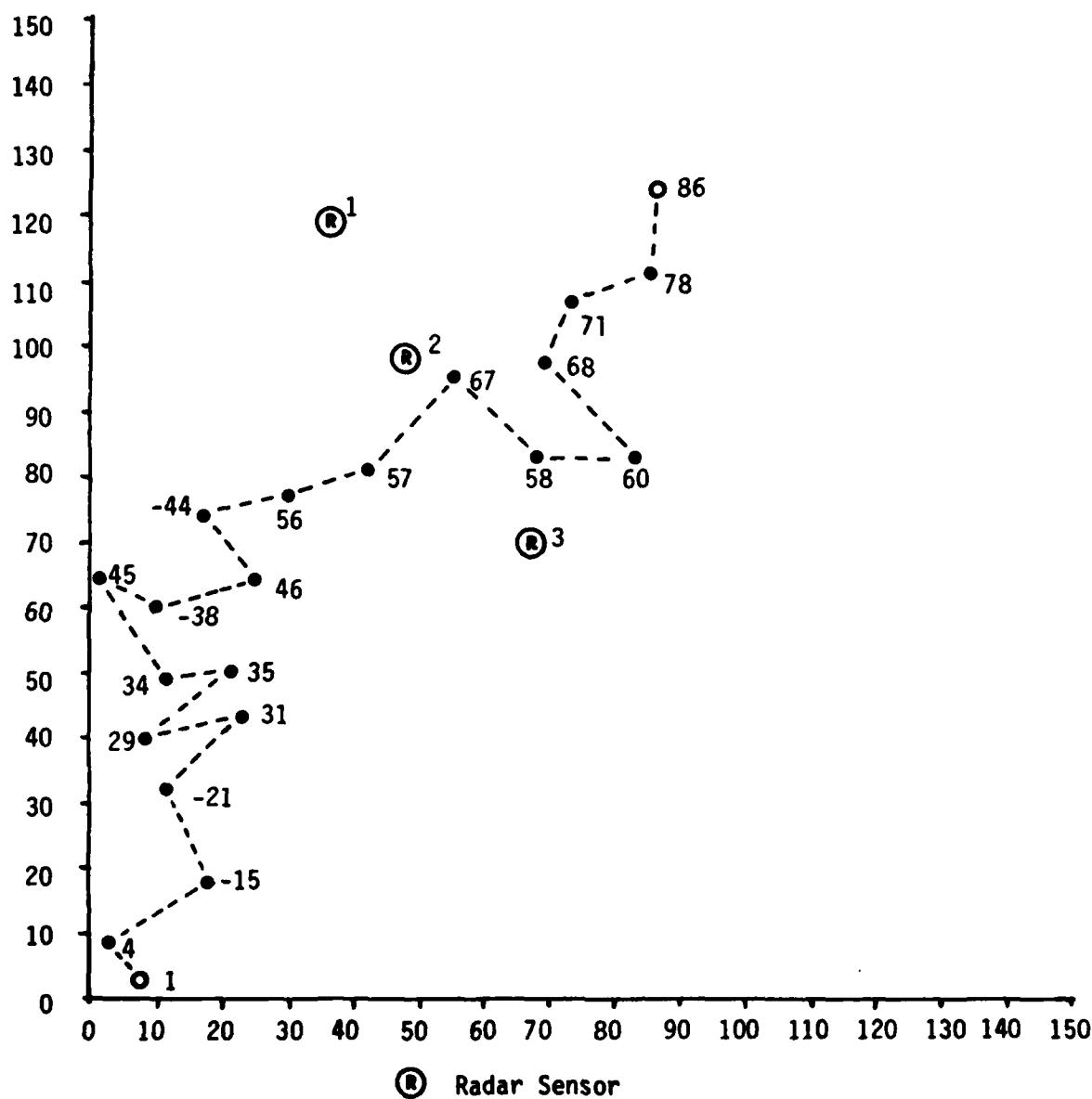


Figure 7.3. Exposure Value Route.

select (Figure 7.4). In Figure 7.4 the radars are deployed in the northern sector and the route avoids them by a southerly route.

When the destination is within 1 km of the current position the final terminal weighting forces the choice of the next position to be the destination or an intermediate node. Normal attacking procedures have some distance from target at which the attack is committed and one proceeds directly towards the target. With high speed aircraft (250 m/sec) this attack point is 3 to 6 km away depending on the type of ordnance being used. Stand-off munitions exist that allow the attacking aircraft to be 20 or more km away when releasing their ordnance, if the target is heavily defended.

The results of the model are a series of linked points which comprise a route. A comparison of Figure 7.4 with Figure 7.1 indicates that the preferred route C is approached with the radar avoidance weighting. The degree of match between the model route and the manual route give a visual indication of acceptability.

7.4 Model Evaluation

The exposure value of each route node point was used as a basis of comparison. Since the routes are not of equal length, the exposure of the node links were used to establish the exposure value of a route. The calculation of route exposure is given below:

$$\text{EVR} = \sum_{i=1}^{n-1} \text{EV}(N_{i+1}) \left[\frac{d_{i+1}}{D} \right]$$

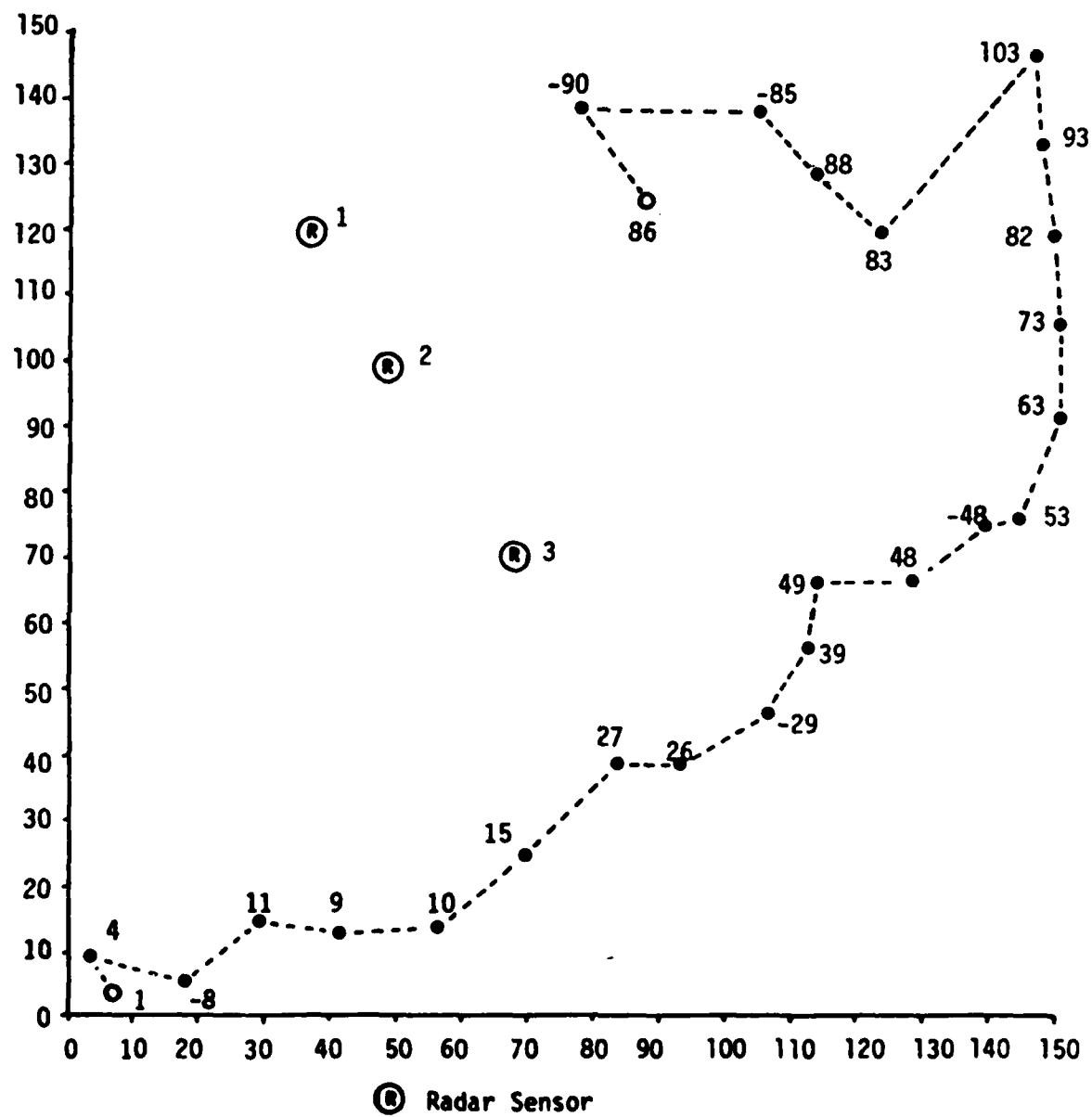


Figure 7.4. Complete Information Route.

$$\text{where } D = \sum_{i=1}^{n-1} d_{i+1},$$

D = The total length of the route,

$EV(N_{i+1})$ = The exposure value of route node $i+1$,

d_{i+1} = The distance from node i to node $i+1$,

EVR = The exposure value of the route.

Utilizing this relation the model routes can be compared with the manually chosen routes. The scenario for the manual selection and the model is Case 1. In Table 7.1 the route exposure values are given for the three manual routes and the model route. The preferred route C and the model route achieved an exposure value of 0.844 and 0.888 respectively.

The other routes that were developed by the model indicate that the deployment of the sensors within the terrain have a definite effect on the selection process. Rough terrain with sensors deployed to cover the low elevation corridors is the most difficult case for the model to evaluate and select a minimum exposure, minimum elevation route for penetrating the air defenses.

Table 7.1 Route Exposure Values

Route	EVR
A	1.582
B	1.325
C	0.844
Model	0.888

CHAPTER VIII

CONCLUSIONS AND RECOMMENDATIONS

8.1 Conclusions

This research has addressed an area of air defense modeling which is normally analyzed visually with topographic maps and coverage diagrams before any tactical gaming is performed. A significant problem in analyzing terrain from a topographic map is perceiving the 3-dimensional aspects of terrain features. The degree of visibility a manually developed route will have can only, at best, be estimated. Any route selected is based on the particular individual's ability to be a good tactician. Using the subjective route for air defense modeling adds an unknown to the war gaming results.

The model that has been presented overcomes the shortcomings cited above and provides a minimum-exposure, minimum-elevation route. The developed route then serves as a baseline from which other flight paths can be evaluated. The model provides the visibility or exposure of all the high and low elevation nodes within the area. These values can be used as a reference for evaluating the visibility of specific areas of the terrain in addition to route identification.

Terrain roughness has a marked effect in the developed route. By placing the radar sensors at key positions to cover approach corridors, the model develops long routes in searching for a minimum exposure route. The long routes indicate the problem of traversing an area undetected by modern air defenses. The addition of more sensors

increases the penalty associated with travel through an area and also increases the route length. In the 35 by 35 km case the penalty value increased from 12783 for the three radar case to 95154 for the ten radar case. The route nodes also varied from 181 to 466 in the initial routes.

8.2 Recommendations for Further Research

In testing this model it became very obvious that minor changes in weighting of a single node point would result in an entirely different route. Further research is needed into the sensitivity of the weighting scheme utilized in this model.

The decision logic that is used in this model is by no means the only one that should be used. There needs to be the ability to enter check points through which the route must pass on its way to the destination. Along this same line of reasoning, the model could be modified to evaluate a proposed route rather than find the route.

The idea of limiting the next node selection to a neighborhood about the current position could be expanded to other problems besides air defense aircraft routes. The routing of oil and gas pipelines could be analyzed using the model. The radar sites could be a town or built up areas to be avoided. The weighting of the height penalty could be increased to favor level terrain.

Lastly, the author hopes that this research might serve as a start for further effort into the general problem of routing.

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APPENDICES

APPENDIX A

ROUTING PROBLEMS

Within this appendix are the data tables for the additional problem cases discussed in Chapter 6. Each set of tables is preceded by a page identifying the case. The tables for exposure values in these cases were not included for the sake of brevity.

Case 2 - Area 1, Route 2, Sensor set 1.

Table A.1. Case 2 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
31	770	10150	30	26	1610	10010
30	1610	10010	28	74	560	9200
28	560	9200	35	2	1470	10500
35	1470	10500	34	164	770	10430
34	770	10430	45	1	70	11480
45	70	11480	-38	154	700	11200
-38	700	11200	-42	260	560	12040
-42	560	12040	-52	231	560	13090
-52	560	13090	-44	97	1190	12180
-44	1190	12180	46	188	1750	11480
46	1750	11480	-33	214	2660	10520
-33	2660	10520	32	354	2590	10290
32	2590	10290	-22	452	3290	9240
-22	3290	9240	29	145	2730	9940
29	2730	9940	24	232	3710	9660
24	3710	9660	25	243	4760	9660
25	4760	9660	33	228	3650	10430
33	3650	10430	36	295	4760	10570
36	4760	10570	37	240	5810	10640
37	5810	10640	38	198	6510	10760
38	6510	10760	43	298	6580	11410
43	6580	11410	52	278	6580	12320
52	6580	12320	61	255	7560	13230
61	7560	13230	-46	252	8540	12250
-46	8540	12250	54	87	9380	12320
54	9380	12320	53	56	10060	12320
53	10060	12320	63	71	10500	13370
63	10500	13370	73	27	10500	14350
73	10500	14350	82	57	10430	15330
82	10430	15330	92	96	10290	16240
92	10290	16240	96	285	9450	16450

Table A.2. Case 2 - Node Linkage

NODE NO.	31	TOTAL LINKS	7
X,Y,Z COORDINATE	11,	45,	280
LINKED TO	34	28	35
EXPOSURE	100	53	34
WEIGHTED	101	168	70
			30
			-21
			-23
			-38
NODE NO.	30	TOTAL LINKS	9
X,Y,Z COORDINATE	23,	43,	280
LINKED TO	35	34	32
EXPOSURE	100	51	118
WEIGHTED	101	104	238
			74
			714
			281
			688
			374
			618
NODE NO.	28	TOTAL LINKS	4
X,Y,Z COORDINATE	8,	40,	280
LINKED TO	34	35	-21
EXPOSURE	100	0	258
WEIGHTED	101	2	518
			296
NODE NO.	35	TOTAL LINKS	6
X,Y,Z COORDINATE	21,	50,	280
LINKED TO	34	46	-34
EXPOSURE	91	258	372
WEIGHTED	104	518	742
			408
			550
			214
NODE NO.	34	TOTAL LINKS	3
X,Y,Z COORDINATE	11,	49,	280
LINKED TO	45	-38	-23
EXPOSURE	0	254	180
WEIGHTED	1	255	181
NODE NO.	45	TOTAL LINKS	3
X,Y,Z COORDINATE	10,	54,	300
LINKED TO	55	-38	-42
EXPOSURE	228	163	211
WEIGHTED	458	164	424
NODE NO.	-38	TOTAL LINKS	3
X,Y,Z COORDINATE	10,	56,	310
LINKED TO	46	-42	-44
EXPOSURE	151	259	165
WEIGHTED	304	260	332
NODE NO.	-42	TOTAL LINKS	3
X,Y,Z COORDINATE	9,	72,	330
LINKED TO	55	-44	-52
EXPOSURE	279	126	230
WEIGHTED	280	254	231
NODE NO.	-52	TOTAL LINKS	5
X,Y,Z COORDINATE	8,	57,	350
LINKED TO	55	70	-54
EXPOSURE	270	313	339
WEIGHTED	542	314	480
			97
			494
NODE NO.	-44	TOTAL LINKS	5
X,Y,Z COORDINATE	17,	74,	330
LINKED TO	55	46	56
EXPOSURE	305	167	208
WEIGHTED	620	188	418
			504
			486
NODE NO.	46	TOTAL LINKS	5
X,Y,Z COORDINATE	25,	64,	300
LINKED TO	51	56	-34
EXPOSURE	250	266	306
WEIGHTED	502	534	614
			722
			214
NODE NO.	-33	TOTAL LINKS	6
X,Y,Z COORDINATE	39,	56,	300
LINKED TO	32	51	29
EXPOSURE	176	395	177
WEIGHTED	354	792	356
			810
			764
			3360

Table A.2. (cont'd.)

NODE NO.	32	TOTAL LINKS	5
X,Y,Z COORDINATE	37,	47,	280
LINKED TO	29	-24	-34
EXPOSURE	227	291	332
WEIGHTED	496	584	666
NODE NO.	33	TOTAL LINKS	6
X,Y,Z COORDINATE	47,	32,	290
LINKED TO	18	24	20
EXPOSURE	315	268	190
WEIGHTED	632	538	191
NODE NO.	29	TOTAL LINKS	5
X,Y,Z COORDINATE	39,	42,	280
LINKED TO	24	18	15
EXPOSURE	231	262	252
WEIGHTED	232	906	508
NODE NO.	24	TOTAL LINKS	6
X,Y,Z COORDINATE	53,	36,	280
LINKED TO	21	20	25
EXPOSURE	273	265	242
WEIGHTED	487	532	243
NODE NO.	25	TOTAL LINKS	6
X,Y,Z COORDINATE	68,	38,	280
LINKED TO	36	20	13
EXPOSURE	269	269	256
WEIGHTED	3100	540	518
NODE NO.	33	TOTAL LINKS	4
X,Y,Z COORDINATE	55,	45,	280
LINKED TO	36	44	-36
EXPOSURE	254	278	416
WEIGHTED	295	2790	419
NODE NO.	36	TOTAL LINKS	6
X,Y,Z COORDINATE	68,	51,	280
LINKED TO	44	37	47
EXPOSURE	197	279	337
WEIGHTED	3880	240	3380
NODE NO.	37	TOTAL LINKS	7
X,Y,Z COORDINATE	83,	52,	280
LINKED TO	38	42	27
EXPOSURE	197	363	204
WEIGHTED	196	364	418
NODE NO.	36	TOTAL LINKS	5
X,Y,Z COORDINATE	53,	54,	280
LINKED TO	43	42	-37
EXPOSURE	297	250	258
WEIGHTED	298	2510	2593
NODE NO.	43	TOTAL LINKS	5
X,Y,Z COORDINATE	94,	62,	290
LINKED TO	42	52	-37
EXPOSURE	311	277	262
WEIGHTED	3120	278	526
NODE NO.	52	TOTAL LINKS	8
X,Y,Z COORDINATE	54,	76,	300
LINKED TO	60	62	42
EXPOSURE	291	277	231
WEIGHTED	584	278	464
NODE NO.	61	TOTAL LINKS	9
X,Y,Z COORDINATE	129,	89,	336
LINKED TO	66	72	-51
EXPOSURE	339	227	346
WEIGHTED	340	456	694

Table A.2. (cont'd.)

NODE NO.	46	TOTAL LINKS	6
X,Y,Z COORDINATE	122°	75°	330
LINKED TO	48	54	49
EXPOSURE	146	86	234
WEIGHTED	294	87	470
NODE NO.	54	TOTAL LINKS	6
X,Y,Z COORDINATE	134°	76°	310
LINKED TO	53	48	50
EXPOSURE	55	103	90
WEIGHTED	56	208	182
NODE NO.	53	TOTAL LINKS	5
X,Y,Z COORDINATE	144°	76°	300
LINKED TO	50	63	42
EXPOSURE	128	70	110
WEIGHTED	258	71	222
NODE NO.	63	TOTAL LINKS	5
X,Y,Z COORDINATE	150°	51°	360
LINKED TO	73	-57	-61
EXPOSURE	26	259	283
WEIGHTED	27	600	284
NODE NO.	73	TOTAL LINKS	7
X,Y,Z COORDINATE	150°	125°	360
LINKED TO	82	-69	-61
EXPOSURE	56	322	312
WEIGHTED	57	323	626
NODE NO.	82	TOTAL LINKS	5
X,Y,Z COORDINATE	149°	119°	340
LINKED TO	92	-77	-65
EXPOSURE	95	284	288
WEIGHTED	96	205	576
NODE NO.	92	TOTAL LINKS	5
X,Y,Z COORDINATE	147°	132°	330
LINKED TO	96	103	-77
EXPOSURE	284	61	249
WEIGHTED	285	14600	750

Case 3 - Area 1, Route 1, Sensor Set 2.

Table A

FROM	CASTING	WEIGHT	PERCENT	PERCENT	PERCENT
1	690	72			690
-11	662	61			662
19	1796	90			1796
30	2730	116			2730
26	2710	90			2710
36	4760	122			4760
27	5810	1260			5810
26	6910	96			6910
18	5530	88			5530
29	4760	96			4760
13	3890	104			3890
-39	4760	111			4760
47	3920	115			3920
44	4690	114			4690
43	6580	114			6580
-47	7200	122			7200
52	6580	123			6580
60	5810	120			5810
-41	4760	119			4760
-37	5740	111			5740
58	6510	107			6510
42	5880	114			5880
49	7910	116			7910
48	8960	116			8960
50	10010	117			10010
54	9380	123			9380
-46	8540	122			8540
-55	9450	135			9450
53	10020	123			10020
63	10500	133			10500
73	10580	143			10580
82	10430	153			10430
93	10290	162			10290
103	10220	172			10220
-92	9800	170			9800
-93	8050	170			8050
-85	7200	165			7200
92	6370	160			6370

Table A.4. Case 3 - Node Linkage

NODE NO.	1	TOTAL LINKS	6
X,Y,Z COORDINATE	7 _o	3 _o	27 _o
LINKED TO	4	-6	-8
EXPOSURE	85	223	173
WEIGHTED	86	224	174
NODE NO.	-11	TOTAL LINKS	6
X,Y,Z COORDINATE	12 _o	16 _o	53 _o
LINKED TO	14	4	19
EXPOSURE	95	52	40
WEIGHTED	96	106	41
NODE NO.	19	TOTAL LINKS	7
X,Y,Z COORDINATE	22 _o	27 _o	30 _o
LINKED TO	11	30	-23
EXPOSURE	154	53	180
WEIGHTED	310	54	181
NODE NO.	30	TOTAL LINKS	7
X,Y,Z COORDINATE	35 _o	42 _o	28 _o
LINKED TO	32	28	20
EXPOSURE	154	91	123
WEIGHTED	155	92	248
NODE NO.	28	TOTAL LINKS	6
X,Y,Z COORDINATE	51 _o	32 _o	28 _o
LINKED TO	33	21	25
EXPOSURE	140	126	105
WEIGHTED	141	254	106
NODE NO.	36	TOTAL LINKS	8
X,Y,Z COORDINATE	66 _o	51 _o	26 _o
LINKED TO	44	25	33
EXPOSURE	232	120	120
WEIGHTED	233	242	242
NODE NO.	37	TOTAL LINKS	8
X,Y,Z COORDINATE	83 _o	52 _o	28 _o
LINKED TO	38	42	27
EXPOSURE	76	242	114
WEIGHTED	77	466	230
NODE NO.	26	TOTAL LINKS	7
X,Y,Z COORDINATE	93 _o	35 _o	26 _o
LINKED TO	27	17	19
EXPOSURE	143	128	57
WEIGHTED	144	258	116
NODE NO.	18	TOTAL LINKS	9
X,Y,Z COORDINATE	75 _o	26 _o	26 _o
LINKED TO	15	27	17
EXPOSURE	154	136	160
WEIGHTED	310	137	161
NODE NO.	25	TOTAL LINKS	5
X,Y,Z COORDINATE	68 _o	15 _o	26 _o
LINKED TO	21	15	27
EXPOSURE	154	148	145
WEIGHTED	310	298	150
NODE NO.	33	TOTAL LINKS	3
X,Y,Z COORDINATE	55 _o	49 _o	28 _o
LINKED TO	44	-36	-35
EXPOSURE	75	255	106
WEIGHTED	152	256	107
NODE NO.	-35	TOTAL LINKS	5
X,Y,Z COORDINATE	68 _o	59 _o	29 _o
LINKED TO	44	47	-41
EXPOSURE	175	106	215
WEIGHTED	176	107	216
			111
			354

Table A.4. (cont'd.)

NODE NO.	47 TOTAL LINKS	4
X,Y,Z COORDINATE	56° 65° 290	
LINKED TO	69 -40 -36 -41	
EXPOSURE	110 260 209 170	
WEIGHTED	111 261 420 342	
NODE NO.	44 TOTAL LINKS	21
X,Y,Z COORDINATE	67° 63° 290	
LINKED TO	42 58 59 60 -43 38 51 27 52 57	
LINKED TO	32 62 65 -41 -37 -40 -35 -36 -49 -33	
LINKED TO	-56	
EXPOSURE	183 207 237 197 68 34 195 93 90 202	
EXPOSURE	67 168 216 243 185 202 215 190 220 149	
EXPOSURE	233	
WEIGHTED	180 208 2380 396 65 70 392 188 910 203	
WEIGHTED	136 338 2170 244 186 203 2190 382 442 300	
WEIGHTED	230	
NODE NO.	43 TOTAL LINKS	6
X,Y,Z COORDINATE	94° 63° 290	
LINKED TO	38 42 52 -37 -39 -47	
EXPOSURE	100 186 79 143 163 98	
WEIGHTED	202 187 800 288 164 99	
NODE NO.	47 TOTAL LINKS	8
X,Y,Z COORDINATE	104° 75° 330	
LINKED TO	52 49 61 62 -50 -45 -41 -49	
EXPOSURE	62 42 172 98 268 149 220 139	
WEIGHTED	63 86 356 990 2690 300 221 1400	
NODE NO.	52 TOTAL LINKS	7
X,Y,Z COORDINATE	94° 76° 300	
LINKED TO	50 62 42 61 -49 -50 -35	
EXPOSURE	156 162 101 169 232 243 153	
WEIGHTED	157 1630 204 340 2330 244 302	
NODE NO.	60 TOTAL LINKS	6
X,Y,Z COORDINATE	63° 83° 300	
LINKED TO	62 58 58 -49 -39 -41	
EXPOSURE	172 122 151 284 141 84	
WEIGHTED	1730 246 304 2650 284 170	
NODE NO.	41 TOTAL LINKS	4
X,Y,Z COORDINATE	66° 71° 300	
LINKED TO	56 55 -35 -37	
EXPOSURE	173 219 234 99	
WEIGHTED	174 2200 235 180	
NODE NO.	37 TOTAL LINKS	1
X,Y,Z COORDINATE	82° 55° 290	
LINKED TO	42 38 -35	
EXPOSURE	229 0 194	
WEIGHTED	230 2 390	
NODE NO.	38 TOTAL LINKS	3
X,Y,Z COORDINATE	91° 54° 240	
LINKED TO	42 -29 -28	
EXPOSURE	151 98 167	
WEIGHTED	162 158 336	
NODE NO.	42 TOTAL LINKS	13
X,Y,Z COORDINATE	84° 63° 290	
LINKED TO	27 58 62 39 49 61 24 -29 -49 -29	
LINKED TO	-49 -28 -45	
EXPOSURE	113 158 169 65 64 185 32 218 202 104	
EXPOSURE	227 169 123	
WEIGHTED	222 310 340 132 65 372 66 438 2090 210	
WEIGHTED	2230 360 124	
NODE NO.	45 TOTAL LINKS	6
X,Y,Z COORDINATE	113° 66° 300	
LINKED TO	39 48 41 -45 -46 -50	
EXPOSURE	65 15 31 197 120 188	
WEIGHTED	172 12 64 198 121 1890	
NODE NO.	48 TOTAL LINKS	8
X,Y,Z COORDINATE	120° 66° 300	
LINKED TO	61 54 50 -46 -32 -48 -45 -31	
EXPOSURE	129 21 24 137 126 17 55 73	
WEIGHTED	290 82 60 270 259 98 203 166	

Table A.4. (cont'd)

NODE NO.	SC TOTAL LINKS	6
X,Y,Z COORDINATE	103° 68° 300	
LINKED TO	53 60 54	-98 -31 -32
EXPOSURE	100 90 98	132 135 96
WEIGHTED	101 102 99	133 172 134
NODE NO.	SA TOTAL LINKS	5
X,Y,Z COORDINATE	134° 76° 310	
LINKED TO	53 -48 -46	-55 -57
EXPOSURE	45 110 69	169 168
WEIGHTED	112 222 70	170 165
NODE NO.	-46 TOTAL LINKS	4
X,Y,Z COORDINATE	122° 75° 330	
LINKED TO	61 -45 -51	-55
EXPOSURE	91 124 219	171
WEIGHTED	920 250 2200	172
NODE NO.	-55 TOTAL LINKS	2
X,Y,Z COORDINATE	135° 90° 370	
LINKED TO	69 63 53	73 -57 -58
EXPOSURE	103 102 32	59 258 272
WEIGHTED	1540 206 66	120 518 273
NODE NO.	53 TOTAL LINKS	3
X,Y,Z COORDINATE	144° 76° 300	
LINKED TO	63 -48 -57	
EXPOSURE	61 100 186	
WEIGHTED	62 101 187	
NODE NO.	63 TOTAL LINKS	4
X,Y,Z COORDINATE	150° 51° 360	
LINKED TO	73 -57 -61	-58
EXPOSURE	26 242 157	170
WEIGHTED	27 243 316	342
NODE NO.	73 TOTAL LINKS	6
X,Y,Z COORDINATE	150° 105° 260	
LINKED TO	82 -65 -61	-67 -58 -57
EXPOSURE	35 348 181	262 171 151
WEIGHTED	36 652 182	2630 172 152
NODE NO.	82 TOTAL LINKS	5
X,Y,Z COORDINATE	149° 115° 340	
LINKED TO	93 -77 -69	-76 -67
EXPOSURE	64 211 314	145 242
WEIGHTED	65 212 315	166 243
NODE NO.	93 TOTAL LINKS	4
X,Y,Z COORDINATE	147° 132° 330	
LINKED TO	103 -77 -92	-76
EXPOSURE	31 280 160	183
WEIGHTED	64 562 161	1840
NODE NO.	103 TOTAL LINKS	6
X,Y,Z COORDINATE	146° 146° 320	
LINKED TO	90 63 -92	-87 -77 -76
EXPOSURE	115 55 176	296 224 215
WEIGHTED	1160 560 177	494 225 2160
NODE NO.	-92 TOTAL LINKS	7
X,Y,Z COORDINATE	146° 143° 330	
LINKED TO	90 63 88	-87 -77 -76 -93
EXPOSURE	103 100 164	295 250 238 179
WEIGHTED	1040 1010 650	592 251 2350 180
NODE NO.	-83 TOTAL LINKS	4
X,Y,Z COORDINATE	115° 144° 330	
LINKED TO	90 -75 -87	-81
EXPOSURE	125 263 324	162
WEIGHTED	1260 254 650	326
NODE NO.	-85 TOTAL LINKS	3
X,Y,Z COORDINATE	104° 137° 330	
LINKED TO	88 92	-81
EXPOSURE	296 156 356	
WEIGHTED	2970 157 3590	
NODE NO.	92 TOTAL LINKS	9
X,Y,Z COORDINATE	91° 129° 300	
LINKED TO	91 86 99	80 -81 -78 -50 -75
EXPOSURE	253 281 96	208 315 295 196 239
WEIGHTED	762 282 48500	62700 156000 29600 59700 24000

Case 4 - Area 1, Route 2, Sensor Set 2.

Table A.5. Case 4 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
31	770	10150	35	164	1470	10500
35	1470	10500	-24	165	2450	5590
-24	2450	5590	-22	177	3290	5240
-22	3290	5240	32	145	2590	10290
32	2590	10290	30	220	1610	10010
30	1610	10010	28	230	560	5800
28	560	9800	34	185	770	10430
34	770	10430	45	34	70	11480
45	70	11480	55	205	560	12390
55	560	12390	-33	153	2660	10520
-33	2660	10920	51	337	2660	11760
51	2660	11760	57	198	2940	12670
57	2940	12670	67	192	3850	13650
67	3850	13650	76	334	3920	14420
76	3920	14420	-73	102	4550	15120
-73	4550	15120	-78	261	5390	15890
-78	5390	15890	-90	281	5390	16660
-90	5390	16660	89	320	6370	16030
89	6370	16030	99	270	5810	17010
99	5810	17010	91	604	6020	16030
91	6020	16030	94	566	5250	16450
94	5250	16450	104	128	4760	17290
104	4760	17290	102	2	3710	17220
102	3710	17220	100	2	2660	17080
100	2660	17080	93	14	1610	16450
53	1610	16450	84	2	1120	15400
84	1120	15400	85	101	1120	15540
85	1120	15540	97	32	580	16590
97	980	16590	86	202	770	15890
86	770	15690	98	1	1750	16870
98	1750	16870	81	46	490	15190
81	490	15150	95	29	2240	16450
95	2240	16450	-66	177	3080	16590
-86	3080	16590	-88	296	3430	16590
-98	3430	16590	-69	167	4480	16660
-89	4480	16660	87	340	3590	15960
87	3990	15960	-65	290	4270	14350
-65	4270	14350	-56	408	3290	13300
-56	3290	13300	-63	274	3290	14280
-63	3290	14280	-74	274	3430	15120
-74	3430	15120	-82	309	3360	16030
-82	3360	16030	-59	462	1540	13930
-59	1540	13930	-71	284	1750	14910
-71	1750	14910	-53	240	2310	13160
-53	2310	13160	-43	302	2240	12180
-43	2240	12160	46	374	1750	11480
46	1750	11480	56	200	2100	12390
56	2100	12390	64	234	2100	13370
64	2100	13370	75	215	3150	14420
75	3150	14420	-72	450	2450	15050
-72	2450	15050	65	217	3080	13510
65	3080	13510	-64	494	2240	14260
-64	2240	14260	-83	274	2870	16100
-63	2870	16100	101	98	6720	17150
101	6720	17150	-93	307	8050	17080
-93	8050	17080	-87	325	8890	16590
-87	8890	16590	96	340	9450	16450

Table A.6. Case 4 - Node Linkage

NODE NO.	31	TOTAL LINKS	7
X,Y,Z COORDINATE	11°	45°	280
LINKED TO	34	28	35
EXPOSURE	201	158	81
WEIGHTED	202	318	164
NODE NO.	35	TOTAL LINKS	8
X,Y,Z COORDINATE	21°	50°	280
LINKED TO	30	34	46
EXPOSURE	193	178	237
WEIGHTED	388	358	238
NODE NO.	-24	TOTAL LINKS	7
X,Y,Z COORDINATE	35°	37°	290
LINKED TO	29	12	18
EXPOSURE	243	155	178
WEIGHTED	486	196	356
NODE NO.	-22	TOTAL LINKS	6
X,Y,Z COORDINATE	47°	32°	260
LINKED TO	18	24	20
EXPOSURE	453	211	171
WEIGHTED	508	424	172
NODE NO.	32	TOTAL LINKS	5
X,Y,Z COORDINATE	37°	47°	280
LINKED TO	25	30	33
EXPOSURE	243	109	314
WEIGHTED	488	220	315
NODE NO.	30	TOTAL LINKS	6
X,Y,Z COORDINATE	23°	43°	220
LINKED TO	34	28	23
EXPOSURE	157	114	303
WEIGHTED	316	270	606
NODE NO.	28	TOTAL LINKS	3
X,Y,Z COORDINATE	8°	40°	280
LINKED TO	34	-21	-23
EXPOSURE	164	236	203
WEIGHTED	185	474	204
NODE NO.	34	TOTAL LINKS	3
X,Y,Z COORDINATE	11°	49°	280
LINKED TO	45	-18	-23
EXPOSURE	33	297	119
WEIGHTED	34	298	120
NODE NO.	45	TOTAL LINKS	3
X,Y,Z COORDINATE	1°	64°	300
LINKED TO	55	-38	-42
EXPOSURE	204	225	255
WEIGHTED	205	207	256
NODE NO.	55	TOTAL LINKS	16
X,Y,Z COORDINATE	8°	77°	340
LINKED TO	70	46	56
LINKED TO	-43	-59	-53
EXPOSURE	254	192	213
EXPOSURE	209	263	242
WEIGHTED	255	183	428
WEIGHTED	420	264	486
NODE NO.	-33	TOTAL LINKS	6
X,Y,Z COORDINATE	78°	56°	300
LINKED TO	51	29	46
EXPOSURE	136	201	274
WEIGHTED	137	404	550
NODE NO.	51	TOTAL LINKS	7
X,Y,Z COORDINATE	78°	49°	300
LINKED TO	56	46	57
EXPOSURE	288	162	197
WEIGHTED	578	326	198

Table A.6. (cont'd.)

NODE NO.	57	TOTAL LINKS	9
X,Y,Z COORDINATE	42°	81°	300
LINKED TO	59	65	56
EXPOSURE	279	284	253
WEIGHTED	560	285	508
NODE NO.	57	TOTAL LINKS	9
X,Y,Z COORDINATE	55°	95°	300
LINKED TO	76	65	59
EXPOSURE	333	264	256
WEIGHTED	334	570	514
NODE NO.	76	TOTAL LINKS	7
X,Y,Z COORDINATE	56°	106°	320
LINKED TO	75	68	65
EXPOSURE	296	229	197
WEIGHTED	794	2250	395
NODE NO.	-73	TOTAL LINKS	6
X,Y,Z COORDINATE	65°	116°	330
LINKED TO	77	87	65
EXPOSURE	306	307	361
WEIGHTED	3070	616	724
NODE NO.	-78	TOTAL LINKS	7
X,Y,Z COORDINATE	77°	127°	320
LINKED TO	94	91	89
EXPOSURE	314	290	192
WEIGHTED	630	582	386
NODE NO.	-50	TOTAL LINKS	4
X,Y,Z COORDINATE	77°	138°	310
LINKED TO	91	85	89
EXPOSURE	301	159	355
WEIGHTED	604	320	712
NODE NO.	99	TOTAL LINKS	6
X,Y,Z COORDINATE	51°	129°	300
LINKED TO	91	59	90
EXPOSURE	301	134	205
WEIGHTED	604	270	2100
NODE NO.	59	TOTAL LINKS	2
X,Y,Z COORDINATE	93°	143°	300
LINKED TO	91	-85	
EXPOSURE	301	454	
WEIGHTED	604	4950	
NODE NO.	91	TOTAL LINKS	2
X,Y,Z COORDINATE	86°	129°	300
LINKED TO	94	-75	
EXPOSURE	282	298	
WEIGHTED	566	598	
NODE NO.	94	TOTAL LINKS	3
X,Y,Z COORDINATE	75°	135°	310
LINKED TO	104	-66	-87
EXPOSURE	63	379	335
WEIGHTED	128	760	680
NODE NO.	104	TOTAL LINKS	2
X,Y,Z COORDINATE	65°	147°	300
LINKED TO	102	-89	
EXPOSURE	0	362	
WEIGHTED	2	726	
NODE NO.	102	TOTAL LINKS	6
X,Y,Z COORDINATE	53°	146°	300
LINKED TO	100	-88	-86
EXPOSURE	0	345	195
WEIGHTED	2	692	392

Table A.6.(cont'd.)

NODE NO.	100	TOTAL LINKS	7
X,Y,Z COORDINATE	38	144	300
LINKED TO	95	58	93
EXPOSURE	101	53	6
WEIGHTED	204	108	14
NODE NO.	93	TOTAL LINKS	8
X,Y,Z COORDINATE	23	135	300
LINKED TO	98	55	97
EXPOSURE	100	53	71
WEIGHTED	101	188	104
NODE NO.	84	TOTAL LINKS	7
X,Y,Z COORDINATE	16	120	300
LINKED TO	85	86	81
EXPOSURE	100	58	52
WEIGHTED	101	116	106
NODE NO.	85	TOTAL LINKS	7
X,Y,Z COORDINATE	16	122	300
LINKED TO	86	81	97
EXPOSURE	100	66	16
WEIGHTED	202	134	32
NODE NO.	97	TOTAL LINKS	3
X,Y,Z COORDINATE	14	137	300
LINKED TO	86	-24	-79
EXPOSURE	100	227	186
WEIGHTED	202	456	374
NODE NO.	86	TOTAL LINKS	4
X,Y,Z COORDINATE	11	127	300
LINKED TO	81	98	-84
EXPOSURE	92	0	277
WEIGHTED	182	1	556
NODE NO.	98	TOTAL LINKS	11
X,Y,Z COORDINATE	25	141	300
LINKED TO	81	-75	-83
LINKED TO	-74	-83	-86
EXPOSURE	22	286	290
EXPOSURE	219	-	-
WEIGHTED	46	287	562
WEIGHTED	440	-	-
NODE NO.	81	TOTAL LINKS	14
X,Y,Z COORDINATE	7	117	300
LINKED TO	70	55	64
LINKED TO	-64	-54	-52
EXPOSURE	232	28	191
EXPOSURE	242	213	195
WEIGHTED	466	29	192
WEIGHTED	486	214	392
NODE NO.	95	TOTAL LINKS	15
X,Y,Z COORDINATE	32	135	310
LINKED TO	87	75	-75
LINKED TO	-74	-51	-84
EXPOSURE	235	217	273
EXPOSURE	252	205	212
WEIGHTED	472	218	546
WEIGHTED	506	412	426
NODE NO.	-86	TOTAL LINKS	4
X,Y,Z COORDINATE	44	137	340
LINKED TO	87	-88	-83
EXPOSURE	169	295	315
WEIGHTED	340	256	632
NODE NO.	-88	TOTAL LINKS	6
X,Y,Z COORDINATE	49	137	340
LINKED TO	87	-82	-83
EXPOSURE	212	351	302
WEIGHTED	426	704	606
NODE NO.	-89	TOTAL LINKS	2
X,Y,Z COORDINATE	64	138	330
LINKED TO	87	-20	-
EXPOSURE	169	283	-
WEIGHTED	340	568	-

Table A.6. (cont'd.)

NODE NO.	87	TOTAL LINKS	19
X,Y,Z COORDINATE	57° 128° 330		
LINKED TO	75 77 78 71	-62 -80 -74 -83 -75 -65	
EXPOSURE	276 257 247 234	351 338 330 319 303 285	
WEIGHTED	554 2520 496 2350	708 678 662 640 608 290	
WEIGHTED	584 556 510 526		
NODE NO.	-65	TOTAL LINKS	5
X,Y,Z COORDINATE	61° 135° 320		
LINKED TO	68 77 -63 -74	-56	
EXPOSURE	314 304 318 313	203	
WEIGHTED	3150 610 638 628	408	
NODE NO.	-56	TOTAL LINKS	5
X,Y,Z COORDINATE	47° 90° 310		
LINKED TO	65 59 -63 -53	-64	
EXPOSURE	292 258 273 252	246	
WEIGHTED	586 512 274 506	494	
NODE NO.	-63	TOTAL LINKS	5
X,Y,Z COORDINATE	47° 104° 330		
LINKED TO	75 65 -74 -64	-72	
EXPOSURE	316 229 273 255	244	
WEIGHTED	638 420 274 512	493	
NODE NO.	-74	TOTAL LINKS	4
X,Y,Z COORDINATE	49° 116° 340		
LINKED TO	75 -62 -72 -83		
EXPOSURE	269 306 281 239		
WEIGHTED	540 309 564 480		
NODE NO.	-82	TOTAL LINKS	10
X,Y,Z COORDINATE	46° 129° 350		
LINKED TO	75 77 -83 -86	-72 -79 -71 -64 -75 -59	
EXPOSURE	275 223 302 305	308 279 265 277 273 230	
WEIGHTED	560 2348 686 612	618 560 532 556 546 462	
NODE NO.	-89	TOTAL LINKS	8
X,Y,Z COORDINATE	22° 99° 350		
LINKED TO	64 70 -59 -64	-71 -68 -58 -52	
EXPOSURE	296 262 322 343	283 244 193 283	
WEIGHTED	494 526 602 344	284 490 388 428	
NODE NO.	-71	TOTAL LINKS	15
X,Y,Z COORDINATE	25° 117° 350		
LINKED TO	75 64 70 65	55 -72 -64 -79 -68 -73	
LINKED TO	-54 -53 -66 -52	-91	
EXPOSURE	271 245 220 226	109 309 336 273 245 263	
EXPOSURE	237 229 216 202	181	
WEIGHTED	500 246 456 459	386 620 614 274 452 264	
WEIGHTED	476 240 439 466	364	
NODE NO.	-93	TOTAL LINKS	4
X,Y,Z COORDINATE	33° 85° 330		
LINKED TO	60 56 65 -43		
EXPOSURE	303 174 192 150		
WEIGHTED	480 390 366 302		
NODE NO.	-43	TOTAL LINKS	4
X,Y,Z COORDINATE	32° 74° 310		
LINKED TO	56 66 -44 -54		
EXPOSURE	267 186 217 222		
WEIGHTED	526 374 436 446		
NODE NO.	45	TOTAL LINKS	4
X,Y,Z COORDINATE	25° 64° 300		
LINKED TO	56 -34 -44 -38		
EXPOSURE	199 234 253 138		
WEIGHTED	200 470 508 278		
NODE NO.	56	TOTAL LINKS	2
X,Y,Z COORDINATE	30° 77° 310		
LINKED TO	60 -44 -54		
EXPOSURE	233 223 220		
WEIGHTED	234 448 442		

Table A.6. (cont'd.)

NODE NO.	64	TOTAL LINKS	4
X,Y,Z COORDINATE	30,	91,	330
LINKED TO	65	75	-54
EXPOSURE	260	218	322
WEIGHTED	522	219	646
NODE NO.	75	TOTAL LINKS	3
X,Y,Z COORDINATE	45,	106,	330
LINKED TO	65	-64	-72
EXPOSURE	273	318	240
WEIGHTED	548	628	490
NODE NO.	-72	TOTAL LINKS	6
X,Y,Z COORDINATE	35,	115,	350
LINKED TO	65	70	-64
EXPOSURE	228	229	345
WEIGHTED	229	460	692
NODE NO.	65	TOTAL LINKS	2
X,Y,Z COORDINATE	44,	93,	310
LINKED TO	59	-64	
EXPOSURE	289	246	
WEIGHTED	580	454	
NODE NO.	-64	TOTAL LINKS	9
X,Y,Z COORDINATE	32,	104,	350
LINKED TO	70	59	-54
EXPOSURE	250	244	286
WEIGHTED	502	450	574
NODE NO.	-83	TOTAL LINKS	28
X,Y,Z COORDINATE	41,	130,	350
LINKED TO	77	69	70
LINKED TO	60	62	52
LINKED TO	-54	-52	-40
EXPOSURE	273	266	216
EXPOSURE	169	183	167
EXPOSURE	232	204	206
WEIGHTED	2700	2670	434
WEIGHTED	1850	1890	1680
WEIGHTED	466	410	207
NODE NO.	101	TOTAL LINKS	6
X,Y,Z COORDINATE	56,	145,	300
LINKED TO	88	90	83
EXPOSURE	306	271	259
WEIGHTED	3070	2720	2600
NODE NO.	-93	TOTAL LINKS	4
X,Y,Z COORDINATE	115,	144,	330
LINKED TO	90	-65	-87
EXPOSURE	194	255	324
WEIGHTED	1550	512	325
NODE NO.	-87	TOTAL LINKS	6
X,Y,Z COORDINATE	127,	137,	340
LINKED TO	96	90	28
EXPOSURE	239	252	182
WEIGHTED	340	126500	91500
			17200
			69300
			21000

Case 5 - Area 2, Route 1, Sensor Set 1.

Table A.7. Case 5 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
3	3620	7280	9	1	4870	7630
9	4670	7630	13	1	4450	8470
13	4450	8470	7	50	5290	7630
7	5290	7630	-2	40	4240	7280
-2	4240	7280	11	202	4100	7980
11	4100	7980	31	17	2560	5670
31	2560	5670	37	2	3470	10640
17	3470	10640	32	37	4240	10080
32	4240	10080	36	52	5290	10640
16	5290	10640	35	160	4730	10430
35	4730	10430	46	54	5500	11270
46	5500	11270	36	105	6340	10710
36	6340	10710	33	36	5600	10150
33	5600	10150	-21	56	5010	9100
-21	5010	9100	12	34	5430	8190
12	5430	8190	22	38	5570	9170
22	5570	9170	26	90	3610	5660
26	3610	5660	19	60	4100	9100
19	4100	9100	-23	72	3120	9240
-23	3120	9240	23	3	4170	9240
23	4170	9240	42	34	2980	11060
42	2980	11060	34	64	2280	10360
34	2280	10360	56	46	2630	12320
56	2630	12320	50	29	3260	11550
50	3260	11550	57	116	3690	12390
57	3690	12390	-62	2	2640	13090
-62	2640	13090	70	166	2210	14000
70	2210	14000	82	68	2560	14510
62	2560	14510	-76	238	2510	14420
-76	2510	14420	-71	492	2700	13720
-71	2700	13720	-52	62	4660	11830
-62	4660	11830	45	52	5150	11270
45	5150	11270	65	10	7180	13230
65	7180	13230	71	20	6020	14140
71	6020	14140	79	64	6790	14560
79	6790	14560	61	190	9560	14770

Table A.8. Case 5 - Node Linkage

NODE NO.	3 TOTAL LINKS			5		
X,Y,Z COORDINATE	25	41	59	350		
LINKED TO	11	8	9	-2	-1	
EXPOSURE	75	148	0	148	206	
WEIGHTED	152	298	1	149	214	
NODE NO.	9 TOTAL LINKS			5		
X,Y,Z COORDINATE	41	59	290			
LINKED TO	7	12	11	13	-2	
EXPOSURE	147	75	65	0	137	
WEIGHTED	148	152	132	1	276	
NODE NO.	13 TOTAL LINKS			6		
X,Y,Z COORDINATE	25	21	290			
LINKED TO	11	19	23	12	7	-21
EXPOSURE	124	79	67	53	24	156
WEIGHTED	250	90	88	54	50	314
NODE NO.	7 TOTAL LINKS			4		
X,Y,Z COORDINATE	47	9	300			
LINKED TO	12	-10	-2	-12		
EXPOSURE	100	234	19	210		
WEIGHTED	202	235	40	219		
NODE NO.	-2 TOTAL LINKS			2		
X,Y,Z COORDINATE	32	4	310			
LINKED TO	11	-1				
EXPOSURE	100	176				
WEIGHTED	202	274				
NODE NO.	11 TOTAL LINKS			21		
X,Y,Z COORDINATE	30	14	300			
LINKED TO	19	23	8	12	18	-28
LINKED TO	-1	-21	-23	-26	-3	-18
LINKED TO	-27					
EXPOSURE	91	98	185	92	95	69
EXPOSURE	195	134	91	278	209	217
EXPOSURE	244					
WEIGHTED	180	198	372	93	96	65
WEIGHTED	192	278	92	598	928	436
WEIGHTED	490					
NODE NO.	31 TOTAL LINKS			6		
X,Y,Z COORDINATE	2	41	300			
LINKED TO	34	19	28	37	-24	-23
EXPOSURE	100	64	19	0	225	80
WEIGHTED	101	130	20	2	452	81
NODE NO.	37 TOTAL LINKS			7		
X,Y,Z COORDINATE	21	52	300			
LINKED TO	42	40	37	28	-40	-41
EXPOSURE	100	40	36	28	255	182
WEIGHTED	202	92	37	58	512	366
WEIGHTED						198
NODE NO.	32 TOTAL LINKS			9		
X,Y,Z COORDINATE	32	44	300			
LINKED TO	35	28	23	19	36	-26
EXPOSURE	116	92	79	39	25	308
WEIGHTED	234	126	150	80	52	309
WEIGHTED						410
WEIGHTED						132
NODE NO.	36 TOTAL LINKS			12		
X,Y,Z COORDINATE	47	52	300			
LINKED TO	35	75	45	46	38	-47
LINKED TO	-27	-26				
EXPOSURE	159	85	160	110	101	166
EXPOSURE	250	231				
WEIGHTED	318	160	322	238	1820	1670
WEIGHTED	502	664				
WEIGHTED						1610
NODE NO.	35 TOTAL LINKS			7		
X,Y,Z COORDINATE	39	46	300			
LINKED TO	35	42	46	-41	-26	-40
EXPOSURE	111	123	26	268	304	223
WEIGHTED	112	208	56	530	610	448
WEIGHTED						235
NODE NO.	46 TOTAL LINKS			9		
X,Y,Z COORDINATE	50	61	320			
LINKED TO	45	47	36	-43	-33	-39
EXPOSURE	100	134	104	141	122	109
WEIGHTED	202	1370	105	1442	1420	123
WEIGHTED						350
WEIGHTED						310

Table A.8. (cont'd.)

NODE NO.	38	TOTAL LINKS	A
X,Y,Z COORDINATE	62°	53°	340
LINKED TO	47	33	27
EXPOSURE	195	17	246
WEIGHTED	392	36	494
	466	546	402
	546	402	321
	402	321	476
	321	476	
NODE NO.	33	TOTAL LINKS	B
X,Y,Z COORDINATE	50°	45°	330
LINKED TO	22	-27	-52
EXPOSURE	49	337	291
WEIGHTED	100	476	292
	574	374	56
	374	56	300
	56	300	336
NODE NO.	-21	TOTAL LINKS	C
X,Y,Z COORDINATE	43°	30°	330
LINKED TO	22	23	19
EXPOSURE	159	48	19
WEIGHTED	159	58	40
	34	662	502
	662	502	
NODE NO.	12	TOTAL LINKS	D
X,Y,Z COORDINATE	49°	17°	300
LINKED TO	22	-12	-10
EXPOSURE	18	315	304
WEIGHTED	38	315	305
	456		
NODE NO.	22	TOTAL LINKS	E
X,Y,Z COORDINATE	51°	31°	330
LINKED TO	27	15	23
LINKED TO	-26	-12	-32
LINKED TO	-41	-49	-36
EXPOSURE	307	287	74
EXPOSURE	314	290	301
EXPOSURE	189	174	260
WEIGHTED	308	298	150
WEIGHTED	630	582	604
WEIGHTED	558	418	508
WEIGHTED	262	276	2900
WEIGHTED	2900	384	
	384		
NODE NO.	28	TOTAL LINKS	F
X,Y,Z COORDINATE	23°	36°	300
LINKED TO	23	19	18
EXPOSURE	125	89	95
WEIGHTED	126	60	192
	392		
NODE NO.	19	TOTAL LINKS	G
X,Y,Z COORDINATE	30°	30°	290
LINKED TO	23	-26	-23
EXPOSURE	100	260	35
WEIGHTED	202	522	72
	80		
NODE NO.	-23	TOTAL LINKS	H
X,Y,Z COORDINATE	16°	32°	310
LINKED TO	18	23	-24
EXPOSURE	119	2	154
WEIGHTED	240	3	310
	154	376	
	376		
NODE NO.	23	TOTAL LINKS	I
X,Y,Z COORDINATE	31°	32°	300
LINKED TO	18	8	42
LINKED TO	-91	-26	-20
LINKED TO	-92	-41	-24
EXPOSURE	87	137	33
EXPOSURE	219	175	272
EXPOSURE	104	169	276
WEIGHTED	196	276	34
WEIGHTED	440	248	273
WEIGHTED	458	458	264
WEIGHTED	264	530	249
WEIGHTED	530	249	241
WEIGHTED	241	360	380
WEIGHTED	360	380	
WEIGHTED	380		
NODE NO.	42	TOTAL LINKS	J
X,Y,Z COORDINATE	14°	58°	300
LINKED TO	50	52	34
EXPOSURE	130	73	31
WEIGHTED	202	78	64
	308	266	178
	266	178	198
	178	198	
	198		
NODE NO.	34	TOTAL LINKS	K
X,Y,Z COORDINATE	4°	48°	300
LINKED TO	52	18	50
LINKED TO	-48	-13	-13
EXPOSURE	61	79	58
EXPOSURE	122	62	
WEIGHTED	124	160	119
WEIGHTED	246	126	
	68	118	109
	118	109	183
	109	183	416
	183	416	978
	416	978	912
	978	912	
	912		
NODE NO.	-56	TOTAL LINKS	L
X,Y,Z COORDINATE	5°	76°	300
LINKED TO	52	50	-62
EXPOSURE	100	28	160
WEIGHTED	202	29	322
	230	198	
	198		

Table A.8. (cont'd.)

NODE NO.	50	TOTAL LINKS	4
X,Y,Z COORDINATE	18°	65°	300
LINKED TO	52	57	-48 -40
EXPOSURE	100	58	151 192
WEIGHTED	202	118	304 193
NODE NO.	57	TOTAL LINKS	6
X,Y,Z COORDINATE	27°	77°	330
LINKED TO	60	-59	-48 -52 -64 -62
EXPOSURE	101	100	75 48 205 0
WEIGHTED	204	202	152 49 2100 2
NODE NO.	-62	TOTAL LINKS	3
X,Y,Z COORDINATE	12°	87°	350
LINKED TO	70	-71	-59
EXPOSURE	82	279	165
WEIGHTED	166	280	332
NODE NO.	70	TOTAL LINKS	3
X,Y,Z COORDINATE	3°	100°	330
LINKED TO	82	-71	-76
EXPOSURE	87	279	175
WEIGHTED	88	560	1760
NODE NO.	82	TOTAL LINKS	6
X,Y,Z COORDINATE	8°	113°	330
LINKED TO	95	84	96 -76 -78 -74
EXPOSURE	142	145	90 237 192 219
WEIGHTED	286	1460	916 238 1930 2200
NODE NO.	-76	TOTAL LINKS	4
X,Y,Z COORDINATE	13°	106°	340
LINKED TO	69	-78	-74 -71
EXPOSURE	96	242	279 245
WEIGHTED	570	2430	2800 492
NODE NO.	-71	TOTAL LINKS	13
X,Y,Z COORDINATE	10°	94°	350
LINKED TO	75	84	52 72 60 -74 -78 -59 -64 -67
LINKED TO	-79	-48	-52
EXPOSURE	199	200	93 167 102 253 231 149 223 305
EXPOSURE	152	75	61
WEIGHTED	2000	2010	88 1680 1030 2540 2320 150 446 3060
WEIGHTED	1530	76	62
NODE NO.	-52	TOTAL LINKS	6
X,Y,Z COORDINATE	28°	69°	350
LINKED TO	45	60	59 -48 -41 -40
EXPOSURE	81	154	177 147 182 138
WEIGHTED	62	310	1760 296 378 270
NODE NO.	45	TOTAL LINKS	20
X,Y,Z COORDINATE	45°	61°	340
LINKED TO	47	59	60 27 65 -41 -53 -43 -40 -39
LINKED TO	-48	-32	-26 -27 -54 -37 -60 -64 -61 -59
EXPOSURE	188	213	122 211 4 211 125 191 186 183
EXPOSURE	116	242	229 233 311 250 321 225 211 65
WEIGHTED	1890	2140	246 212 10 424 1300 1920 378 184
WEIGHTED	258	243	450 468 3120 251 3220 452 3120 132
NODE NO.	65	TOTAL LINKS	9
X,Y,Z COORDINATE	74°	89°	330
LINKED TO	64	73	71 55 -66 -61 -56 -60 -68 -54
EXPOSURE	53	47	19 37 137 344 211 325 297
WEIGHTED	54	48	20 380 138 690 2120 652 2980
NODE NO.	71	TOTAL LINKS	6
X,Y,Z COORDINATE	86°	102°	300
LINKED TO	80	73	75 64 -65 -66
EXPOSURE	100	67	95 52 91 96
WEIGHTED	101	126	66 330 92 970
NODE NO.	79	TOTAL LINKS	10
X,Y,Z COORDINATE	97°	108°	300
LINKED TO	81	67	77 80 75 53 66 -62 -69 -61
EXPOSURE	189	74	100 91 345 276 0 300 94 243
WEIGHTED	190	22500	14100 64400 103000 27700 300 903 47500 122000

Case 6 - Area 2, Route 2, Sensor Set 1.

Table A.9. Case 6 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
35	2770	10500	28	1	3610	9660
28	3610	9660	19	77	4100	9100
19	4100	9100	31	66	4240	10080
31	4240	10080	36	1P	5290	10640
36	5290	10640	34	180	4730	10430
34	4730	10430	46	54	5500	11270
46	5500	11270	38	105	6340	10710
38	6340	10710	32	36	5500	10150
32	5500	10150	-21	56	5010	9100
-21	5010	9100	11	74	5430	8190
11	5430	8190	12	10	4450	8470
12	4450	8470	22	96	4170	9240
22	4170	9240	42	51	2980	11060
42	2980	11060	33	64	2280	10360
33	2280	10360	-45	59	2070	11410
-45	2070	11410	56	2	2630	12320
56	2630	12320	50	29	3260	11550
50	3260	11550	37	46	3470	10640
37	3470	10640	30	2	2560	9870
30	2560	9870	15	2	2580	5030
15	2560	9030	9	7	4870	7630
9	4870	7630	10	2	4100	7980
10	4100	7960	-23	57	3120	9240
-23	3120	9240	-2	52	4240	7280
-2	4240	7280	7	1	5290	7630
7	5290	7630	-13	36	3190	8400
-13	3190	8400	-24	216	2280	9240
-24	2280	9240	-1	116	3190	7280
-1	3190	7280	8	252	2840	7630
8	2840	7630	52	44	2770	11760
52	2770	11760	57	156	3890	12390
57	3890	12390	-62	2	2840	11090
-62	2840	11090	70	166	2210	14000
70	2210	14000	81	68	2560	14510
81	2560	14510	-76	238	2910	14420
-76	2910	14420	-71	492	2700	13720
-71	2700	13720	-52	48	4660	11830
-52	4660	11830	45	82	5150	11270
45	5150	11270	65	10	7150	13230
65	7180	13230	71	20	8020	14140
71	8020	14140	79	66	6790	14560
79	6790	14560	66	1	9840	13510
46	9840	13510	61	48	10260	12670
61	10260	12670	67	1	9280	13720
67	9280	13720	-58	2	9840	12880
-58	9840	12880	69	91	10690	13860
69	10690	13860	62	2	10680	12810
62	10680	12810	68	56	11590	13660
68	11590	13660	76	41	10610	14420
76	10610	14420	84	246	10960	14980

Table A.10. Case 6 - Node Linkage

NODE NO.	35	TOTAL LINKS	8
X,Y,Z COORDINATE	11°	50°	300
LINKED TO	33	42	30
EXPOSURE	100	86	77
WEIGHTED	202	174	156
NODE NO.	28	TOTAL LINKS	7
X,Y,Z COORDINATE	21°	38°	300
LINKED TO	22	19	31
EXPOSURE	134	76	121
WEIGHTED	135	77	249
NODE NO.	19	TOTAL LINKS	7
X,Y,Z COORDINATE	30°	30°	290
LINKED TO	22	12	31
EXPOSURE	114	43	32
WEIGHTED	234	68	66
NODE NO.	31	TOTAL LINKS	8
X,Y,Z COORDINATE	32°	44°	300
LINKED TO	34	22	37
EXPOSURE	100	62	45
WEIGHTED	202	126	92
NODE NO.	36	TOTAL LINKS	12
X,Y,Z COORDINATE	47°	52°	300
LINKED TO	32	34	45
LINKED TO	-27	-26	
EXPOSURE	158	69	160
EXPOSURE	250	231	
WEIGHTED	318	180	322
WEIGHTED	502	464	
NODE NO.	34	TOTAL LINKS	7
X,Y,Z COORDINATE	35°	49°	300
LINKED TO	32	45	46
EXPOSURE	111	123	26
WEIGHTED	112	248	54
NODE NO.	46	TOTAL LINKS	9
X,Y,Z COORDINATE	51°	51°	320
LINKED TO	45	47	35
EXPOSURE	100	126	104
WEIGHTED	202	1370	105
NODE NO.	38	TOTAL LINKS	8
X,Y,Z COORDINATE	52°	53°	340
LINKED TO	47	72	27
EXPOSURE	155	17	246
WEIGHTED	392	36	494
NODE NO.	32	TOTAL LINKS	8
X,Y,Z COORDINATE	50°	45°	330
LINKED TO	21	-27	-32
EXPOSURE	49	327	291
WEIGHTED	100	576	292
NODE NO.	-21	TOTAL LINKS	6
X,Y,Z COORDINATE	43°	30°	330
LINKED TO	21	12	22
EXPOSURE	158	33	48
WEIGHTED	159	66	98
NODE NO.	11	TOTAL LINKS	7
X,Y,Z COORDINATE	49°	17°	300
LINKED TO	7	5	21
EXPOSURE	116	53	76
WEIGHTED	134	108	154
NODE NO.	12	TOTAL LINKS	5
X,Y,Z COORDINATE	35°	21°	290
LINKED TO	10	22	9
EXPOSURE	116	57	70
WEIGHTED	134	98	142

Table A.10. (cont'd.)

NODE NO.	22 TOTAL LINKS	30							
X,Y,Z COORDINATE	31. 32. 300								
LINKED TO	15 45 LINKED TO -20 EXPOSURE 110 EXPOSURE 112 EXPOSURE 273 WEIGHTED 222 WEIGHTED 226 WEIGHTED	10 47 -18 -1 -32 78 117 138 267 79 142 236 278 536	21 -26 -25 -13 -12 70 123 248 240 106 122 296 241	37 -27 -10 -32 52 60 297 216 240 181 189 290 366	30 -43 -35 -39 60 144 216 219 176 105 51 366	9 -41 -3 -42 144 50 76 173 100 51 154	7 -24 -3 -42 50 49 76 173 100 51 154	8 -24 -2 -43 50 49 76 173 100 51 154	62 33
NODE NO.	42 TOTAL LINKS	8							
X,Y,Z COORDINATE	14. 58. 300								
LINKED TO	50 100 WEIGHTED	37 67 68	52 73 74	33 31 64	-42 153 308	-45 132 266	-46 166 376	-46 98 198	
NODE NO.	33 TOTAL LINKS	3							
X,Y,Z COORDINATE	4. 44. 300								
LINKED TO	30 EXPOSURE 100 WEIGHTED	-42 154 155	-45 96 99						
NODE NO.	-45 TOTAL LINKS	3							
X,Y,Z COORDINATE	1. 63. 350								
LINKED TO	52 EXPOSURE 36 WEIGHTED	56 0 2	-42 194 398						
NODE NO.	56 TOTAL LINKS	4							
X,Y,Z COORDINATE	5. 76. 300								
LINKED TO	52 EXPOSURE 100 WEIGHTED	50 28 29	-62 160 322	-55 98 199					
NODE NO.	50 TOTAL LINKS	5							
X,Y,Z COORDINATE	18. 65. 300								
LINKED TO	52 EXPOSURE 100 WEIGHTED	37 22 46	57 58 318	-48 151 304	-40 192 193				
NODE NO.	37 TOTAL LINKS	4							
X,Y,Z COORDINATE	21. 52. 300								
LINKED TO	39 EXPOSURE 2 WEIGHTED	-40 266 524	-41 195 392	-48 110 222	-48				
NODE NO.	30 TOTAL LINKS	3							
X,Y,Z COORDINATE	8. 41. 300								
LINKED TO	15 EXPOSURE 2 WEIGHTED	-24 244 450	-23 38 39						
NODE NO.	15 TOTAL LINKS	14							
X,Y,Z COORDINATE	14. 25. 310								
LINKED TO	8 LINKED TO -2 EXPOSURE 155 EXPOSURE 48 WEIGHTED 312 WEIGHTED	10 -92 -40 55 6 132 109 176 60 7	9 -40 -41 6 132 130 173 266	-23 -20 -13 132 130 208 261 212 138 257	-13 -20 -24 -18 -26	-18 -21 -18 -26	-3 -1 -1	-26	
NODE NO.	4 TOTAL LINKS	3							
X,Y,Z COORDINATE	41. 5. 290								
LINKED TO	7 EXPOSURE 100 WEIGHTED	10 5 2	-2 120 242						
NODE NO.	10 TOTAL LINKS	15							
X,Y,Z COORDINATE	30. 14. 300								
LINKED TO	7 LINKED TO -10 EXPOSURE 68 EXPOSURE 231 WEIGHTED 69 WEIGHTED	8 -12 -24 169 87 135 237 176 240	21 -2 -20 119 121 237 235 246	-2 -13 -20 172 66 267 200 67	-1 -1 -27 172 66 267 200 67	-23 -26 -26	-3 -1	-16	
NODE NO.	-23 TOTAL LINKS	12							
X,Y,Z COORDINATE	16. 32. 310								
LINKED TO	6 LINKED TO -41 EXPOSURE 150 EXPOSURE 202 WEIGHTED	45 -2 75 30 348	-24 -13 220 124 276 272	-13 -18 -20 276 287 221	-26 -2 -27 287 221 133	-1 -1 -1	-40 -42	-42	
NODE NO.	20 TOTAL LINKS	14							
X,Y,Z COORDINATE	14. 32. 310								
LINKED TO	7 LINKED TO -41 EXPOSURE 150 EXPOSURE 202 WEIGHTED	8 -2 75 30 348	21 -2 220 124 276 272	-2 -13 -20 276 287 221	-1 -23 -26	-3 -1	-16	-16	

Table A.10. (cont'd.)

NODE NO.	-2 TOTAL LINKS	2
X,Y,Z COORDINATE	32, 7	4, -1
LINKED TO	32	310
EXPOSURE	0	236
WEIGHTED	1	474
NODE NO.	7 TOTAL LINKS	13
X,Y,Z COORDINATE	47, -21	9, 2
LINKED TO	21	15
LINKED TO	7	3
EXPOSURE	86	273
EXPOSURE	266	57
WEIGHTED	190	274
WEIGHTED	534	36
NODE NO.	-13 TOTAL LINKS	4
X,Y,Z COORDINATE	17, 8	20, -18
LINKED TO	17	-24
LINKED TO	20	-3
EXPOSURE	140	246
WEIGHTED	262	216
NODE NO.	-24 TOTAL LINKS	6
X,Y,Z COORDINATE	4, 8	32, -18
LINKED TO	8	-3
EXPOSURE	82	285
WEIGHTED	166	430
NODE NO.	-1 TOTAL LINKS	2
X,Y,Z COORDINATE	17, 8	4, -3
LINKED TO	17	171
WEIGHTED	292	344
NODE NO.	8 TOTAL LINKS	23
X,Y,Z COORDINATE	12, -21	9, 2
LINKED TO	21	52
LINKED TO	-10	-42
LINKED TO	-43	-27
EXPOSURE	102	249
EXPOSURE	252	255
EXPOSURE	173	169
WEIGHTED	103	250
WEIGHTED	253	256
WEIGHTED	348	1700
NODE NO.	52 TOTAL LINKS	12
X,Y,Z COORDINATE	11, 57	68, 60
LINKED TO	57	-42
LINKED TO	-64	-67
EXPOSURE	77	51
EXPOSURE	201	269
WEIGHTED	156	164
WEIGHTED	2120	2700
NODE NO.	57 TOTAL LINKS	6
X,Y,Z COORDINATE	27, 60	77, -59
LINKED TO	60	-59
EXPOSURE	101	100
WEIGHTED	204	152
NODE NO.	-62 TOTAL LINKS	3
X,Y,Z COORDINATE	12, 70	87, -71
LINKED TO	70	-55
EXPOSURE	82	279
WEIGHTED	166	332
NODE NO.	70 TOTAL LINKS	3
X,Y,Z COORDINATE	3, 81	100, -71
LINKED TO	81	-76
EXPOSURE	87	279
WEIGHTED	88	1760
NODE NO.	81 TOTAL LINKS	6
X,Y,Z COORDINATE	8, 95	113, 82
LINKED TO	95	96
EXPOSURE	142	145
WEIGHTED	286	910
NODE NO.	-76 TOTAL LINKS	4
X,Y,Z COORDINATE	13, 82	106, -78
LINKED TO	82	-76
EXPOSURE	96	242
WEIGHTED	970	2430

Table A.10. (cont'd.)

NODE NO.	-71	TOTAL LINKS	12
X,Y,Z COORDINATE	104	96	350
LINKED TO	71	-2	72
LINKED TO	-48	-12	
EXPOSURE	162	163	170
EXPOSURE	52	59	
WEIGHTED	1630	1540	1510
WEIGHTED	53	40	
NODE NO.	-52	TOTAL LINKS	6
X,Y,Z COORDINATE	384	69	350
LINKED TO	45	60	59
LINKED TO	81	154	177
EXPOSURE	82	310	1780
WEIGHTED	188	213	122
WEIGHTED	182	118	242
WEIGHTED	65	246	66
WEIGHTED	1890	2140	246
WEIGHTED	184	238	243
WEIGHTED	132	450	468
WEIGHTED	3120	3220	3120
NODE NO.	45	TOTAL LINKS	21
X,Y,Z COORDINATE	45	61	340
LINKED TO	47	59	60
LINKED TO	-39	-48	-32
LINKED TO	-59		-26
EXPOSURE	188	213	122
EXPOSURE	182	118	242
EXPOSURE	65	246	66
WEIGHTED	1890	2140	246
WEIGHTED	184	238	243
WEIGHTED	132	450	468
WEIGHTED	3120	3220	3120
NODE NO.	65	TOTAL LINKS	9
X,Y,Z COORDINATE	74	89	330
LINKED TO	64	73	71
EXPOSURE	53	47	15
WEIGHTED	54	48	20
WEIGHTED	380	138	380
WEIGHTED	690	2120	652
WEIGHTED	2980		
NODE NO.	71	TOTAL LINKS	6
X,Y,Z COORDINATE	86	102	300
LINKED TO	80	73	79
EXPOSURE	100	67	85
WEIGHTED	202	136	86
WEIGHTED	330	92	970
NODE NO.	79	TOTAL LINKS	9
X,Y,Z COORDINATE	97	108	300
LINKED TO	67	77	80
EXPOSURE	74	140	91
WEIGHTED	75	141	184
WEIGHTED	345	346	276
WEIGHTED	277	1	301
WEIGHTED	190	190	988
NODE NO.	85	TOTAL LINKS	9
X,Y,Z COORDINATE	112	93	250
LINKED TO	67	61	77
EXPOSURE	77	33	166
WEIGHTED	156	68	167
WEIGHTED	250	234	208
WEIGHTED	103	103	132
WEIGHTED	191	191	330
NODE NO.	61	TOTAL LINKS	4
X,Y,Z COORDINATE	118	81	290
LINKED TO	62	53	51
EXPOSURE	190	140	37
WEIGHTED	191	282	76
WEIGHTED	290	1	378
WEIGHTED	112		
NODE NO.	67	TOTAL LINKS	5
X,Y,Z COORDINATE	104	96	290
LINKED TO	63	77	-72
EXPOSURE	41	76	100
WEIGHTED	89	77	101
WEIGHTED	266	2	
NODE NO.	-52	TOTAL LINKS	6
X,Y,Z COORDINATE	112	64	300
LINKED TO	63	62	53
EXPOSURE	190	179	104
WEIGHTED	382	180	210
WEIGHTED	91	91	145
WEIGHTED	114		
NODE NO.	69	TOTAL LINKS	7
X,Y,Z COORDINATE	127	98	300
LINKED TO	76	68	-78
EXPOSURE	140	114	158
WEIGHTED	141	115	155
WEIGHTED	2	2	664
WEIGHTED	392	40	
NODE NO.	62	TOTAL LINKS	6
X,Y,Z COORDINATE	124	83	300
LINKED TO	58	56	68
EXPOSURE	152	88	52
WEIGHTED	306	178	56
WEIGHTED	262	325	60

Table A.10. (cont'd.)

NODE NO.	68 TOTAL LINKS	5			
X,Y,Z COORDINATE	137.	98.	300		
LINKED TO	78	76	-65	-73	-63
EXPOSURE	223	40	346	319	215
WEIGHTED	224	41	694	640	432

NODE NO.	76 TOTAL LINKS	7					
X,Y,Z COORDINATE	125.	106.	300				
LINKED TO	84	77	78	-72	-80	-84	-65
EXPOSURE	245	119	175	69	267	289	222
WEIGHTED	246	60000	52200	49000	28800	87000	111500

Case 7, Area 2, Route 1, Sensor Set 2.

Table A.11. Case 7 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
3	3820	7280	9	2	4870	7630
9	4870	7630	13	1	4450	8470
13	4450	8470	7	50	5290	7630
7	5290	7630	-2	40	4240	7280
-2	4240	7280	11	101	4100	7580
11	4100	7980	31	17	2560	9870
31	2560	9870	37	1	3470	10640
37	3470	10640	50	41	3260	11550
50	3260	11550	56	22	2630	12320
56	2630	12320	-59	159	3610	12550
-59	3610	12950	-71	60	2700	13720
-71	2700	13720	-78	48	3540	14560
-78	3540	14560	-79	1	4590	15120
-79	4590	15120	87	89	5150	15470
87	5150	15470	90	35	6060	15540
90	6060	15540	83	5	6900	14980
83	6900	14980	80	36	7610	14700
80	7610	14700	79	34	8790	14560
79	8790	14560	81	160	9560	14770

Table A.12. Case 7 - Node Linkage

NODE NO.	3 TOTAL LINKS					5
X,Y,Z COORDINATE	26,	4,	50			
LINKED TO	11	8	9	-2	-1	
EXPOSURE	75	107	0	148	166	
WEIGHTED	76	216	2	298	334	
NODE NO.	9 TOTAL LINKS					5
X,Y,Z COORDINATE	41,	9,	290			
LINKED TO	7	12	11	13	-2	
EXPOSURE	147	75	65	0	137	
WEIGHTED	296	152	132	1	276	
NODE NO.	13 TOTAL LINKS					6
X,Y,Z COORDINATE	35,	21,	290			
LINKED TO	11	19	23	12	7	-21
EXPOSURE	124	79	87	53	24	156
WEIGHTED	250	80	88	108	50	314
NODE NO.	7 TOTAL LINKS					4
X,Y,Z COORDINATE	47,	9,	300			
LINKED TO	12	-10	-2	-12		
EXPOSURE	100	265	15	248		
WEIGHTED	202	532	40	498		
NODE NO.	-2 TOTAL LINKS					2
X,Y,Z COORDINATE	32,	4,	310			
LINKED TO	11	-1				
EXPOSURE	100	96				
WEIGHTED	101	194				
NODE NO.	11 TOTAL LINKS					21
X,Y,Z COORDINATE	30,	14,	300			
LINKED TO	19	23	8	12	18	28
LINKED TO	-1	-21	-23	-26	-3	-18
LINKED TO	-27					
EXPOSURE	91	58	144	92	95	64
EXPOSURE	155	134	91	218	176	103
EXPOSURE	183				175	265
WEIGHTED	92	99	290	186	96	65
WEIGHTED	312	270	92	219	354	352
WEIGHTED	368				540	544
WEIGHTED					298	542
NODE NO.	31 TOTAL LINKS					6
X,Y,Z COORDINATE	2,	41,	300			
LINKED TO	14	18	22	37	-24	-23
EXPOSURE	100	64	17	0	228	80
WEIGHTED	101	130	40	1	458	81
NODE NO.	37 TOTAL LINKS					7
X,Y,Z COORDINATE	21,	52,	300			
LINKED TO	42	50	32	20	-40	-41
EXPOSURE	100	48	36	28	259	183
WEIGHTED	202	41	74	58	256	368
WEIGHTED					167	
NODE NO.	58 TOTAL LINKS					6
X,Y,Z COORDINATE	18,	65,	300			
LINKED TO	92	62	56	97	-48	-48
EXPOSURE	100	93	10	58	219	193
WEIGHTED	202	100	22	59	448	308
NODE NO.	56 TOTAL LINKS					4
X,Y,Z COORDINATE	9,	76,	300			
LINKED TO	52	-42	-45	-39		
EXPOSURE	100	219	165	150		
WEIGHTED	202	219	332	159		
NODE NO.	-59 TOTAL LINKS					5
X,Y,Z COORDINATE	23,	85,	350			
LINKED TO	97	68	-62	-64	-71	
EXPOSURE	100	147	165	107	39	
WEIGHTED	101	296	332	100	68	
NODE NO.	-71 TOTAL LINKS					5
X,Y,Z COORDINATE	18,	96,	350			
LINKED TO	78	-62	-76	-70	-78	
EXPOSURE	100	236	120	129	47	
WEIGHTED	202	237	121	130	48	

Table A.12. (cont'd.)

NODE NO.	-78	TOTAL LINKS	6
X,Y,Z COORDINATE	22°	108°	340
LINKED TO	89	75	82
EXPOSURE	90	78	17
WEIGHTED	91	71	36
NODE NO.	-79	TOTAL LINKS	9
X,Y,Z COORDINATE	37°	116°	330
LINKED TO	86	67	72
EXPOSURE	100	68	90
WEIGHTED	101	69	91
NODE NO.	87	TOTAL LINKS	6
X,Y,Z COORDINATE	45°	121°	320
LINKED TO	86	85	90
EXPOSURE	132	40	38
WEIGHTED	133	41	39
NODE NO.	90	TOTAL LINKS	6
X,Y,Z COORDINATE	56°	122°	310
LINKED TO	85	91	86
EXPOSURE	132	103	77
WEIGHTED	133	104	156
NODE NO.	83	TOTAL LINKS	8
X,Y,Z COORDINATE	70°	114°	300
LINKED TO	91	73	88
EXPOSURE	124	98	91
WEIGHTED	250	158	92
NODE NO.	80	TOTAL LINKS	5
X,Y,Z COORDINATE	83°	110°	300
LINKED TO	71	73	88
EXPOSURE	100	105	133
WEIGHTED	202	212	266
NODE NO.	79	TOTAL LINKS	10
X,Y,Z COORDINATE	97°	108°	300
LINKED TO	81	71	67
EXPOSURE	179	108	124
WEIGHTED	180	76300	37500
			13600
			62400
			19200
			15600
			816
			47500
			55000

Case 8 - Area 2, Route 2, Sensor Set 2.

Table A.13. Case 8 - Node Linkage for Route

FROM	EASTING	NORTHING	TO	PENALTY	EASTING	NORTHING
35	2770	10500	28	1	3610	9660
28	3610	9660	37	67	3470	10640
37	3470	10640	30	2	2560	9870
30	2560	9870	15	50	251	9030
15	2580	9030	9	7	4870	7630
9	4670	7630	12	1	4450	8470
12	4450	8470	7	50	5290	7630
7	5290	7630	-2	40	4240	7280
-2	4240	7280	10	101	4100	7980
10	4100	7980	31	37	4240	10080
31	4240	10080	36	52	5290	10640
36	5290	10640	46	119	5500	11270
46	5500	11270	34	8	4730	10430
34	4730	10430	32	156	5500	10150
32	5500	10150	-21	56	5010	5100
-21	5010	9100	11	34	5430	8190
11	5430	8190	21	19	5570	9170
21	5570	9170	19	110	4100	9100
19	4100	9100	-23	72	3120	9240
-23	3120	9240	22	18	4170	9240
22	4170	9240	42	34	2980	11060
42	2980	11060	33	64	2280	10360
33	2280	10360	56	34	2630	12320
56	2630	12320	50	29	3260	11550
50	3260	11550	57	59	3890	12390
57	3890	12390	-62	110	2840	13090
-62	2640	13090	70	2	2210	14000
70	2210	14000	81	1	2560	14910
81	2560	14910	96	1	3610	15960
56	3610	15960	105	1	4660	17010
105	4660	17010	91	1	6620	15540
51	6620	15540	88	59	7670	15470
88	7670	15470	83	22	6900	14580
63	6900	14580	60	46	7610	14700
80	7810	14700	79	34	8790	14560
79	6790	14560	66	52	9840	13510
66	9840	13510	76	144	10610	14420
76	10610	14420	84	191	10560	14580

Table A.14. Case 8 - Node Linkage

NODE NO.	35	TOTAL LINKS	8
X,Y,Z COORDINATE	11,	50,	300
LINKED TO	33	42	30
EXPOSURE	100	66	77
WEIGHTED	202	87	156
NODE NO.	28	TOTAL LINKS	7
X,Y,Z COORDINATE	23,	38,	300
LINKED TO	22	19	31
EXPOSURE	134	76	121
WEIGHTED	155	77	244
NODE NO.	37	TOTAL LINKS	7
X,Y,Z COORDINATE	21,	52,	300
LINKED TO	42	50	31
EXPOSURE	100	47	43
WEIGHTED	202	48	88
NODE NO.	30	TOTAL LINKS	4
X,Y,Z COORDINATE	8,	41,	300
LINKED TO	33	15	-24
EXPOSURE	100	24	214
WEIGHTED	101	50	430
NODE NO.	15	TOTAL LINKS	22
X,Y,Z COORDINATE	14,	29,	310
LINKED TO	19	22	6
LINKED TO	-23	-13	-24
LINKED TO	-40	-41	-16
EXPOSURE	61	73	114
EXPOSURE	132	130	211
EXPOSURE	177	171	220
WEIGHTED	124	148	230
WEIGHTED	133	262	424
WEIGHTED	178	172	442
NODE NO.	9	TOTAL LINKS	5
X,Y,Z COORDINATE	41,	9,	290
LINKED TO	7	11	10
EXPOSURE	147	75	65
WEIGHTED	296	152	132
NODE NO.	12	TOTAL LINKS	6
X,Y,Z COORDINATE	35,	21,	290
LINKED TO	10	19	22
EXPOSURE	124	79	87
WEIGHTED	250	80	88
NODE NO.	7	TOTAL LINKS	9
X,Y,Z COORDINATE	47,	9,	300
LINKED TO	11	-10	-2
EXPOSURE	100	265	19
WEIGHTED	202	532	48
NODE NO.	-8	TOTAL LINKS	2
X,Y,Z COORDINATE	32,	4,	310
LINKED TO	10	-1	-
EXPOSURE	100	96	-
WEIGHTED	101	194	-
NODE NO.	10	TOTAL LINKS	18
X,Y,Z COORDINATE	38,	14,	300
LINKED TO	19	22	8
LINKED TO	-26	-3	-10
EXPOSURE	91	97	143
EXPOSURE	216	173	172
WEIGHTED	92	58	288
WEIGHTED	217	348	346
NODE NO.	31	TOTAL LINKS	8
X,Y,Z COORDINATE	32,	44,	300
LINKED TO	34	22	19
EXPOSURE	116	79	39
WEIGHTED	234	160	88
NODE NO.	36	TOTAL LINKS	12
X,Y,Z COORDINATE	47,	52,	300
LINKED TO	32	39	45
LINKED TO	-27	-26	-10
EXPOSURE	158	89	239
EXPOSURE	169	171	118
WEIGHTED	318	180	240
WEIGHTED	388	344	119
			1860
			1600
			2060
			2060
			410
			1830

Table A.14. (cont'd.)

NODE NO.	46	TOTAL LINKS	10
X,Y,Z COORDINATE	59,	61,	320
LINKED TO	45	47	36
EXPOSURE	257	215	187
WEIGHTED	516	2160	1880
NODE NO.	34	TOTAL LINKS	6
X,Y,Z COORDINATE	19,	49,	300
LINKED TO	32	45	-41
EXPOSURE	78	185	267
WEIGHTED	158	186	268
NODE NO.	32	TOTAL LINKS	9
X,Y,Z COORDINATE	59,	45,	330
LINKED TO	21	38	-27
EXPOSURE	49	183	275
WEIGHTED	100	1840	552
NODE NO.	-21	TOTAL LINKS	6
X,Y,Z COORDINATE	43,	30,	330
LINKED TO	21	22	19
EXPOSURE	158	48	15
WEIGHTED	318	98	40
NODE NO.	11	TOTAL LINKS	4
X,Y,Z COORDINATE	49,	17,	300
LINKED TO	21	-12	-10
EXPOSURE	18	346	335
WEIGHTED	19	694	680
NODE NO.	21	TOTAL LINKS	23
X,Y,Z COORDINATE	51,	31,	330
LINKED TO	27	13	22
LINKED TO	-26	-12	-32
LINKED TO	-41	-40	-36
EXPOSURE	337	321	74
EXPOSURE	254	321	233
EXPOSURE	190	175	195
WEIGHTED	3380	644	150
WEIGHTED	510	644	2340
WEIGHTED	191	176	1960
NODE NO.	19	TOTAL LINKS	4
X,Y,Z COORDINATE	30,	30,	250
LINKED TO	22	-26	-23
EXPOSURE	100	200	35
WEIGHTED	101	402	72
NODE NO.	-23	TOTAL LINKS	4
X,Y,Z COORDINATE	16,	32,	310
LINKED TO	22	-24	-13
EXPOSURE	8	228	137
WEIGHTED	18	458	276
NODE NO.	22	TOTAL LINKS	21
X,Y,Z COORDINATE	21,	32,	300
LINKED TO	8	42	33
LINKED TO	-24	-20	-18
LINKED TO	-43	-41	-32
EXPOSURE	96	33	32
EXPOSURE	175	300	186
EXPOSURE	171	300	91
WEIGHTED	194	34	66
WEIGHTED	352	602	374
WEIGHTED	1720	188	184
NODE NO.	42	TOTAL LINKS	7
X,Y,Z COORDINATE	14,	38,	300
LINKED TO	50	52	35
EXPOSURE	100	73	31
WEIGHTED	101	74	64
NODE NO.	33	TOTAL LINKS	11
X,Y,Z COORDINATE	4,	48,	300
LINKED TO	52	50	46
LINKED TO	-13	-13	-17
EXPOSURE	61	58	33
EXPOSURE	62	59	39
WEIGHTED	62	59	39
WEIGHTED	126	59	250
NODE NO.	56	TOTAL LINKS	8
X,Y,Z COORDINATE	9,	76,	300
LINKED TO	52	50	-62
EXPOSURE	100	28	214
WEIGHTED	202	29	215

Table A.14. (cont'd.)

NODE NO.	50	TOTAL LINKS	4
X,Y,Z COORDINATE	18,	65,	300
LINKED TO	52	57	-48 -40
EXPOSURE	100	58	219 193
WEIGHTED	202	59	440 388
NODE NO.	57	TOTAL LINKS	6
X,Y,Z COORDINATE	27,	77,	350
LINKED TO	60	-59	-48 -52 -64 -62
EXPOSURE	172	160	143 122 191 54
WEIGHTED	173	322	286 246 192 110
NODE NO.	62	TOTAL LINKS	3
X,Y,Z COORDINATE	12,	87,	350
LINKED TO	70	-71	-59
EXPOSURE	0	195	226
WEIGHTED	2	156	454
NODE NO.	70	TOTAL LINKS	3
X,Y,Z COORDINATE	3,	100,	330
LINKED TO	P1	-71	-76
EXPOSURE	0	195	86
WEIGHTED	1	392	87
NODE NO.	81	TOTAL LINKS	6
X,Y,Z COORDINATE	8,	113,	330
LINKED TO	95	P2	96 -76 -78 -74
EXPOSURE	57	49	0 147 97 127
WEIGHTED	116	50	1 296 98 256
NODE NO.	96	TOTAL LINKS	8
X,Y,Z COORDINATE	23,	128,	330
LINKED TO	82	102	95 185 -93 -85 -92 -79
EXPOSURE	63	149	54 0 190 54 140 24
WEIGHTED	64	150	110 1 382 55 282 50
NODE NO.	105	TOTAL LINKS	13
X,Y,Z COORDINATE	38,	143,	330
LINKED TO	87	86	90 85 82 95 91 -85 -88 -93
EXPOSURE	79	-95	-92
EXPOSURE	81	62	28 13 59 53 0 148 137 120
EXPOSURE	96	121	96
WEIGHTED	164	126	29 28 120 108 1 149 138 258
WEIGHTED	87	244	194
NODE NO.	51	TOTAL LINKS	6
X,Y,Z COORDINATE	66,	122,	310
LINKED TO	90	82	85 88 -87 -77
EXPOSURE	124	87	95 58 180 73
WEIGHTED	250	176	192 59 181 148
NODE NO.	88	TOTAL LINKS	6
X,Y,Z COORDINATE	81,	121,	320
LINKED TO	80	P3	89 -81 -87 -90
EXPOSURE	29	10	116 139 146 150
WEIGHTED	60	22	117 140 294 151
NODE NO.	83	TOTAL LINKS	7
X,Y,Z COORDINATE	70,	114,	300
LINKED TO	73	85	80 90 -77 -81 -79
EXPOSURE	124	76	47 56 161 54 97
WEIGHTED	250	154	48 114 324 55 196
NODE NO.	80	TOTAL LINKS	5
X,Y,Z COORDINATE	63,	110,	300
LINKED TO	71	73	79 89 -81
EXPOSURE	100	105	33 154 146
WEIGHTED	202	212	34 195 157
NODE NO.	79	TOTAL LINKS	9
X,Y,Z COORDINATE	97,	108,	300
LINKED TO	71	67	77 29 93 66 -22 -69 -81
EXPOSURE	106	124	135 207 191 51 271 94 109
WEIGHTED	218	125	136 208 192 52 272 198 220

Table A.14. (cont'd.)

NODE NO.	66	TOTAL LINKS	9
X,Y,Z COORDINATE	112,	93,	290
LINKED TO	67	61	77
EXPOSURE	127	100	160
WEIGHTED	256	202	161
		350	234
			157
			143
			144
			239
			580

NODE NO.	76	TOTAL LINKS	9
X,Y,Z CCORCINATE	123,	106,	300
LINKED TO	69	84	77
EXPOSURE	155	190	110
WEIGHTED	780	191	55500
		54600	39600
			79800
			23400
			61800
			94000

APPENDIX B

FORTRAN PROGRAM FOR ROUTING MODEL

The program that has been developed as a result of this research is currently running on a CDC Cyber 7400 series machine. The programmed model has been tested on a ten kilometer area and was run for a 35 by 35 km area. The longest running feature of the model is the line of sight calculations. The model has 14 subroutines which are controlled by the main program and one subroutine. The relationship between the subroutines is shown in Figure B-1.

Within this appendix is a short discussion of the model. The basic purpose and operations of the various subroutines are given first. The arrays in COMMON and those that are not are defined. Also variables within COMMON are defined along with some which are used only in a single subroutine. With one exception, flow charts were not drawn for the model since the definition of the variables and the comments within the program itself should be sufficient. The logic of subroutine CLUST is not obvious, therefore a flow chart was drawn for this subroutine. Lastly, within this appendix is a listing of the Fortran computer code for the 10 by 10 km size model.

Main Program

The main program is an executive routine that directs the operation of the model. Five subroutines are called by the main program. The initial call is to INDATA which is a short subroutine that reads the terrain data. After this call the main program groups this elevation

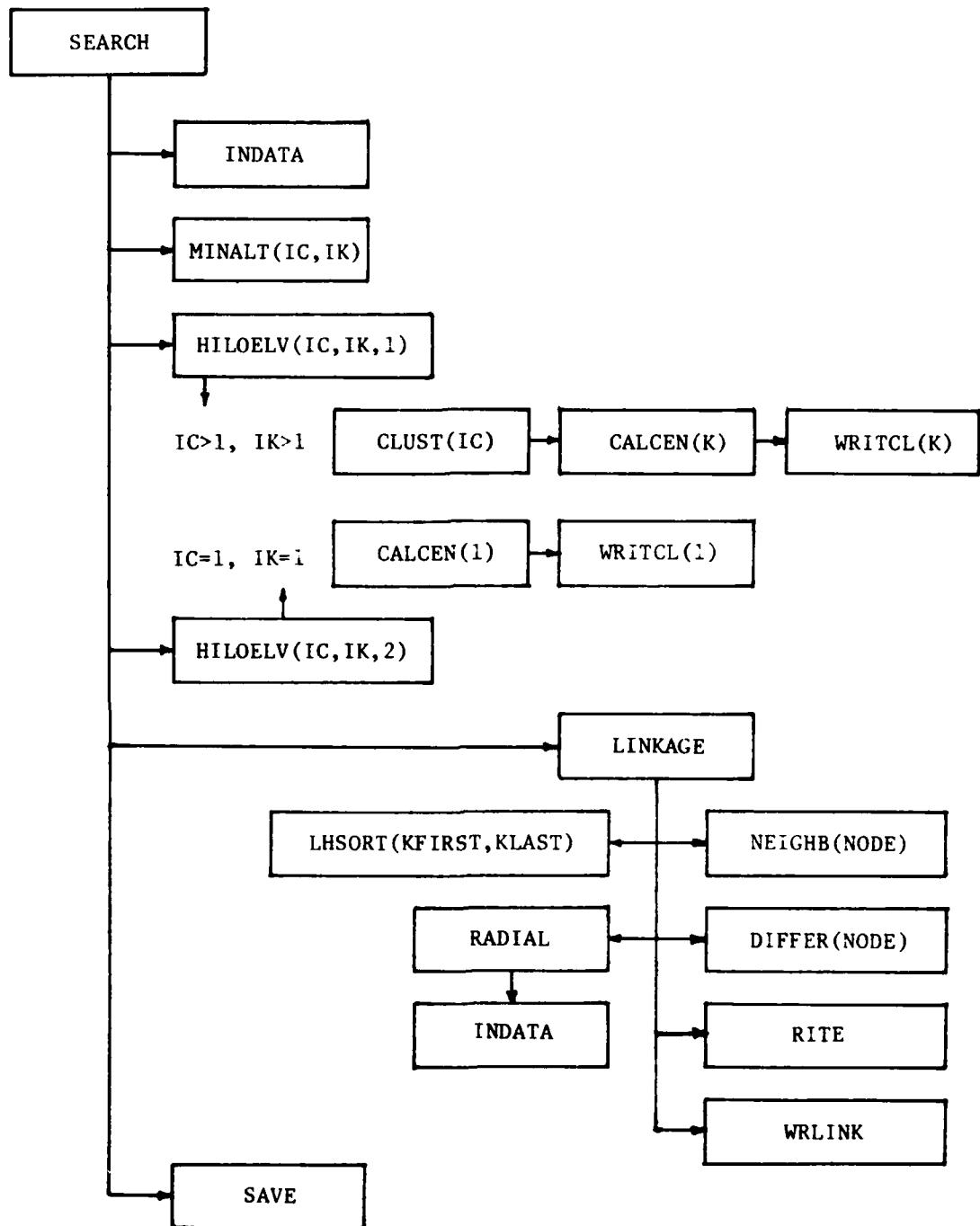


Figure B-1. Main Program and Subroutine Relationship.

data into elevation bands. Each sensor site's elevation is obtained from this data by finding the sensor's location within the elevation data array. A call is then made to the MINALT subroutine to determine both the maximum and minimum elevation groups within each elevation data array of 1 km square. Two calls are made to HILOELV subroutine; the first call is for processing the low elevation band and the second call is for the high elevation band. The next subroutine called is LINKAGE which is an executive subroutine that directs the routing process. If the results of route development are to be retained for further use, then SAVE can be called.

INDATA

This subroutine only reads the elevation data for the model. The terrain data is read in strips of 1 km wide and up to 50 km long. The data is stored into arrays of 15 by 15 data points and have a terrain interval of 70 meters between points. As each new strip of terrain is needed, a call is made to this subroutine.

MINALT

The minimum and maximum elevation data points in an array are found and stored in arrays in a packed format. The array ISET contains the row and column index of each low point and the array MSET contains the high points. The data is processed sequentially from the first terrain data array element such that if a new minimum or maximum is found, the pointers and counter are reset.

HILOELV

This subroutine is divided into two major parts. An IF test is performed on a call parameter IL0 to determine whether the low

elevation (IC, — ,IL0=1) or high elevation data (— ,IK,IL0=2) is processed. The logic is the same for each part. A call is made to CLUST which identifies disjoint groups of elevation data. After finding the members of each cluster a call is made to CALCEN to calculate the cluster center. If there is only a single value in this cluster, CLUST is skipped and CALCEN is called directly. The values on these centers are then stored in LOWCEN or HICEN depending on which type of elevation data is being processed. After storing these values a return is made to the main program.

CLUST

Once the low or high data points are identified the cluster to which they belong is determined by the beginning and end of each data point string. The data points have been found sequentially; therefore, the breaks in adjacency of points define the cluster boundaries. Since the row and column indexes are stored by letting IVAL = (ROW * 100) + COLUMN, subtracting two consecutive values will indicate whether they are adjacent. When all the members of a cluster are found, a call is made to CALCEN to calculate the centroid of the cluster.

CALCEN

This subroutine calculates the centroid of the cluster found in CLUST. The mean of row indexes (\bar{Y}) and mean of column indexes (\bar{X}) are the values for the center of the cluster. Since the indexes are integer values, the sum of the indices has a half added to allow for truncation of the decimal portion. An IF test is made on the calculated indexes for the center to ensure that they are within the array dimensions.

For debug purposes several write statements in this subroutine can be set.

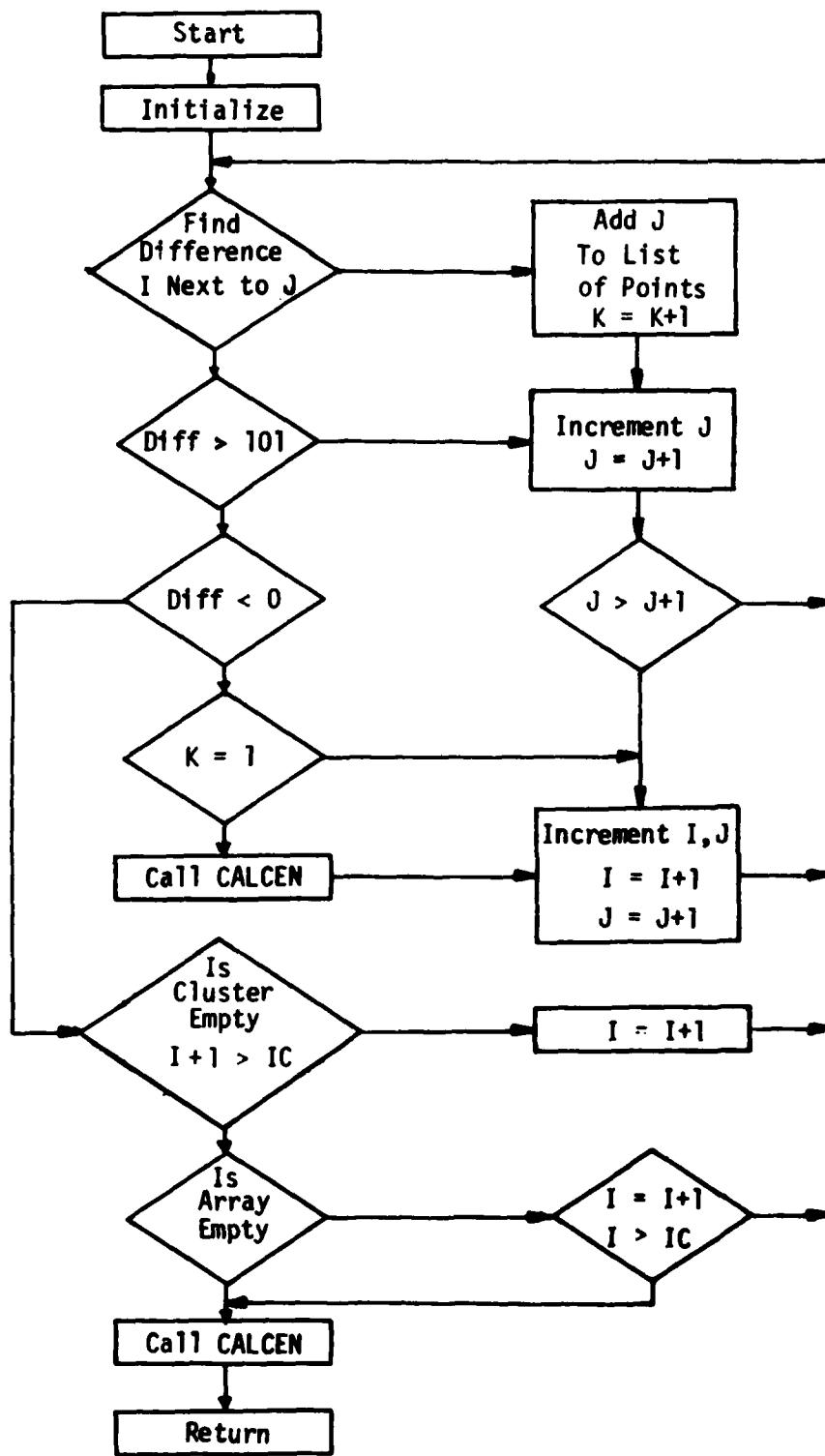


Figure B-2. Subroutine CLUST.

WRITCL

To list the clusters and centers this subroutine can be called letting LWRIT \geq 3. The low (or high) elevation cluster and pointers to the cluster members are listed. When this routine is called, LH is checked to decide whether high or low elevation values are to be printed.

LINKAGE

Once all the high and low elevation centers have been found, the main program calls this subroutine. The remaining portion of the model is directed by LINKAGE. The first subroutine it calls is LHSORT to sort the high and low lists of centers. Then subroutine RADIAL is called to determine the LOS between each node point and each sensor. RADIAL also calculates the first part of the penalty function.

The routine now processes each route node by finding all other node points which are within 1 km. These other nodes are the neighborhood of points that have possible links between them and the current node being evaluated. Two arrays, LINK and LINKTO, are used to store which nodes are in the neighborhood, the penalty value associated with the nodes and a beginning of the list for each node. The high nodes are identified by a minus sign. Having defined the neighborhoods and penalty values for each point in the neighborhood, the route node is selected. Control is then returned to the main program.

RADIAL

This subroutine is the most time consuming of the model. To determine visibility of two terrain points requires more effort than would seem to be necessary. The first problem is to locate where the two points are in the terrain data base. Along the vector connecting

these points a search is made for any terrain feature that would block the line of sight.

The subroutine first determines whether the sensor or the node is the westernmost point. If necessary the logic will swap the two points to set the node as the western point and the sensor as the eastern point. Having established the ends of the LOS vector, the tangent from the horizontal and the sine and cosine are calculated.

With those parameter values the routine begins the search along the vector. The vector is tested to locate its direction. Depending on whether it's between 0° - 45° , 45° - 135° , or 135° - 180° will give a heading of north, east or south respectively. The calculations used are given in section 4.3.

The routine finishes by listing the exposure values calculated for the number of sensors that can see each node. These values will then be used by DIFFER for those nodes which lie along the route corridor.

LHSORT

The initial point and the terminal point are added to the list of low elevation centers. The low elevation centers (nodes) are sorted into ascending order by row. This sorting is to ease the logic for the model. After the low centers are finished the high elevation centers are sorted in the same manner. Pointers KFIRST and KLAST are used to locate the initial and terminal nodes and are set after the sorting of LOWCEN. The lists of low and high nodes are written out as tables before returning to LINKAGE.

NEIGHB

To define a neighborhood it was found that the normal visual search pattern is limited to 1 km. The nodes which lie within 1 km are considered

to be neighbors of the current node. The resulting area is a 2 km square with the principle node in the center. Having sorted the arrays of centers, only 15 rows in either direction from the current row are searched for a neighbor. For any row that is searched, only those nodes which are within 15 columns on either side of the current node are retained as neighbors. When both the low and high centers that are in the neighborhood have been found, they are stored for use by subroutine DIFFER. The results can be listed by having $LWRIT \geq 2$.

DIFFER

For each neighborhood the distance from the current (primary) node is calculated and stored. The DIST array retains the distances for low centers in the first column and the high centers in the second column. The minimum and maximum distance and elevation are found while the distance between node points is calculated. Once these values are obtained they are sorted in ascending order by distance. A value of $LWRIT \geq 2$ will allow the printing of these results. The routine then completes the calculation of the exposure value for these nodes using the values stored by RADIAL.

RITE

This routine will write several of the large arrays to temporary storage if there are more values than the arrays can handle. These data are then read back into the program as needed on top of those values no longer needed.

SAVE

This routine will save the route and linkage arrays for plotting. A TAPE 7 is set up to store the data in a format for plotting the X-Y

coordinates of the nodes. The routine can be easily modified to write any data that should be retained.

WRLINK

After the route has been found, this routine will list the linkage information used in constructing the route. Listed are the arrays, the pointers and nodes with their exposure values.

Arrays in COMMON

IDATA(I,J,K)	This array contains terrain elevation values. It is a three dimensional array where the index K indicates the map sheets. The initial values are reassigned based on the equation given in section 4.2
LOWCEN(I,J,K)	The X, Y and Z coordinate of the low elevation nodes are stored in this array. Index I contains the Y value, J contains the X value, and K contains the Z value.
HICEN(I,J,K)	This array is just like LOWCEN except it contains the X, Y and Z coordinate of the high elevation nodes.
IPOINT(I)	This array is used throughout the model to store pointers.
ISET(I)	The row and column indexes of each cluster member are packed into this array. The first time used it contains low elevation points. The second time it contains the high elevation points.
MSET(I)	This array stores the high elevation cluster members for use by ISET.
CEROID(X,Y,Z)	As the centers for the low and high centers are being calculated CEROID is used to temporarily store them before placing them in either LOWCEN or HICEN.
ISITE(I,J,K)	The location of the sensors are stored in this array. Up to 10 sensors can be used as currently dimensioned.
INITIAL(I)	The location of the starting point for the route is entered into this array.
LAST(I)	The terminal point for the route is stored in this array.
LINK(I)	This array contains the pointers to the entries of LINKTO. The value in location I gives the beginning of the node list in LINKTO that is associated with node I of array FROM.

LINKTO(I,J,K)	This array has the node number of the nodes linked to node I of FROM. J is the exposure value of that node and K is the weighted exposure value.
FROM(I)	The route nodes are stored in order of occurrence in this array. If I is the tenth entry then this node number is the tenth node of the route.
TO(I,J)	The first entry I contains the node that is reached from the FROM(I) node. The value stored in J is the weighted exposure for the node traveled to FROM(I).
DETLO(I)	The visibility value for a low elevation node is stored in this array.
DETHI(I)	The visibility value for a high elevation node is contained in this array.
DIST(I,J)	The distance between a primary route node and the neighborhood nodes are stored in DIST. The I value is for low elevation nodes and the J value is for high elevation nodes.
SYSR(I)	This array has the weapon system kill radius in km. This value is converted to the units used by the model. If the first value is zero, then radar avoidance weighting is not used.
SR(I,J)	The range between the current node and the sensor, the angle to the sensor and the angle of coverage are stored in this array. This information is used for the radar avoidance weighting.

Arrays not in COMMON

MPOINT(I)	For small lists which need pointers this array is set equivalent to the last part of IPOINT to save core storage. This array is used in several subroutines in this manner.
IFINISH(I)	To keep up with the progress of the LOS calculations in RADIAL, this array has the bits of an array element set to one as each node-sensor pair is completed. The zero through nine bit are used for low elevation nodes and up to 10 sensors. The ten through nineteen bit are used for high elevation nodes.
NLIST(I)	After the route is found, the smoothing routine stores the modified route in this array.

Variables in COMMON

JSTRIP	The current map sheet that is being used by the model.
KCET	The number of clusters that are found is stored in this variable until it can be added to either NLOW or NHI depending on whether it is low or high elevation clusters.
NLOW	This variable is the total number of low elevation nodes found plus the initial and final route nodes.
NHI	The total number of high elevation nodes found is stored in this variable.
SMAX	As the node-sensor combinations are being processed the maximum distance is checked. If a distance is found which is greater than SMAX then the new value is assigned to SMAX.
NBLKS	This variable is the number of data blocks written on to temporary storage.
LWRIT	This variable is used to obtain detail data on the operations of the model. It is mainly used for checking results. IF LWRIT > 5 then everything is printed. As this variable increases in value the amount of printing decreases. A value over 3 turns off the detail printing.
LDEBG	To debug the clustering portion of the model this variable can be set ≠ 1.
LALT	The minimum elevation for the map sheet currently being used.
HALT	The maximum elevation for the current map sheet.
LH	If LH is set to 1 then low elevation points are being processed. IF LH is 2 then high elevation points are being processed.
SENALT	The altitude of the sensor above local terrain is entered in this variable.
VEHALT	The vehicle altitude it will be flying above local terrain. Can be used for a ground vehicle by setting it to zero.
NSITE	The number of sensors that are located in the area of interest. A maximum of ten can currently be used.

RE	This variable is the radius of the earth for use in the LOS calculations to allow for earth curvature.
MDIM	This variable is the number of data points in the terrain data array. It is now set for a 15 by 15 array.
GRID	The grid interval (in meters) between the terrain data points. From this research the grid interval was 70 meters.
SWEA	The easting of the southwest corner of the terrain area being analyzed.
SWNR	The northing of the southwest corner.
LTRS	The UTM letter designation for the grid zone of the southwest corner.
IRADUS	The radius value to be used to determine a neighborhood of nodes. A value of 15 (1 km) is currently being used.
LNEBR	The number of low elevation nodes within the neighborhood for the current route node being evaluated.
KNEBR	The number of high elevation nodes within the neighborhood.
IROW	The row value (y-axis) of the current route node being evaluated.
JCOL	The column (x-axis) of the current route node being evaluated.
KFIRST	The location of the initial route node within the LOWCEN array.
KLAST	The location of the terminal or destination node within the LOWCEN array.
IC	The number of nodes that the route passes through.
IFREE	The total number of linkages that were found as the route was being developed.
RANGE	The range at which the weighting scheme narrows the search area down. When the terminal point is within 1 km of the current position the field of view is narrowed down to 90°. Node points outside these parameters have a higher weight assigned to them.

KMAT	The maximum number of terrain data arrays in the north-south direction is assigned this variable.
ISTRIP	This variable is set equal to the number of map sheets being used.
JMAT	The current array within a map sheet that is being used by the model.
RATE	The distance between terrain points in the data base that are being used. In this research every data point is used thus RATE is set to one.

Subroutine RADIAL Variables

NORTH	These variables are the map sheet boundaries and the names correspond to the boundary edge.
SOUTH	
EAST	
WEST	
ZCURVE	This parameter is a logical value that be set if curvature of the earth is used for LOS calculations.
DZ	The amount of curvature that is present when correcting for earth curvature.
XSIT,XP YSIT,YP ZSIT,ZP KSIT	These variables are the X, Y and Z coordinates of the sensor that is currently being used in the LOS calculations. The KSIT value is the integer value of XSIT.
XS1 YS1 ZS1 KS1	These variables are the X, Y and Z coordinates of the current node being processed by RADIAL. The KS1 is the integer value of XS1.
XSP YSP ZSP	The difference between the sensor and node are found for each coordinate and stored in these variables.
DIS RMAX	This variable is the vector distance between the sensor and node in the X-Y plane. RMAX is set equivalent to DIS.
R	This variable is the vector distance from the node to the terrain point in the data base that LOS is being checked.
TM	The tangent to the eastern point from the horizontal is stored in this variable.
T	The tangent to the terrain is calculated and stored in variable for comparison with TM.
YWEST	The Y component of the tangent T on the west map edge is contained in this variable to correct for vector crossing map sheets.
Z	The elevation of the current terrain point being checked for masking is assigned to this variable.

XSIN	The sine of the azimuth angle measured clockwise from north for the node-sensor vector is stored in this variable.
YCOS	This variable is the cosine of the azimuth angle.
ZNORTH ZSOUTH	These variables are logicals to indicate whether the vector is heading north or south.
NAR	This variable is the array within the map sheet where the terrain point is located.
X,IX	These variables are the x coordinate for the current terrain point.
Y,JY	These variables are the y coordinate for the current terrain point.
IDX,JDY	These variables are the increment in X and Y respectively.
IFIN	This variable is used to check for completion of a sensor-node pair.
IEXP	The sensor bit in IFINISH is set by using the exponent of 2 corresponding to the bit location in the computer word.
RTOD	This variable is the number of radians to degrees.
EAST1 NORTH1	The easting and northing of the beginning of a route segment or path leg along the route.
EAST2 NORTH2	The easting and northing of the end node of the route segment that begins at EAST1,NORTH1.

Subroutine DIFFER Variables

DMIN	The minimum distance between any node in the neighborhood of the current route node being processed.
DMAX	The maximum distance between any node in the neighborhood of the current route node being evaluated.
DRANG	The difference between DMAX and DMIN is assigned this variable.
KZMIN	The minimum elevation for any node in the neighborhood for the route node being evaluated.

KZMAX The maximum elevation for any node in the neighborhood for the route node being evaluated.

KZRANG The difference of KZMAX less KZMIN is assigned this variable.

Subroutine LINKAGE Variables

NWEIG This variable is the weight a node point has because of its location with respect to the current route node.

IFLAG If the procedure cannot find any node points in a neighborhood of a route point, the rectilinear distance for a neighborhood is doubled. IFLAG is then set to -1 and the model stops if no nodes still cannot be found.

NPEN This variable is the weight exposure value the penalty function calculates for the node in the neighborhood.

LPEN This variable is used to store the current minimum NPEN that has been found.

NEWPT The node in the neighborhood with the current minimum exposure is assigned to NEWPT.

XI,IX The X coordinate difference between the route node and the neighborhood node is stored in these variables.

YJ,JY The Y coordinate difference for the same two nodes as XI above.

KANG The angle at which the terminal node lies from the current route node is measured from the x-axis and assigned to KANG.

IANG This angle is the direction of a neighborhood node from the route node.

IAK This angle is the difference between KANG and IANG.

RANG The range from the route node to the terminal node is stored in this variable.

RA This range is from the route node to the neighborhood node.

FORTRAN LISTING

```

PROGRAM SEARCH(INPLT=80,OUTPUT=137,TAPE5=INPUT,
1 TAPE6=OUTPUT,TAPE7,TAPE8,TAPE9)
COMMON/IDAT/ KMAT,ISTRIP,IData(15,15,10)
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250),
1 ISET(250),MSET(250),CEROID(250,3)
COMMON/SENVER/ LALT,FALT,SEALNT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTRS
COMMON/SRAD/ RANGE,RE,MDIM,RATE,NSITE,ISITE(10,3),SYSR(10)
INTEGER FALT,CERCID,HICEN,GRID,SWEA,SWNR,SAVETP
INTEGER SEALNT,VEHALT
DATA INT,KMAT,ISTRIP,GRID,RANGE/10,10,10,70,14.3/
DATA KCET,LWRIT,LDEBG,NLOW,NHI/0,1,1,0,0/
C
C *** KMAT IS SET UP FOR 10 ARRAYS WITHIN A STRIP OF DATA ***
C *** ISTRIP IS SET UP FOR 10 STRIPS ***
C
      NSITE = 3
      LWRIT = 3
      LDEBG = 1
C
C *** READ INPUT DATA ***
C
      READ(5,900) ISTRIP,KMAT,SAVETP,LWRIT,LDEBG
      READ(5,901) INT,GRID,LTRS,SWEA,SWNR
      READ(5,902) SEALNT,VEHALT,IRADUS,RANGE,RE,RATE,MDIM
      READ(5,903) INITIAL(2),INITIAL(1),INITIAL(3)
      READ(5,903) LAST(2),LAST(1),LAST(3)
      READ(5,904) NSITE
      IF(NSITE .GT. 10) GO TO 1200
100 DO 125 I=1,NSITE
      READ(5,903) ISITE(I+2),ISITE(I+1),ISITE(I,3)
      READ(5,905) SYSR(I)
125 SYSR(I) = SYSR(I)*1000.0/GRID
C
      WRITE(6,510)
      DO 1000 JK=1,ISTRIP
      JSTRIP = JK
      CALL INDATA
C
C *** GROUP DATA INTO ALTITUDE BANDS          ***
C *** INT IS THE BAND INTERVAL               ***
C *** JMAT IS THE MATRIX BEING SUBDIVIDED FOR ANALYSIS ***
C
      DO 660 I=1,15
      DO 660 J=1,15
      DO 660 K=1,KMAT
660 IData(I,J,K)=(((IData(I,J,K)-1)/INT)*INT)+INT
C
C *** FIND THE LOCATION OF THE SENSORS IN THE TERRAIN DATA ***
C

```

```

DO 700 I=1,NSITE
ICOL = JK*15
NX = ISITE(I,2)
IF(NX .GT. ICCL) GO TO 700
ICOL = (JK-1)*15
IF(NX .LT. ICOL) GO TO 700
NX = NX-(JK-1)*15
NY = ISITE(I,1)
NZ = (NY-1)/15
NY = NY-NZ*15
NZ = NZ+1
ISITE(I,3) = IDATA(NY,NX,NZ)
700 CONTINUE
IF (LWRIT .LE. 4) GO TO 675
DO 501 K=1,KMAT
WRITE(6,911)
501 WRITE(6,912) ((IDATA(I,J,K),J=1,15),I=1,15)
WRITE(6,910)
C
C *** MINALT FINDS MIN AND MAX ELEVATION IN EACH ARRAY ***
C *** HILOELV OVERSEE THE CLUSTERING OF ELEVATION BANDS ***
C
675 DO 800 JJ=1,KMAT
JMAT = JJ
IC=1
IK=1
CALL MINALT(IC,IK)
CALL HILOELV(IC,IK,1)
IF(IC .EG. 225) GO TO 800
CALL HILOELV(IK,IK,2)
800 CCNTINUE
1000 CCNTINUE
WRITE(6,910)
WRITE(6,915) ISTRIP,KMAT,SAVETP,LWRIT,LDEEG
WRITE(6,916) INT,GRID,LTRS,SWEA,SLNR
WRITE(6,917) SENALT,VEHALT,IRADIUS,RANGE,RE,RATE,MDIM
WRITE(6,918) INITIAL(2),INITIAL(1),INITIAL(3)
WRITE(6,919) LAST(2),LAST(1),LAST(3)
WRITE(6,913)
DO 1100 I=1,NSITE
1100 WRITE(6,920) ISITE(I,2),ISITE(I,1),ISITE(I,3),SYSR(I)
CALL LINKAGE
IF(SAVETP .GT. 0) CALL SAVE
STOP
1200 WRITE(6,914) NSITE
NSITE = 10
GC TO 100
C
900 FFORMAT(5I5)
901 FFORMAT(2I5,10X,A2,2I4)
902 FFORMAT(3I5,3F10.3,I5)
903 FFORMAT(3I10)

```

```
904 FORMAT(I5)
905 FORMAT(F10.2)
910 FORMAT(1H1)
911 FORMAT(/10X,*ALTITUDE ARRAY*/)
912 FORMAT(15(1X,I6))
913 FORMAT(20X,*SENSOR LOCATION*/24X,*X*,7X,*Y*,7X,*Z*,  
1 7X,*SYS R*)
914 FORMAT(////5X,*NUMBER OF SITES GREATER THAN 10 - *,I6/  
1 EX,*NSITE SET TO 10*)
915 FORMAT(//20X,*INPUT DATA*/20X,*ISTRIP KMAT SAVETP *,  
1 *LWRIT LCEBG*/ 20X,5(I5,1X))
916 FCRRMATE(20X,*INT GRID LTRS SWEA SWNR*/  
1 20X,2(I5,1X),A2,2(1X,I5))
917 FORMAT(20X,*SERALT VEHALT IRADUS RANGE RE*,10X,  
1 *RATE MDIM*/20X,3(I5,1X),F8.3,1X,F10.2,1X,F8.3,1X,I6)
918 FORMAT(20X,*INITIAL POINT ON ROLTE - X,Y,Z*/  
1 20X,3(I6,2X))
919 FORMAT(20X,*DESTINATION POINT FOR RROUTE - X,Y,Z*/  
1 20X,3(I6,2X))
920 FORMAT(20X,3(I5,3X),F10.3)
END
```

```

SUBROUTINE HILOELV(IC,IK,ILO)
C
C *** THIS SUBROUTINE CONTROLS HIGH/LOW CLUSTERING      **
C *** IC IS THE NUMBER OF MEMBERS IN LOWCEN             **
C *** IK IS THE NUMBER OF MEMBERS IN HICEN              **
C *** LOWCEN CONTAINS THE LOW ELEVATION CENTROIDS       **
C *** HICEN CONTAINS THE HIGH ELEVATION CENTROIDS       **
C *** NLOW IS THE NUMBER OF LOWCEN CENTROIDS            **
C *** NHI IS THE NUMBER OF HICEN CENTROIDS              **
C *** KCET IS CURRENT COUNT OF CLUSTER MEMBERSHIP        **
C
COMMON/IDAT/ KMAT,ISTRIP,IData(15,15,10)
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250),
1 ISET(250),MSET(250),CEROID(250,3)
COMMON/SENVER/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTRS
INTEGER HALT,CERCID,HICEN
C
IF(ILC .EG. 2) GO TO 20
C
C *** PROCESS LOWCEN **                                 **
C *** IF IC=1 ONLY ONE VALUE WAS FOUND FOR MEMBERSHIP   **
C *** IF IC=225 THEN ALL THE ELEVATION VALUES ARE THE SAME   **
C *** THE SAME LOGIC IS USED FOR IK                      **
C
LH = 1
IF(IC .EG. 1) GO TO 500
IF(IC .EG. 225) GO TO 550
CALL CLUST(IC)
GO TO 610
500 IPOINT(1) = 1
GO TO 600
550 IPOINT(1) = 113
600 CALL CALCEN(1)
610 CONTINUE
C
C *** STORE NEW MEMBERS **                            **
DO 625 L=1,KCET
LOWCEN(NLOW+L,1) = CEROID(L,1)
LOWCEN(NLOW+L,2) = CEROID(L,2)
625 LOWCEN(NLOW+L,3) = CEROID(L,3)
NLOW = NLOW+KCET
KCET = 0
650 L=1,250
ISET(L) = 0
650 IPOINT(L) = 0
RETURN
C
C *** PROCESS HICEN **                                **
C

```

```
20 LH = 2
DO 100 I=1,IK
100 ISET(I) = MSET(I)
IF(IK .EQ. 1) GO TO 700
IF(IK .EQ. 225) GO TO 750
CALL CLUST(IK)
GO TO 810
700 IPOINT(1) = 1
GO TO 800
750 IPOINT(1) = 113
800 CALL CALCEN(1)
810 CONTINUE
C
C *** STORE NEW MEMBERS ***
DO 825 L=1,KCET
HICEN(NHI+L,1) = CEROID(L,1)
HICEN(NHI+L,2) = CEROID(L,2)
825 HICEN(NHI+L,3) = CEROID(L,3)
NHI = NHI+KCET
KCET = 0
DO 850 L=1,250
ISET(L) = 0
850 IPOINT(L) = 0
RETURN
END
```

```
SUBROUTINE INDATA
COMMON/IDAT/ KMAT,ISTRIP,IData(15,15,10)
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
INTEGER HALT
C
C *** READ INPUT TERRAIN DATA ***
C
READ(8) LALT,HALT
DO 600 IMAT=1,KMAT
600 READ(8) ((IData(IRCW,ICOL,IMAT),IROW=1,15),ICOL=1,15)
RETURN
END
```

```

SUBROUTINE MINALT(IC,IK)
C
C *** THIS SUBROUTINE FINDS THE MIN AND MAX ELEVATION   **
C *** BANDS IN EACH JMAT ARRAY OF IDATA. IVAL IS THE   **
C *** ARRAY ELEMENT THAT IS BEING CHECKED FOR MIN/MAX   **
C
C
COMMON/LCENT/ LLOWCEN(250,3),HICEN(250,3),KCET,NLOW,NFI,
1 SMAX,LWRIT,LDEEG,JMAT,JSTRIP,LH
COMMON/POINT/ INITIAL(3),LAST(3),IPCINT(250),
1 ISET(250),MSET(250),CEROID(250,3)
COMMON/IDAT/ KMAT,ISTRIP,IData(15,15,10)
INTEGER CEROID,HICEN
C
DO 5 I=1,250
MSET(I) = 0
5 ISET(I) = 0
20 IFF = 1
    IL = 15
    JF = 1
    JL = 15
500 MIN VAL = 999999
    MAX VAL = -999999
C
C *** FOR IVAL
C *** A POSITIVE VALUE INDICATES IVAL OUTSIDE CLUSTER   **
C *** A ZERO VALUE - IVAL IN CLUSTER                      **
C *** A NEGATIVE VALUE INDICATES A NEW CLUSTER          **
C
DC 800 I=IFF,IL
DC 800 J=JF,JL
IVAL=IData(I,J,JMAT)
IF(IVAL = MIN VAL) 700,750,625
625 IF(MAX VAL = IVAL) 650,660,800
C
C *** STORE INDICES FOR I AND J WITH MAXIMAL VALUE IN MSET   **
C *** IK IS A COUNT OF THE VALUES FOUND                      **
C
650 IK = 0
    MAX VAL = IVAL
660 IK = IK+1
    MSET(IK) = I*100+J
    GO TO 800
C
C *** STORE INDICES FOR I AND J WITH MINIMAL VALUE IN ISET   **
C *** IC IS A COUNT OF THE VALUES FOUND                      **
C
700 IC=0
    MIN VAL = IVAL
750 IC = IC+1
    ISET(IC) = I*100+J
800 CONTINUE
    RETURN
    END

```

```

SUBROUTINE CLUST(IC)
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1   SMAX,LWRIT,LDERG,JMAT,JSTRIP,LH
COMMON/PCINT/ INITIAL(3),LAST(3),IPCINT(250),
1 ISET(250),MSET(250),CEROID(250,3)
INTEGER CEROID,HICEN
C
C *** THIS SUBROUTINE FINDS THE MEMBERS OF EACH CLUSTER ***
C *** IPOINT STORES THE INDEX OF ISET FOR THE CURRENT CLUSTER ***
C *** I IS THE BEGINNING OF THE ISET CLUSTER ***
C *** J IS THE CURRENT VALUE IN ISET BEING EVALUATED ***
C *** FOR INCLUSION IN THE CLUSTER ***
C
      I=1
 30 K=1
    IPOINT(1)=I
 35 J = I+1
 40 IVAL = ISET(J)-ISET(I)
 52 IF((IVAL.EG.1).CR.(IVAL.EQ.99).OR.(IVAL.EQ.100).OR.
1   (IVAL.EQ.101)) GO TO 60
C
C *** TRUE - INCREMENT I      ***
IF(IVAL .GT. 101) GO TO 54
C
C *** TRUE - J IS PAST LAST ENTRY  ***
IF(IVAL .LE. 0) GO TO 82
J = J+1
IF( J .GT. (I+16)) GO TO 70
GO TO 40
54 IF((I+1) .EG. J) GO TO 85
    I = I+1
    GO TO 35
C
C *** PLACE IVAL INTO CLUSTER USING ITS INDEX ***
C
 60 DC 62 L=1,K
 62 IF(IPPOINT(L) .EG. J) GO TO 64
    K = K+1
    IPOINT(K) = J
 64 J = J+1
    GO TO 40
C
C *** NO CHANGE IN K INDICATES THAT NO NEW MEMBERS EXIST ***
70 IF(K .EG. 1) GO TO 75
    I = I+1
    GO TO 35
C
C *** ISOLATED POINT ***
75 CALL CALCEN(1)
    I = I+1
    IF(I .GT. IC) RETURN
    GO TO 30

```

```
E2 IF((I+1) .LT. IC) GO TO 84
DC 83 L=1,K
83 IF(IPCINT(L) .EQ. (J-1)) GO TO 90
   I = I+1
   IF(I .GT. IC) GO TO 90
   GO TO 35
84 I = I+1
   GO TO 35
85 CALL CALCEN(K)
   I = I+1
   GO TO 30
C
C *** END CLUSTER ***
C
90 CALL CALCEN(K)
RETURN
END
```

```

SUBROUTINE CALCEN(K)

C *** DETERMINE THE CENTROID OF THE CLUSTER ***
C
COMMON/ICAT/ KMAT,ISTRIP,IData(15,15,10)
COMMON/LCENT/ LCWCEN(250,3),HICEN(250,3),KCET,NLCW,NHI,
I SMAX,LWRIT,LDERG,JMAT,JSTRIP,LF
COMMON/POINT/ INITIAL(3),LAST(3),IPCINT(250),
I ISET(250),MSET(250),CERCID(250,3)
COMMON/SENVEH/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
I SWEA,SWNR,LTRS
INTEGER CEROID,HICEN,HALT

C *** INUM IS THE ROW INDEX - Y COORD   **
C *** JNUM IS THE COLUMN INDEX - X COORD   **
C
KDUM = 0
JNUM = 0
INUM = 0
KCET = KCET+1

C *** CALCULATE THE MEAN VALUES   **
C
DC 100 L=1,K
LL = IPCINT(L)
KDUM = ISET(LL)/100
JNUM = (ISET(LL) - KDUM *100) + JNUM
100 INUM = KDUM + INUM

C *** THIS CALCULATION ADDS A HALF TO ALLOW FOR TRUNCATION   **
C
JNUM = (2*JNUM+K)/(2*K)
INUM = (2*INUM+K)/(2*K)
IF(JNUM .GT. 15) JNUM=15
IF(INUM .GT. 15) INUM=15

C *** NEED TO STORE WHICH ARRAY IS BEING PROCESSED   **
IROW = (JMAT-1)*15+INUM
ICOL = (JSTRIP-1)*15+JNUM
CEROID(KCET,1) = IROW
CEROID(KCET,2) = ICOL
CEROID(KCET,3) = IData(INUM,JNUM,JMAT)
IF(LWRIT .LE. 3) GO TO 10
CALL WRITCL(K)
10 IF(LDERG .EQ. 1) RETURN

C
WRITE(6,900) KDUM,ISTRIP,JMAT,INUM,JNUM,KCET,
1 CEROID(KCET,1),CEROID(KCET,2),CEROID(KCET,3),IROW,ICOL
900 FORMAT(10X,*KDUM ISTRIP JMAT INUM JNUM*,2X,
1 *KCET CEROID(I,1),(I,2),(I,3) IROW ICOL*/
2 10X,E(I5,1X),E,X,3(I6,2X),2(I5,1X))
WRITE(6,901) NLCW,NHI,LALT,HALT,LH

```

```
501 FORMAT(10X,*NLOW NHI LALT HALT LF*/
1      10X,5(I5,1X))
RETURN
END
```

```

SUBROUTINE WRITCL(K)
C
C *** THIS SUBROUTINE WRITES RESULTS OF CLUSTERING ***
C *** LH - 1 IS LOWCEN, 2 IS HICEN ***
C
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEEG,JMAT,JSTRIP,LH
COMMON/PCINT/ INITIAL(3),LAST(3),IPOINT(250),
1 ISET(250),MSET(250),CEROID(250,3)
INTEGER CEROID,HICEN
DATA NEXT,NEXTL,NEXTH/1,1,1/
NEXT = NEXTL
IF(LH .EQ. 2) NEXT=NEXTH
WRITE (6,900)
900 FORMAT(///)
IF(LH .EQ. 1) WRITE(6,901)
IF(LH .EQ. 2) WRITE(6,902)
901 FORMAT(//10X,*LOW ELEVATION CLUSTER*)
902 FORMAT(//10X,*HIGH ELEVATION CLUSTER*)
WRITE (6,903) NEXT,K
WRITE (6,904) (IPOINT(I),I=1,K)
903 FORMAT(5X,*CLUSTER NUMBER *,I4/
1 5X,*TOTAL MEMBERS IN CLUSTER *,I3/)
904 FORMAT(5X,*PCINTERS TO CLUSTER MEMBER*/10(2X,I8))
N1 = IPOINT(1)
N2 = IPOINT(K)
WRITE (6,905) (ISET(I),I=N1,N2)
WRITE (6,906) NEXT,CEROID(KCET,2),CEROID(KCET,1),
1 CEROID(KCET,3)
905 FORMAT(/5X,*PACKED CLUSTER LOCATION RCW-COLUMN*/10(2X,I8))
906 FORMAT( // 5X,*CENTER OF CLUSTER NUMBER *,I4/
1 5X,*X-COORD*,I4,* Y-COORD*,I4,* Z-COORD*,I4//)
NEXT = NEXT+1
IF(LH .EQ. 1) NEXTL=NEXT
IF(LH .EQ. 2) NEXTH=NEXT
RETURN
END

```

SUBROUTINE LINKAGE

```

C
C *** LINKAGE ROUTINE
C *** IPCINT HAS LIST OF NEIGHBORHOOD POINTS
C *** NODE - NODE NUMBER OF POINT BEING EVALUATED
C *** NLOW - NUMBER OF POINTS IN LOWCEN
C *** NHI - NUMBER OF POINTS IN HICEN
C *** LNEBR - POINTS IN NEIGHBORHOOD FOR LOWCEN
C *** KNEBR - POINTS IN NEIGHBORHOOD FOR HICEN
C
C     COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1     SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
     COMMON/POINT/ INITIAL(3),LAST(3),IPCINT(250)
     COMMON/SENVH/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
1     SWEA,SWNR,LTRS
     COMMON/SRAD/ RANGE,RE,MDIM,RATE,NSITE,ISITE(10,3),SYSR(10)
     COMMON/KINK/ LINK(250),LINKTO(1500,3),NBLKS,IC,
1     IRADIUS,LNEBR,KNEBR
     COMMON/DET/ DETLO(250),DETHI(250),FROM(250),TO(250,2)
     COMMON/EDGE/ DIST(100,2),IRCW,JCCL,LSTR
     DIMENSION MPCINT(125),SR(10,3),NLIST(250)
     INTEGER HICEN,GRID,FROM,TO,SWEA,SWNR
     INTEGER EAST1,EAST2
     EQUIVALENCE (IPOINT(126),MPOINT(1))
     DATA IRADIUS/15/
     DATA DETLO,DETHI/500*0/
     DATA SMAX,RTCD/100.0,57.2957795131/

C
     NBLKS = CLDS = 1
     IFREE = KFIRST = KLAST = 0
     LTOTAL = 0

C
C *** SORT LOWCEN AND HICEN **
C
     CALL LHSCRT(KFIRST,KLAST)

C
C *** DEVELOP NETWKRK **
C
     CALL RADIAL
     DC 10 I=1,250
     FROM(I) = 0
     TO(I,1) = 0
10    TO(I,2) = 0

C
C *** CONSTRUCT ROLTE **
C
     15 IC      = 1
     NODE    = KFIRST
     NEWPT   = NODE

C
C *** FIND NEIGHBORHOOD ABOUT A LOW POINT **
C

```

```

20 IROW = LOWCEN(NODE,1)
JCOL = LOWCEN(NODE,2)
LCWCEN(NODE,1) = -(1000000+IROW)
LOWCEN(NODE,2) = -(1000000+JCOL)
CALL NEIGHB(NODE)
CALL DIFFER(NODE)

C
30 FROM(IC) = NEWPT
IF(LWRIT .LE. 2) GO TO 35
WRITE(6,921) NODE,JCOL,IROW,NEWPT,LLEN,IC
35 XI = LAST(2)-JCOL
YJ = LAST(1)-IROW
KANG = RTOD*(ATAN2(YJ,XI))
RANG = SGRT(XI**2 + YJ**2)
DO 50 I=1,NSITE
XI = ISITE(I,2)-JCOL
YJ = ISITE(I,1)-IROW
SR(I,1) = SGRT(XI**2 + YJ**2)
IF((XI .EG. C.0) .OR. (SR(I,1) .EG. 0)) GO TO 50
SR(I,2) = RTCO*(ATAN2(YJ,XI))
SR(I,3) = ABS(RTOD*(ATAN2(SYSR(I),SR(I,1))))
50 CONTINUE
C
C ***      FIND MIN PENALTY VALUE      **
C ***      ANGLE HEADING IS MEASURED FROM X-AXIS      **
C ***      IAK ANGLE IS MEASURED FROM HEADING      **
C ***      THREE WEIGHTING SCHEMES      **
C ***      HEADING, RADAR AVOIDANCE, TERMINAL      **
C
LLEN = 1000000
LA = LINK(IC)
LE = LINK(IC+1)-1
IF(LB .LE. 0) LE=IFREE
DO 200 LL=LA,LB
NJ = LINKTO(LL,1)
IF(NJ .LT. 0) GO TO 120
IX = LOWCEN(NJ,2)
JY = LOWCEN(NJ,1)
GO TO 125
120 IX = HICEN(-NJ,2)
JY = HICEN(-NJ,1)
125 XI = IX-JCOL
YJ = JY-IRCW
RA = SGRT(XI**2 + YJ**2)
IANG = RTCO*(ATAN2(YJ,XI))
IAK = IANG-KANG
IF(IAK .GT. 180) IAK=360-IAK
IF(IAK .LT.-180) IAK=360+IAK
C
C *** HEADING WEIGHTING  **
C
AWEIG = (IABS(IAK))/90+1

```

```

IF(RANG .GT.RANGE) GO TO 130
C
C *** TERMINAL WEIGHTING ***
C
NWEIG = 2*(IABS(IAK)/45)+1
IF(RA .GT. RANG) NWEIG=100*NWEIG
GO TO 150
C
C *** RADAR AVOIDANCE WEIGHTING ***
C
130 IF(SYSR(1) .LE. 0.0) GO TO 150
DO 135 I=1,NSITE
ANG = IANG
ANG = ABS(SR(I,2)-ANG)
IF(ANG .GT. SR(I,3)) GO TO 135
NWEIG = 2
IF(RA .GT. (SR(I,1)-SYSR(I))) NWEIG=10
GO TO 150
135 CONTINUE
150 NPEN = NWEIG*LINKTO(LL,2)+NWEIG
LINKTO(LL,3) = NPEN
C
IF(LWRIT .LE. 2) GO TO 175
WRITE(6,520) NODE,NJ,LA,LB,IC,IFREE,RANGE,RANG,RA
WRITE(6,524) IAK,IANG,KANG,NWEIG,LPEM,NPEN,XI,YJ
175 IF(NPEN .GE. LPEN) GO TO 200
LPEN = NPEN
NEWPT = LINKTC(LL,1)
200 CONTINUE
C
IF(LWRIT .GT. 2) WRITE(6,521) NODE,JCOL,IROW,NEWPT,LPEN,IC
IF(NEWPT .EG. KLAST) GO TO 475
NCDE = NEWPT
TC(IC,1) = NEWPT
TC(IC,2) = LPEN
IC = IC+1
LTOTAL = LTOTAL+LPEN
IF(IC .GE. 1950) CALL RITE
IF(IFREE .GE. 1800) CALL RITE
IF(NODE .LT. 0) GO TO 400
GO TO 20
C
C *** FIND NEIGHBORHOOD ABOUT A HIGH POINT ***
C
400 NODE = -NEWPT
IROW = HICEN(NODE,1)
JCOL = HICEN(NODE,2)
HICEN(NODE,1) = -(1000000+IROW)
HICEN(NODE,2) = -(1000000+JCOL)
CALL NEIGHB(NODE)
CALL DIFFER(NCDE)
GO TO 30

```

```

450 IF(IFLAG .EQ. -1) GO TO 475
    IFLAG = -1
    IRADUS = 2*IRADLS
    GO TO 15
475 TO(IC,1) = NEWPT
    TO(IC,2) = LPEN
C
C *** CHECK FOR DATA BLOCKS WRITTEN TO WORKING STORAGE ***
C
    IF(NBLKS .GT. 1) GO TO 700
C
C *** REMOVE LARGE NEGATIVE VALUE FROM ROUTE NODES ***
C
480 DO 500 I=1,IC
    NN = FROM(I)
    IF(NN .LT. 0) GO TO 485
    LCWCEN(NN,1) = -(LCWCEN(NN,1)+1000000)
    LCWCEN(NN,2) = -(LCWCEN(NN,2)+1000000)
    GO TO 500
485 NN = -NN
    HICEN(NN,1) = -(HICEN(NN,1) +1000000)
    HICEN(NN,2) = -(HICEN(NN,2) +1000000)
500 CONTINUE
C
C *** WRITE NODE POINTS OF THE ROUTE ***
C
    LL = 0
    WRITE(6,910)
    DO 650 I=1,IC
    LL = LL+1
    NOD1 = FROM(I)
    NOD2 = TC(I,1)
    IF(NOD1 .LT. 0) GO TO 550
    NCRTH1 = GRIC*LOWCEN(NOD1,1)+SWNR
    EAST1 = GRIC*LOWCEN(NOD1,2)+SWEA
    IF(NOD2 .LT. 0) GO TO 575
525 NORTH2 = GRIC*LOWCEN(NOD2,1)+SWNR
    EAST2 = GRIC*LOWCEN(NOD2,2)+SWEA
    GO TO 600
550 NOD1 = -NOD1
    NORTH1 = GRIC*HICEN(NOD1,1)+SWNR
    EAST1 = GRIC*HICEN(NOD1,2)+SWEA
    IF(NOD2 .GT. 0) GO TO 525
575 NOD2 = -NOD2
    NORTH2 = GRIC*HICEN(NOD2,1)+SWNR
    EAST2 = GRIC*HICEN(NOD2,2)+SWEA
600 WRITE(6,911) FROM(I),EAST1,NORTH1,TO(I,1),
    1           TO(I,2),EAST2,NORTH2
    IF(LL .LE. 25) GO TO 650
    WRITE(6,910)
    LL = 0
650 CONTINUE

```

```

      WRITE(6,512) LTRS,SWEA,SWNR,LTOTAL
      CALL WRLINK
      ICK = IC-1
      LA = 0
      K = 1
      DO 800 I=1,ICK
      IF(K .GE. IC) GO TO 850
      LA = LA+1
      NJ = FROM(I)
      NN = TC(K,1)
      NLIST(LA) = NJ
      IF(NJ .LT. 0) GO TO 670
      JCOL = LCWCEN(NJ,2)
      IROW = LCWCEN(NJ,1)
      GO TO 675
 670  JCOL = HICEN(-NJ,2)
      IROW = HICEN(-NJ,1)
 675  IF(NN .LT. 0) GO TO 680
      IX = LCWCEN(NN,2)
      JY = LCWCEN(NN,1)
      GO TO 685
 680  IX = HICEN(-NN,2)
      JY = HICEN(-NN,1)
 685  XI = IX-JCCL
      YJ = JY-IROW
      DISA = SQRT(XI**2 + YJ**2)
      K = K+1
      LL = K
      DO 800 J=LL,IC
      NJ = TC(J,1)
      IF(NJ .LT. 0) GO TO 690
      IX = LCWCEN(NJ,2)
      JY = LCWCEN(NJ,1)
      GO TO 695
 690  IX = HICEN(-NJ,2)
      JY = HICEN(-NJ,1)
 695  XI = IX-JCCL
      YJ = JY-IROW
      DISB = SQRT(XI**2 + YJ**2)
      IF(DISB .GT. DISA) GO TO 800
      K = J+1
      DISA = DISB
 800  CONTINUE
      I = ICK+1
      LA = LA+1
      NLIST(LA) = FROM(I)
 850  CONTINUE
      NLIST(LA+1) = TO(IC,1)
      WRITE(6,515)
      DO 875 J=1,LA
 875  WRITE(6,916) NLIST(J),NLIST(J+1)

```

C

```

IF(NBLKS .LT. CLCE) GO TO 710
RETURN
700 CALL RITE
OLDB = NBLKS-1
REWIND 9
710 READ(9) NBLKS,IFREE,IC
READ(9) ((FROM(I),I=1,IC)
READ(9) ((TO(I,J),J=1,2),I=1,IC)
READ(9) (LINK(I),I=1,IC)
READ(9) ((LINKTO(I,J),J=1,3),I=1,IFREE)
GO TO 480
C
910 FORMAT(1H1////30X,*TABLE      NODE LINKAGE FOR ROUTE//*
1 19X,*FRCM*,4X,*EASTING*,2X,*NORTHING*,
2 6X,*TO*,4X,*PENALTY*,3X,*EASTING*,2X,*NORTHING*)
911 FORMAT(18X,I5,2X,2(I9,1X),2X,I5,2X,3(I5,1X))
912 FFORMAT( //19X,*SOUTHWEST CORNER *,A2,2I4//*
1 110X,*TOTAL PENALTY*/110X,*RUNNING TOTAL*/110X,I12)
915 FFORMAT(1H1////30X,*TABLE      MODIFIED ROUTE//*
1 37X,*FROM*,5X,*TO*)
916 FFORMAT(36X,I5,2X,I5)
920 FFORMAT(/6X,*NODE NJ LA LB IC IFREE RANGE*,*
1 6X,*RANG RA*/5X,6(I4,1X),3(F8.3,1X))
921 FORMAT(10X,*NODE X-CRD Y-CRD*/10X,3(I4,1X)/10X,*NEWPT*,*
1 2X,*LPEN IC*/10X,I4,1X,I10,1X,I4)
924 FFORMAT( 8X,*IAK IANG KANG NWEIG LPEN*,*
1 7X,*NPEN*, 5X,*XI*,10X,*YJ*/
1 5X,I5,1X,I5,1X,I5,1X,I5,1X,I10,1X,I10,2(F10.4,1X))
END

```

```

SUBROUTINE LHSORT(KFIRST,KLAST)
C
C *** THIS SUBROUTINE SORTS LOWCEN AND HICEN ***
C *** IN ASCENDING ORDER BY ROWS ***
C
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLCW,NFI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250)
INTEGER HICEN
C
NLOW = NLOW+1
LOWCEN(NLOW,1) = INITIAL(1)
LOWCEN(NLOW,2) = -INITIAL(2)*LAST(2)
LOWCEN(NLOW,3) = INITIAL(3)
NLOW = NLOW+1
LOWCEN(NLOW,1) = LAST(1)
LOWCEN(NLOW,2) = -LAST(2)
LOWCEN(NLOW,3) = LAST(3)
C
C *** LOWCEN ***
C
KK = NLOW-1
DO 10 J=1,KK
JJ = J+1
DO 10 I=JJ,NLOW
IF(LOWCEN(J,1) .LE. LOWCEN(I,1)) GO TO 10
IS1 = LOWCEN(J,1)
IS2 = LOWCEN(J,2)
IS3 = LOWCEN(J,3)
LOWCEN(J,1) = LOWCEN(I,1)
LOWCEN(J,2) = LOWCEN(I,2)
LOWCEN(J,3) = LOWCEN(I,3)
LOWCEN(I,1) = IS1
LOWCEN(I,2) = IS2
LOWCEN(I,3) = IS3
10 CONTINUE
C
IS2 = -INITIAL(2)*LAST(2)
DO 15 I=1,NLCW
IF(LOWCEN(I,2) .GT. 0) GO TO 15
IF(LOWCEN(I,2) .EQ. IS2) KFIRST=I
IF(LOWCEN(I,2) .EQ. -LAST(2)) KLAST=I
15 CCNTINUE
WRITE(6,907) INITIAL(2),LAST(2),IS2,LOWCEN(KFIRST,2),
1 LOWCEN(KLAST,2),KFIRST,KLAST
907 FORMAT(/ 2X,*INITIAL*,2X,*LAST*,4X,*IS2*,6X,*LOWCEN-1*,
1 2X,*LOWCEN-L*,2X,*KFIRST*,3X,*KLAST*/2X,7(16,2X))
LOWCEN(KFIRST,2) = INITIAL(2)
LOWCEN(KLAST,2) = LAST(2)
WRITE(6,906)
WRITE(6,900)
KL = 0

```

```

DO 20 I=1,NLCW+10
KK = I-1+10
IF(KK .GT. NLCW) KK=NLOW
KL = KL+1
WRITE(6,901) (LOWCEN(J,2),J=I,KK)
WRITE(6,902) (LOWCEN(J,1),J=I,KK)
WRITE(6,903) (LOWCEN(J,3),J=I,KK)
IF(KL .LE. 7) GO TO 20
WRITE(6,906)
WRITE(6,900)
KL = 0
20 CONTINUE
WRITE(6,904) NLOW
C
C *** HICEN ***
C
KK = NHI-1
DO 30 J=1,KK
JJ = J+1
DO 30 I=JJ,NFI
IF(HICEN(J,1) .LE. HICEN(I,1)) GO TO 30
IS1 = HICEN(J,1)
IS2 = HICEN(J,2)
IS3 = HICEN(J,3)
HICEN(J,1) = HICEN(I,1)
HICEN(J,2) = HICEN(I,2)
HICEN(J,3) = HICEN(I,3)
HICEN(I,1) = IS1
HICEN(I,2) = IS2
HICEN(I,3) = IS3
30 CONTINUE
C
WRITE(6,906)
WRITE(6,905)
KL = 0
DO 40 I=1,NHI+10
KK = I-1+10
IF(KK .GT. NFI) KK=NHI
KL = KL+1
WRITE(6,901) (HICEN(J,2),J=I,KK)
WRITE(6,902) (HICEN(J,1),J=I,KK)
WRITE(6,903) (HICEN(J,3),J=I,KK)
IF(KL .LE. 7) GO TO 40
WRITE(6,906)
WRITE(6,905)
KL = 0
40 CONTINUE
WRITE(6,904) NFI
WRITE(6,906)
C
900 FORMAT(//////40X,*TABLE      LOW ELEVATION NODE POINTS*)
901 FORMAT(18X,*X-COORDINATE *,10I7)

```

```
902 FORMAT(18X,*Y-COORDINATE *,10I7)
903 FORMAT(18X,*Z-COORDINATE *,10I7/)
904 FORMAT(//18X,*NUMBER OF NODES *,I5)
905 FORMAT(////40X,*TABLE      HIGH ELEVATION NODE POINTS*)
906 FORMAT(1H1)
      RETURN
      END
```

```

SUBROUTINE NEIGHB(NODE)
C
C *** IROW IS ROW INDEX (Y-COORD) BEING EVALUATED **
C *** JCOL IS COLUMN INDEX (X-COORD) ***
C *** NODE LOCATION CURRENTLY BEING PROCESSED ***
C
      COMMON/LCENT/ LCWCEN(250,3),HICEN(250,3),KCET,NLOW,RHI,
      1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
      COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250)
      COMMON/SENVET/ LALT,HALT,SENALT,VELALT,IFREE,GRID,
      1 SWEA,SWNR,LTRS
      COMMON/KINK/ LINK(250),LINKTO(1500,3),NBLKS,IC,
      1 IRADUS,LNEBR,KNEBR
      COMMON/EDGE/ DIST(100,2),IROW,JCOL,LSTR
      DIMENSION MPOINT(125)
      INTEGER HICEN
      EQUIVALENCE (IPOINT(125),MFCINT(1))

C
      IRAD = IRADUS
      10 LA = IROW-IRAD
      IF(LA .LE. 0) LA=1
      LB = IROW+IRAD
C
C *** IBEG IS THE INDEX VALUE WHERE LA = RCW NUMBER ***
C *** IEND IS THE INDEX VALUE WHERE LB+1 = RCW # ***
C *** IPOINT HAS INDEX VALUE OF LOWCEN FOR NEIGHBORHOOD ***
C *** THIS RESTRICTS THE SEARCH TO ONLY THOSE RCWS ***
C *** THAT ARE NEAR THE "NODE" ***
C
      DO 100 I=1,NLCW
      NROW = LCWCEN(I,1)
      IF(NROW .LT. LA) GO TO 100
      IBEG = I
      GO TO 101
100  CCNTINUE
101  DO 102 I=IBEG,NLOW
      NROW = LOWCEN(I,1)
      IF(NROW .LT. LB) GO TO 102
      IEND = I
      GO TO 103
102  CONTINUE
C
C *** FIND THE NEIGHBORHOOD OF LOW ELEVATION POINTS ***
C
      103 LNEBR = 0
      DO 104 I=IBEG,IEND
      IF(LOWCEN(I,1) .LT.-1000000) GO TO 104
      LDIFF = IABS(LOWCEN(I,1)-IROW)
      IF(LDIFF .GT. IRAD) GO TO 104
      LDIFF = IABS(LOWCEN(I,2)-JCOL)
      IF(LDIFF .GT. IRAD) GO TO 104
      LNEBR = LNEBR+1

```

```

        IF(LNEBR .EQ. 100) GO TO 400
        IPOINT(LNEBR) = I
104    CONTINUE
        IF(LNEBR .EQ. 0)    GO TO 300
125    IFLAG = 0
        DO 200 I=1,NFI
        NROW = HICEN(I,1)
        IF(NROW .LT. LA)    GO TO 200
        IBEG = I
        GO TO 201
200    CONTINUE
201    DO 202 I=IBEG,NHI
        NROW = HICEN(I,1)
        IF(NROW .LT. LB)    GO TO 202
        IEND = I
        GO TO 203
202    CCNTINUE
C
C *** FIND THE NEIGHBORHOOD OF HIGH ELEVATION POINTS ***
C
203    KNEBR = 0
        DO 204 I=IBEG,IEND
        IF(HICEN(I,1) .LT.-1000000) GO TO 204
        LDIFF = IABS (HICEN(I,1)-IROW)
        IF(LDIFF .GT. IRAD) GO TO 204
        LDIFF = IABS (HICEN(I,2)-JCOL)
        IF(LDIFF .GT. IRAD) GO TO 204
        KNEBR = KNEBR+1
        IF(KNEBR .GT. 100) GO TO 500
        MPOINT(KNEBR) = I
204    CONTINUE
        IF(LWRIT .LE. 2) RETURN
        WRITE(6,500) NODE,JCOL,IROW
        DO 275 N1=1,LNEBR
        N2 = IPOINT(N1)
275    WRITE(6,901) N1,N2,LOWCEN(N2,2),LOWCEN(N2,1),LOWCEN(N2,3)
        WRITE(6,902)
        DO 285 N1=1,KNEBR
        N2 = MPOINT(N1)
285    WRITE(6,901) N1,N2,HICEN(N2,2),HICEN(N2,1),HICEN(N2,3)
C
900    FORMAT(/EX,* PRIMARY NODE *,I4,I5,* ,X-COORD *,
1 I5,* ,Y-COORD*/10X,*LOW POINTS*)
901    FORMAT(10X,*NEIGHB - *,I3,* NODE *,I3,* .*,I5,
1 *,X-COORD *,I5,* ,Y-COORD*,I5,* ,Z-COORD*)
902    FORMAT(10X,*HIGH POINTS*)
        RETURN
C
C *** THIS ENSURES THAT AT LEAST ONE POINT BUT NOT MORE ***
C *** THAN 100 POINTS ARE FOUND ***
C
300    IRAD = 2*IRAC

```

AD-A091 793

ARMY MISSILE COMMAND REDSTONE ARSENAL AL PLANS ANAL--ETC F/G 15/3
A HEURISTIC ROUTE SELECTION MODEL FOR LOW LEVEL AIRCRAFT FLIGHT--ETC(U)
MAY 80 M J DORSETT

UNCLASSIFIED

DRSMT/D-AD-5-TR

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MH

3-3

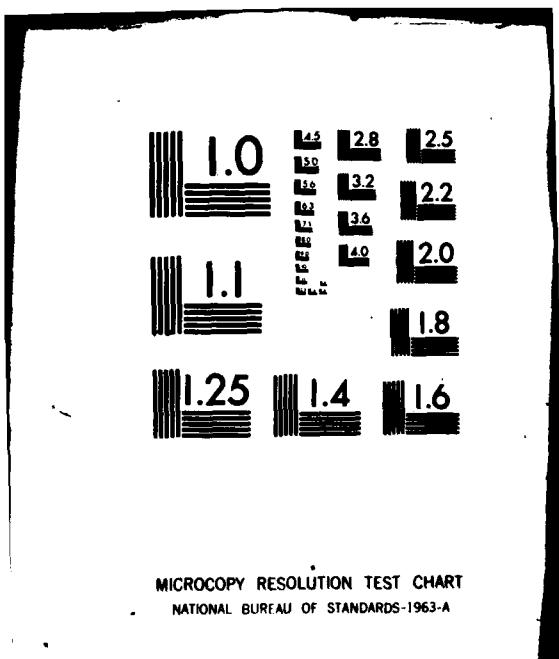
END

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DTIC



```
IF(IRAD .GT. 999999) RETURN
GO TO 10
400 IRAD = IRAD/2
IF(IRAD .EQ. 0) GO TO 450
GO TO 10
450 LNEBR = 100
GO TO 125
500 IF(IFLAG .EQ. 1) GO TO 600
IRAD = IRAD/2
IFLAG = 1
GO TO 203
600 KNEBR = 100
RETURN
END
```

```

SUBROUTINE DIFFER(NODE)

C
C *** THIS SUBROUTINE FINDS RANGE OF HEIGHT AND DISTANCE **
C *** DIST(I,1) = THE PLANAR DIST TO PCINT FOR LOWCEN   **
C *** CIST(I,2) = THE PLANAR DIST TO PCINT FOR HICEN    **
C *** DMIN = MIN DIST BETWEEN NODE AND ADJACENT POINTS  **
C *** DMAX = MAX DIST BETWEEN NODE AND ADJACENT POINTS  **
C *** KZMIN = MIN ELEVATION BETWEEN NODE AND ADJ PTS    **
C *** KZMAX = MAX ELEVATION BETWEEN NODE AND ADJ PTS    **
C
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250)
COMMON/SENVER/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTRS
COMMON/KINK/ LINK(250),LINKTO(1500,3),NELKS,IC,
1 IRADLS,LNEBR,KNEER
CCMMON/DET/ DETL0(250),DETFI(250),FRCM(250),TO(250+2)
CCMMON/EDGE/ DIST(100,2),IRCW,JCCL,LSTR
DIMENSION MPOINT(125)
INTEGER HICEN
EQUIVALENCE (IFCINT(126),MPOINT(1))
DATA RTDC,LSTR/57.2957795131+1/

C
C *** INITIALIZE VARIABLES **
C
DO 10 I=1,100
CIST(I,1) = 0.0
10 DIST(I,2) = 0.0
DMIN = 1000000
DMAX = -1000000
KZMIN = 1000000
KZMAX = -1000000
C
C *** PROCESS LOWCEN
C
DC 130 I=1,LNEER
J = IPOINT(I)
YJ = LOWCEN(J,1)-IROW
XI = LOWCEN(J,2)-JCOL
KZI = LOWCEN(J,3)
IF(KZI .GE. KZMIN) GO TO 15
KZMIN = KZI
15 IF(KZI .LE. KZMAX) GO TO 20
KZMAX = KZI
20 CONTINUE
DIST(I,1) = SQRT(XI**2+YJ**2)
IF(DIST(I,1) .GE. DMIN) GO TO 120
DMIN = DIST(I,1)
120 IF(DIST(I,1) .LE. DMAX) GO TO 130
DMAX = DIST(I,1)
130 CCNTINUE

```

```

C
C *** PROCESS HICEN ***
C
      DO 150 I=1,KNEBR
      J    = MPOINT(I)
      YJ  = HICEN(J,1)-IROW
      XI  = HICEN(J,2)-JCOL
      KZI = HICEN(J,3)
      IF(KZI .GE. KZMIN) GO TO 35
      KZMIN = KZI
      GO TO 45
  35 IF(KZI .LE. KZMAX) GO TO 45
      KZMAX = KZI
  45 CONTINUE
      DIST(I,2) = SQRT(XI**2+YJ**2)
      IF(DIST(I,2) .GE. DMIN) GO TO 140
      DMIN = DIST(I,2)
      GO TO 150
  140 IF(DIST(I,2) .LE. DMAX) GO TO 150
      DMAX = DIST(I,2)
  150 CONTINUE
      IF(LWRIT .LE. 2) GO TO 75
      WRITE(6,900) NODE,JCOL,IROW,LNEBR
      DO 50 LA=1,LNEBR,10
      LB = LA-1+10
      IF(LB .GT. LNEBR) LB=LNEER
  50 WRITE(6,501) (DIST(I,1),I=LA,LB)
      WRITE(6,500) NODE,JCOL,IROW,KNEBR
      DO 60 LA=1,KNEBR,10
      LE = LA-1+10
      IF(LE .GT. KNEBR) LE=KNEER
  60 WRITE(6,502) (DIST(I,2),I=LA,LE)
C
C *** SCRT IN INCREASING ORDER ***
C
      75 IF(LNEBR .EQ. 1) GO TO 85
      KK = LNEBR-1
      DO 250 J=1,KK
      JJ = J+1
      DO 250 I=JJ,LNEER
      IF(DIST(J,1) .LE. DIST(I,1)) GO TO 250
      SA1 = DIST(J,1)
      JSA = IPCINT(J)
      DIST(J,1) = DIST(I,1)
      IPOINT(J) = IPOINT(I)
      DIST(I,1) = SA1
      IPOINT(I) = JSA
  250 CONTINUE
  85 IF(KNEBR .EQ. 1) GO TO 300
      KK = KNEBR-1
      DO 275 J=1,KK
      JJ = J+1

```

```

DO 275 I=JJ,KNEBR
IF(DIST(J,2) .LE. DIST(I,2)) GO TO 275
SA1 = DIST(J,2)
JSA = MPOINT(J)
DIST(J,2) = DIST(I,2)
MPOINT(J) = MPOINT(I)
DIST(I,2) = SA1
MPOINT(I) = JSA
275 CONTINUE
IF(LWRIT .LE. 2) GO TO 300
WRITE(6,903) DMIN,DMAX,KZMIN,KZMAX
WRITE(6,900) NODE,JCOL,IROW,LNEBR
DO 90 LA=1,LNEBR,10
LB = LA-1+10
IF(LB .GT. LNEBR) LB=LNEBR
90 WRITE(6,901) (DIST(I,1),I=LA,LB)
WRITE(6,900) NCDE,JCOL,IROW,KNEBR
CO 95 LA=1,KNEBR,10
LB = LA-1+10
IF(LB .GT. KNEBR) LB=KNEBR
95 WRITE(6,902) (DIST(I,2),I=LA,LB)

C *** CALCULATE PENALTY VALUE FOR POINTS ***
C
300 DRANG = DMAX-DMIN
IF(DRANG .GT. 0.0) DRANG=1.0/DRANG
ZRANG = KZMAX-KZMIN+1
IF(ZRANG .GT. 0.0) ZRANG=1.0/ZRANG
CO 320 I=1,LNEBR
IFREE = IFREE+1
IJ = IPOINT(I)
LINKTO(IFREE,1) = IJ
XYZ = LOLCEN(IJ,3)-KZMIN
XYZ = DETLC(IJ)+XYZ*ZRANG
320 LINKTO(IFREE,2) = 100.0*(XYZ+1-(DIST(I,1)-DMIN)*DRANG)
CO 325 I=1,KNEBR
IFREE = IFREE+1
IJ = MPCINT(I)
LINKTO(IFREE,1) = -IJ
XYZ = HICEN(IJ,3)-KZMIN
XYZ = DETHI(IJ)+XYZ*ZRANG
325 LINKTO(IFREE,2) = 100.0*(XYZ+1-(DIST(I,2)-DMIN)*DRANG)
LINK(IC) = LSTR
LSTR = IFREE+1

C
900 FCRMAT(/ 5X,*FROM DIFFER* / 5X,*NODE *,I4,I5,* ,X-COORD *,
1 I5,* ,Y-COORD *,I5,* ,LINKS*)
901 FORMAT( 5X,*CISTANCE LOW *,10(1X,F10.3))
902 FCRMAT( 5X,*CISTANCE HIGH *,10(1X,F10.3))
903 FCRMAT(11X,*CPIN*,8X,*DMAX KZMIN KZMAX*/
1 5X,2(F10.4,2X),I4,2X,I4)
RETURN
END

```

```
SUBROUTINE RITE
C
C *** THIS SUBROUTINE SAVES ARRAYS IN WORKING STORAGE ***
C
COMMON/SENVEH/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTPS
COMMON/KINK/ LINK(250),LINKTO(1500+3),NELKS,IC,
1 IRADUS,LNEBR,KNEBR
COMMON/DET/ DETL0(250),DETHI(250),FRCM(250),TO(250,2)
COMMON/EDGE/ DIST(100+2),IRCW,JCCL,LSTR
INTEGER FROM,TC
C *** BINARY UNFORMATTED TAPE ***
WRITE(9) NBLKS,IFREE,IC
WRITE(9) (FROM(I),I=1,IC)
WRITE(9) ((TC(I,J),J=1,2),I=1,IC)
WRITE(9) (LINK(I),I=1,IC)
WRITE(9) ((LINKTC(I,J),J=1,3),I=1,IFREE)
IFREE = IC = LSTR = 1
NELKS = NBLKS+1
RETURN
END
```

```

SUBROUTINE WRLINK
C
C *** THIS SUB* WRITES THE LINKAGE THAT'S BEEN DEVELOPED ***
C
      COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
      1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
      COMMON/POINT/ INITIAL(3),LAST(3),IPOINT(250)
      COMMON/SENVER/ LALT,FALT,SENALT,VEHALT,IFREE,GRID,
      1 SWEA,SWNR,LTRS
      COMMON/RINK/ LINK(250),LINKTO(1500,3),NBLKS,IC,
      1 IRADUS,LNEBR,KNEBR
      COMMON/DET/ DETLC(250),DETFI(250),FROM(250),TO(250,2)
      INTEGER HICEN,FROM,TO
      WRITE(6,500)
500  FCRMAT(1H1 /10X,*NODE LINKAGE CUTFUT*)
      WRITE(6,501) IFREE,NBLKS,NLOW,IRADUS
901  FCRMAT(10X,*IFREE NELKS      NLOW      IRADUS*/
      1 10X,4(1E,1X))
      NM = IFREE+1
      CC 15 NA=1,NM,10
      NB = NA-1+10
      15 WRITE(6,502) (LINKTO(I,1),I=NA,NE),(LINKTC(I,2),I=NA,NB),
      1 (LINKTO(I,3),I=NA,NB)
902  FORMAT(1GX,*LINKTO(I,1)  *,10(2X,I6)/
      1     10X,*LINKTO(I,2)  *,10(2X,I6)/
      2     10X,*LINKTO(I,3)  *,10(2X,I6)/)
      WRITE(6,503)
903  FORMAT(1H1)
      WRITE(6,504)
      CO 10 J=1,IC,10
      JJ = J-1+10
      IF(JJ .GT. IC) JJ=IC
      10 WRITE(6,505) (LINK(I),I=J,JJ)
904  FORMAT(/10X,*LINKAGE POINTERS*/)
905  FCRMAT(10X,10(1E,2X))
      KC = 0
      DC 20 NJ=1,IC
      IF(KC .EG. 0) WRITE(6,906)
      KC = KC+1
      NN = FROM(NJ)
      J = LINK(NJ)
      JJ = LINK(NJ+1)-1
      IF(JJ .LT. 0) JJ=IFREE
      JJJ= JJ-J+1
      WRITE(6,507) NN,JJJ
      IF(NN .GT. 0) WRITE(6,908) LOWCEN(NN,2),
      1           LOWCEN(NN,1),LOWCEN(NN,3)
      IF(NN .LT. 0) WRITE(6,908) HICEN(-NN,2),
      1           HICEN(-NN,1),HICEN(-NN,3)
      WRITE(6,909) (LINKTO(I,1),I=J,JJ)
      WRITE(6,910) (LINKTO(I,2),I=J,JJ)
      WRITE(6,911) (LINKTO(I,3),I=J,JJ)

```

```
IF(KC .LE. 5) GO TO 20
KC = 0
20 CONTINUE
C
906 FORMAT(1H1/////////34X,*NODE LINKAGE*)
907 FORMAT(/20X,*NODE NO.,*,I5,* TOTAL LINKS *,I4)
908 FORMAT(20X,*X,Y,Z COORDINATE *,I4,1H9 ,1X,I4,1H9 ,1X,I4)
909 FORMAT(20X,*LINKED TO *,10I7)
910 FORMAT(20X,*EXPOSURE   *,10I7)
911 FORMAT(20X,*WEIGHTED   *,10I7)
RETURN
END
```

```
SUBROUTINE SAVE
C
C *** THIS ROUTINE IS USED TO WRITE VALUES OUT FOR PLOTTING ***
C
COMMON/LCENT/ LOWCEN(250,3),HICEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEBG,JMAT,JSTRIP,LH
COMMON/SENVER/ LALT,HALT,SENALT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTRS
COMMON/KINK/ LINK(250),LINKTO(1500,3),NELKS,IC,
1 IRADIUS,LNEBR,KNEBR
COMMON/DET/ DETLC(250),DETHI(250),FRCP(250),TO(250,2)
INTEGER ICEN,FROM,TO
C
      WRITE(7,900) NLOW,NHI,IC,IFREE
      WRITE(7,901) ((LOWCEN(I,J),J=1,3),I=1,NLOW)
      WRITE(7,901) ((HICEN(I,J),J=1,3),I=1,NHI)
      WRITE(7,902) (DETLC(I),I=1,NLOW)
      WRITE(7,902) (DETHI(I),I=1,NHI)
      WRITE(7,901) (FROM(I),I=1,IC)
      WRITE(7,901) ((TO(I,J),J=1,2),I=1,IC)
      WRITE(7,901) (LINK(I),I=1,IC)
      WRITE(7,901) ((LINKTO(I,J),J=1,3),I=1,IFREE)
900 FORMAT(4I10)
901 FORMAT(10(I9,1X))
902 FORMAT(10F10.3)
      RETURN
      END
```

```

SUBROUTINE RADIAL

C
C *** THIS ROUTINE CALCULATES THE LINE OF SIGHT (LOS)    **
C *** BETWEEN NODE FCINT AND SENSORS. LOS IS THE          **
C *** INTERVISIBILITY BETWEEN PTS. ONCE ANY TERRAIN        **
C *** MASKING POINT IS FOUND PROCESSING OF THAT NODE-    **
C *** SENSOR COMBINATION IS FINISHED.                      L**
C

COMMON/ICAT/ KMAT,ISTRIP,IData(15,15,10)
COMMON/LCENT/ LCWCEN(250,3),HCEN(250,3),KCET,NLOW,NHI,
1 SMAX,LWRIT,LDEEG,JMAT,JSTRIP,LH
COMMON/PCINT/ INITIAL(3),LAST(3),IPOINT(250)
COMMON/SENVER/ LALT,FALT,SENALT,VEHALT,IFREE,GRID,
1 SWEA,SWNR,LTRS
COMMON/SRAD/ RANGE,RE,MDIM,RATE,NSITE,ISITE(10,3),SYSR(10)
COMMON/DET/ DETLC(250),DETHI(250),DISLC(250),
1 DISHI(250),XX(250)
DIMENSION IFINISH(250)
INTEGER SENALT,VEHALT,HICEN,EAST,WEST,SOUTH,GRID
LOGICAL ZCLRVE,ZNORTH,ZSOUTH
EQUIVALENCE (RMAX,DIS)
DATA RE,SRTWH,RATE/490200.0,0.7071068,1.0/
DATA SENALT,VEHALT,MDIM/3,10,15/

C
C ***      INITIALIZE      **
C

REWIND 6
ZCURVE= RE.GT.0.0
ZGRID = GRID
RE    = RE/ZGRID
DZ    = 0.0
C *** AREA LIMITS   **
NORTH = KMAT*MCIM
SOUTH = 1
C

DO 2400 JK=1,ISTRIP
JSTRIP = JK
EAST = JSTRIP*MCIM
WEST = (JSTRIP-1)*MDIM+1
CALL INDATA
LH = 1
ILCOF = NLCW
DO 2400 KLN=1,2
C
DO 2000 KK=1,NSITE
KSIT = ISITE(KK,2)
YSIT = ISITE(KK,1)
ZSIT = ISITE(KK,3)+SENALT
C
DO 2000 LP=1,ILOOP
C *** TEST IFINISH FOR COMPLETION   **
IEXP = (LH-1)*10+KK-1

```

```

IFIN = AND(IFINISH(LP),2**(IEXP))
IF(IFIN .NE. 0) GO TO 2000
IF(LH .EG. 2) GO TC 400
C
KS1 = LOWCEN(LP,2)
IF (((KS1.GT.EAST) .AND. (KSIT.GT.EAST))
1 .OR. ((KS1.LT.WEST) .AND. (KSIT.LT.WEST))) GO TO 2000
C
C *** DETERMINE WESTERN MOST POINT OF PAIR ***
IF((KSIT-KS1) .GE. 0) GO TO 300
C
C *** SWAP SENSOR AND NODE ***
C
XP = KS1
YP = LOWCEN(LP,1)
ZP = LOWCEN(LP,3)+VEHALT
KS1 = KSIT
XS1 = KSIT
YS1 = YSIT
ZS1 = ZSIT
GO TO 525
C
300 XS1 = KS1
YS1 = LOWCEN(LP,1)
ZS1 = LOWCEN(LP,3)+VEHALT
XP = KSIT
YF = YSIT
ZP = ZSIT
GO TO 525
C
400 KS1 = HICEN(LP,2)
IF (((KS1.GT.EAST) .AND. (KSIT.GT.EAST))
1 .OR. ((KS1.LT.WEST) .AND. (KSIT.LT.WEST))) GO TO 2000
C
C *** DETERMINE WESTERN MOST POINT OF PAIR ***
IF((KSIT-KS1) .GE. 0) GO TC 410
C
C *** SWAP SENSOR AND NODE ***
C
XP = KS1
YP = HICEN(LP,1)
ZP = HICEN(LP,3)+VEHALT
KS1 = KSIT
XS1 = KSIT
YS1 = YSIT
ZS1 = ZSIT
GO TO 525
C
410 XS1 = KS1
YS1 = HICEN(LP,1)
ZS1 = HICEN(LP,3)+VEHALT
XP = KSIT

```

```

      YP = YSIT
      ZP = ZSIT
C
C *** CALCULATE TANGENT AND DISTANCE BETWEEN SENSOR/NODE   **
C *** THE AZIMUTH ANGLE IS MEASURED FROM NCRTH CLOCKWISE    **
C
      525 XSP = XP-XS1
          YSP = YP-YS1
          ZSP = ZP-ZS1
          DIS = SQRT(XSP**2 + YSP**2)
          IF(ZCURVE) DZ=0.5*DIS*(DIS/RE)
          TM = (ZSP-DZ)/(DIS*ZGRID)
          XSIN = XSP/DIS
          YCOS = YSP/DIS
          ZNORTH = .FALSE.
          ZSOUTH = .FALSE.

C
C *** DETERMINE STARTING INDICES AND MAP SHEET BOUNDARIES   **
C
      10 IF(KS1 .LT. WEST) GC TO 560
          NX = XS1-WEST
          YWEST = 0.0
          GC TO 570
      560 NX = 0
          YWEST = YCCS*((WEST-XS1)/XSIN)
      570 IF (ABS(XSIN).LE.SRTWH) GO TO 1150
C
C ***      EAST   **
C
      IX = NX
      X = IX+WEST
      IDX = 1
      1020 IX = IX+IDX
          X = X+RATE
          IF(IX .GT. MDIM) GC TO 2000
          R = (X-XS1)/XSIN
          JY = R*YCOS+YS1
          NAR = (JY-1)/MDIM
          JY = JY-NAR*MDIM
          NAR = NAR+1

C
C *** TANGENT FOR ALL COMPASS DIRECTIONS   **
C *** IF NAR OUTSIDE MAP SHEET - LOS EXIST   **
C
      1075 IF((NAR .LT. SOUTH) .OR. (NAR .GT. \CRTH)) GO TO 1800
          Z = ICATA(JY,IX,NAR)
          IF(ZCURVE) DZ=0.5*R*(R/RE)
          T = (Z-ZS1-DZ)/(R*ZGRID)
          IF(T .LE. TM) GO TO 1090
          GO TO 1900
      1090 IF(R .GE. RMAX) GC TO 1800
          IF(ZNCRTH) GC TO 1130

```

```

IF(ZSCUTH) GO TO 1135
GO TO 1020
C
C *** NORTH ***
C
1130 Y = Y+DY
JY = JY+JDY
IF(JY .LE. MDIM) GO TO 1140
JY = 1
NAR = NAR+1
GO TO 1140
C
C *** SOUTH ***
C
1135 Y = Y+DY
JY = JY+JDY
IF(JY .GE. 1) GO TO 1140
JY = MDIM
NAR = NAR-1
1140 R = (Y-YS1)/YCOS
IX = R*X SIN+XS1
IF(IX .GT. MCIM) IX=IX-WEST+1
IF(IX .GT. MCIM) GO TO 2000
GO TO 1075
1150 IF(YCOS .GT. 0.0) GO TO 1160
C
C *** SCLTH ***
C
ZSOUTH = .TRLE.
JY = YS1+YWEST-RATE
NAR = (JY-1)/MCIM
JY = JY-NAR*MCIM
NAR = NAR+1
Y = YS1+YWEST-RATE
DY = -RATE
JDY = -1
GO TO 1140
C
C *** NORTH ***
C
1160 ZNORTH = .TRLE.
JY = YS1+YWEST
NAR = JY/MDIM
JY = JY+1-NAR*MCIM
NAR = NAR+1
Y = YS1+YWEST+RATE
DY = RATE
JDY = 1
GO TO 1140
1800 IF(LH .EG. 2) GO TO 1850
DETLO(LP) = DETLO(LP)+1.0
DISLO(LP) = DISLO(LP)+DIS

```

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